

# CS Repair and Refurbishment Developments at SDSM&T

Christian Widener, Ph.D.

**South Dakota School of Mines and Technology  
& VRC Metal Systems**

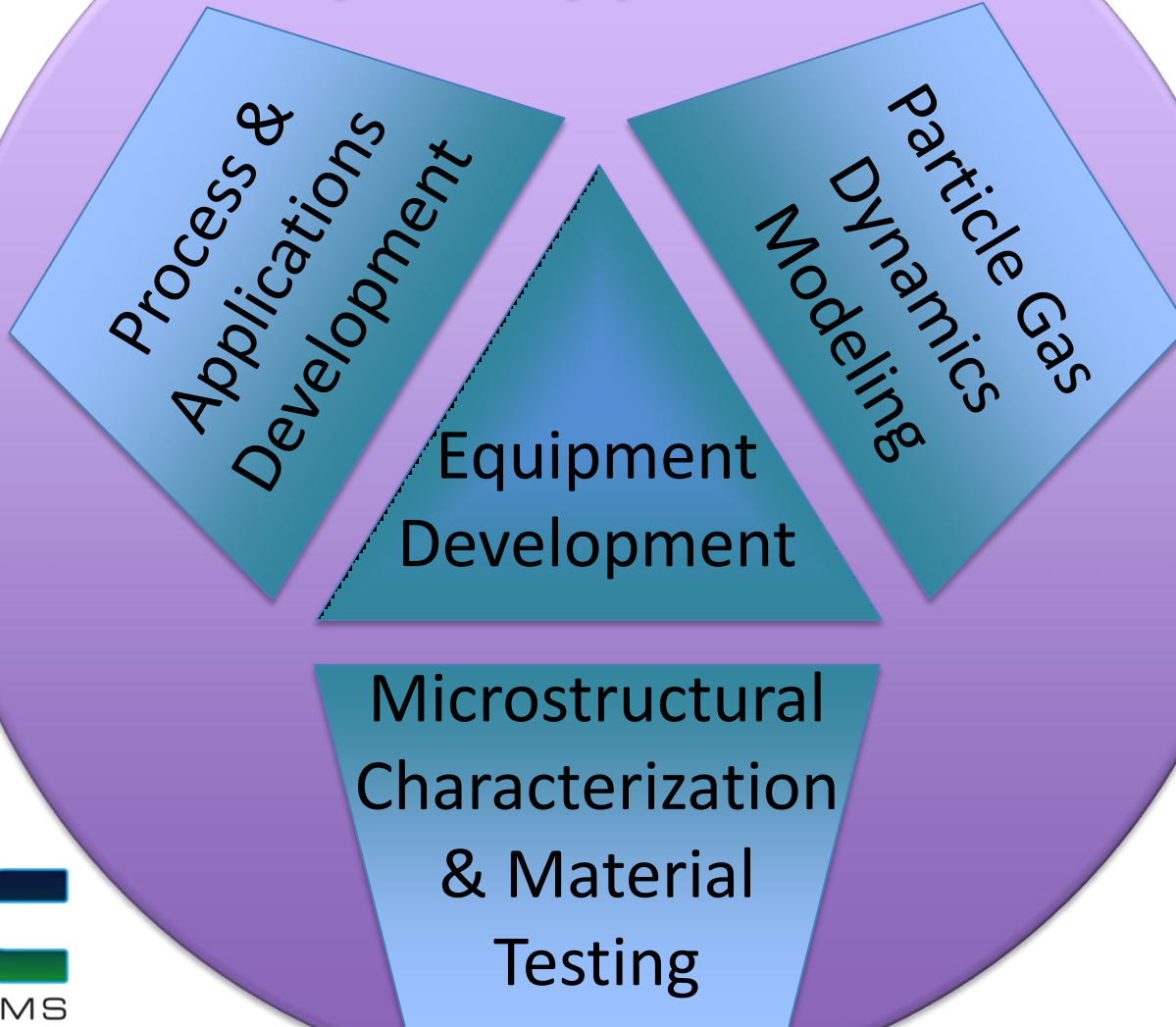
**Michael Carter, Todd Curtis, Ozan Ozdemir, Reza  
Rokni,**

**Dr. Grant Crawford, Dr. Bharat Jasthi, Dr. Marius  
Ellingsen**

**South Dakota School of Mines and Technology**



# Repair Applications



# Applied Research Efforts Underway

- **Microstructural Investigation & Material Testing**
  - Emphasis on understanding metallurgy of powders & coatings
  - Aluminum & other structural alloys
- **Computational Fluid Dynamics Modeling**
  - Nozzle Design & Parameter Prediction
  - Gas Mixing
- **Equipment Development**
  - VRC Gen III
  - Supporting Equipment: Nozzles, Motion Systems, Powder Processing
- **Applications Development**
  - Repair for DOD components
  - Cold Spray as Coating & Additive Process for new parts

# Microstructure

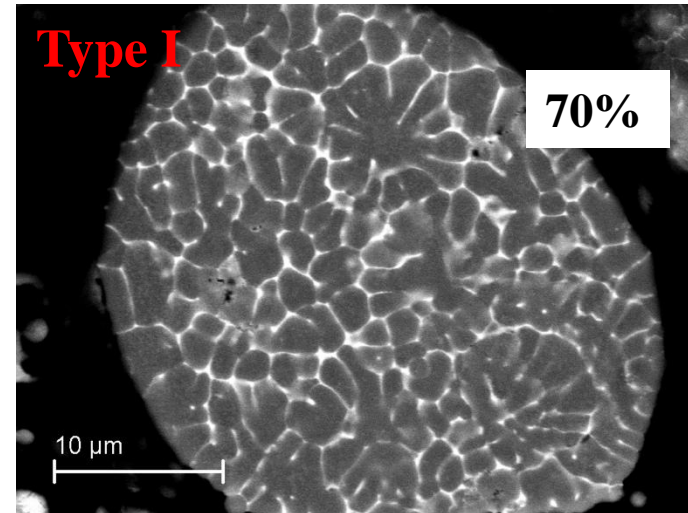
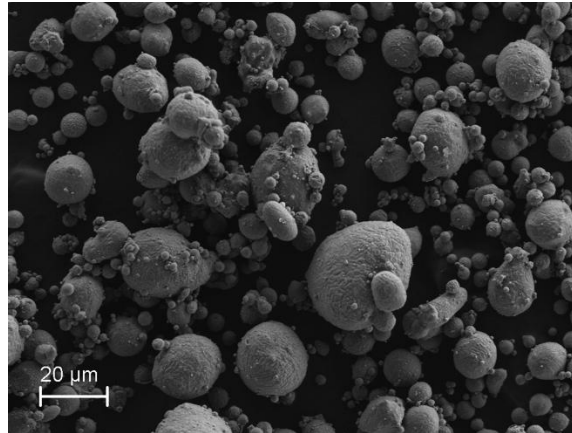
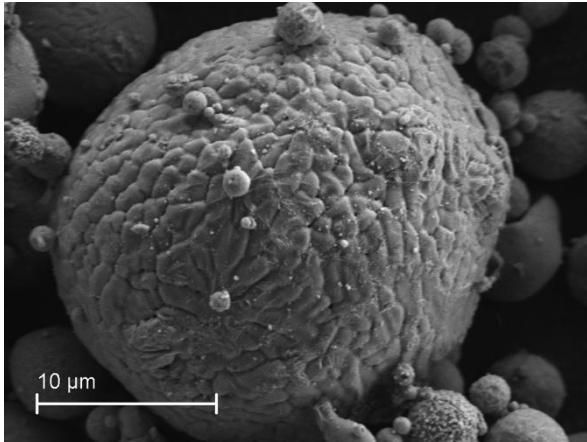
- **Lessons Learned**

1. Cold Spray retains the microstructure of the powder material.
  - Solid state
  - Minimal time for diffusion
  - Addition of plastic strain
2. Better properties can be achieved through optimization of powder material conditions and process parameters.
  - Structural properties are possible...

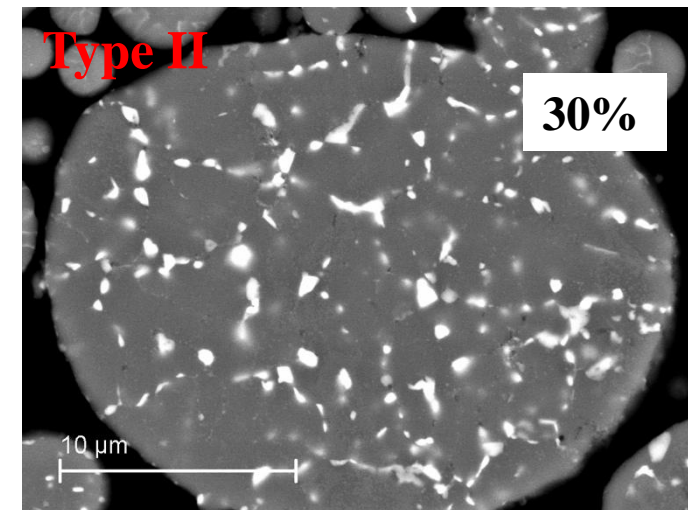
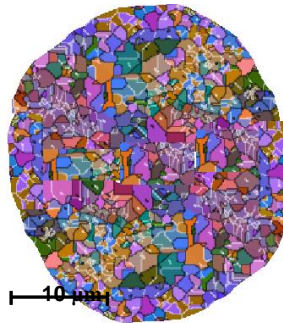
# Powder Characterization

- Standard Testing
  - **Hardness** – needed for modeling
  - **SEM images** – understand morphology
  - **Microtrack particle analysis** – understand size distribution
    - Fines – clogging – deposition quality
    - Size range – deposition efficiency
  - **DSC** – understand material condition (temper & thermal sensitivity)
  - **EBSD** – understand elemental distribution, grain size, etc.

# Al 7075 Powder Microstructure



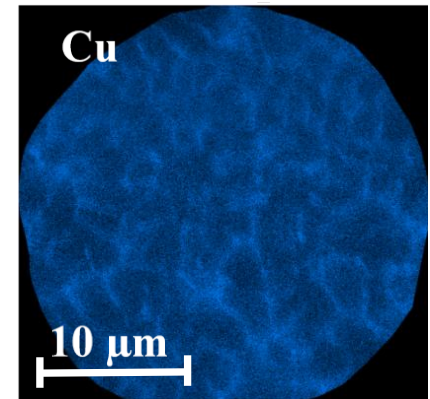
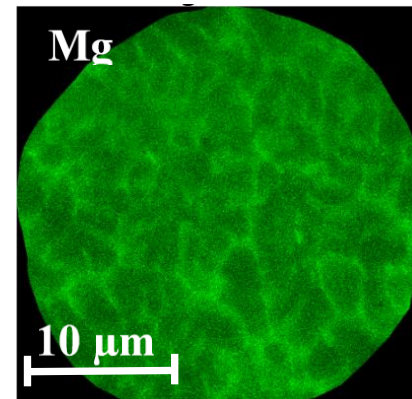
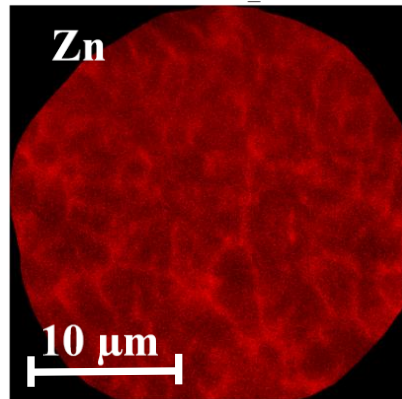
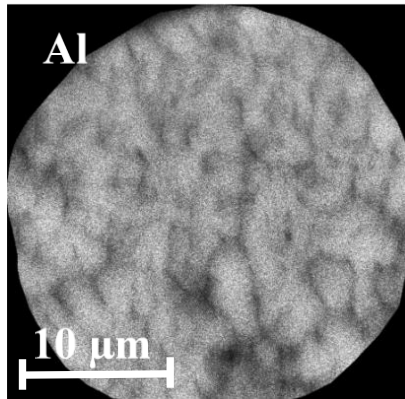
- Valimet 7075 -325 Mesh powder
- Variable particle size
- Particle Dia:  $18.6 \pm 8.2 \mu\text{m}$
- Powder grain size: 1-4  $\mu\text{m}$
- Two particle microstructure types



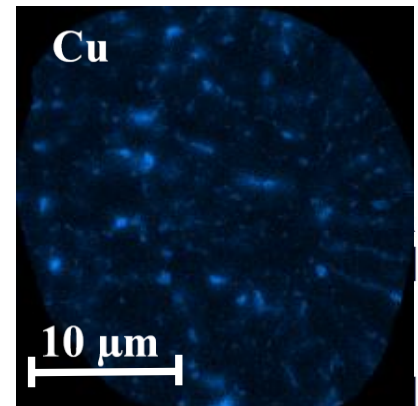
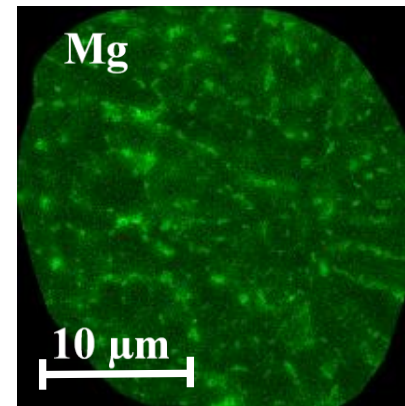
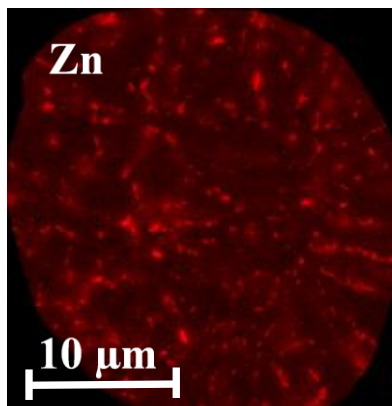
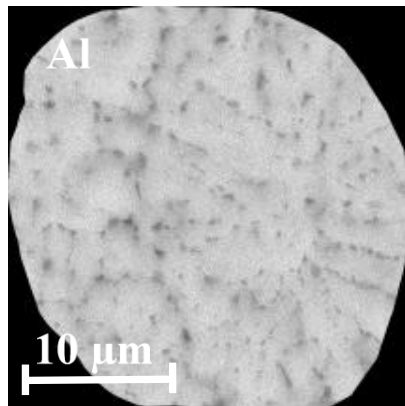


# EDS Map of Al 7075 Powder Cross Section

Type I

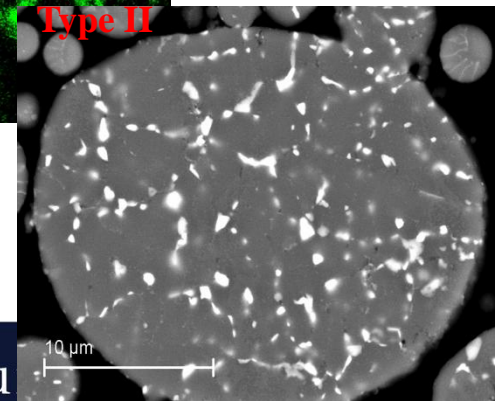
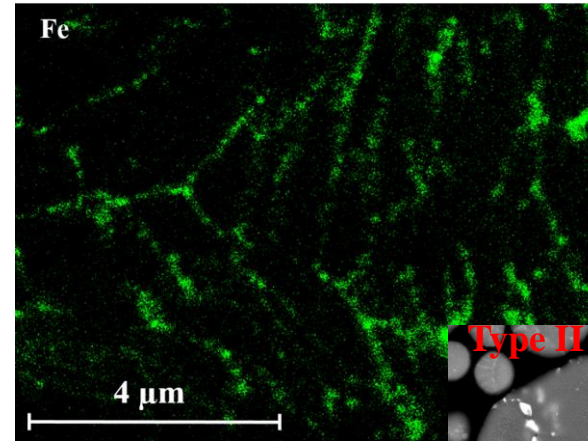
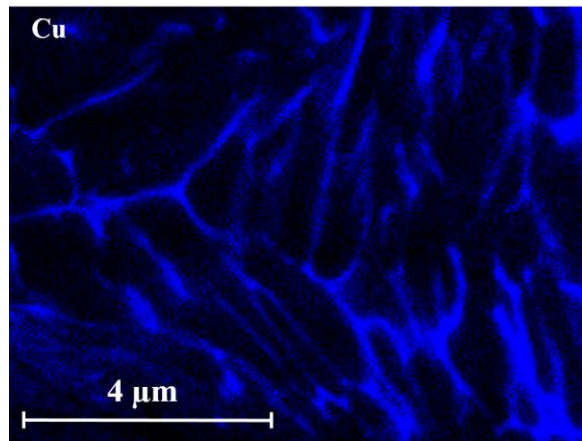
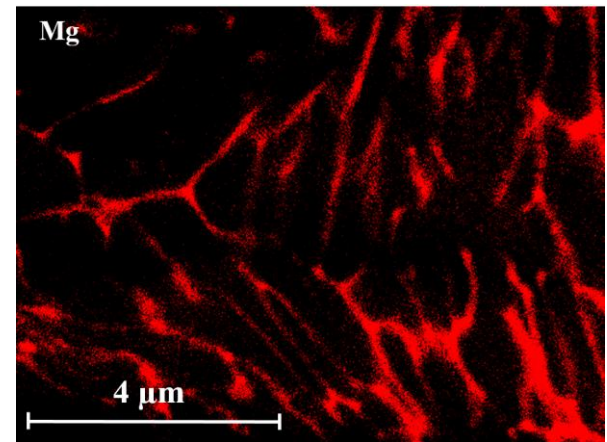
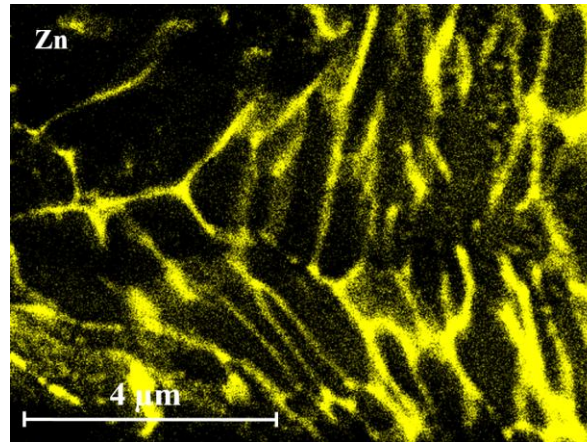
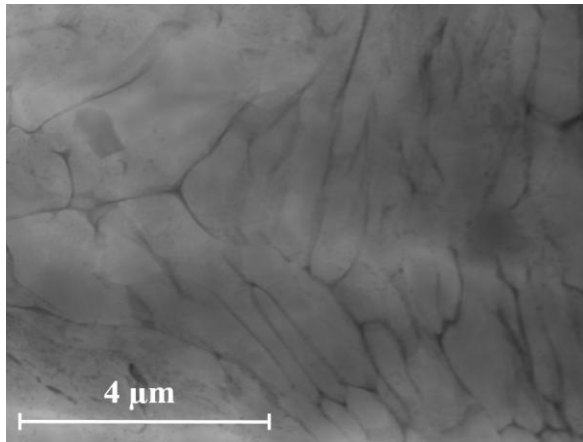


Type II



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# Segregation at GB's



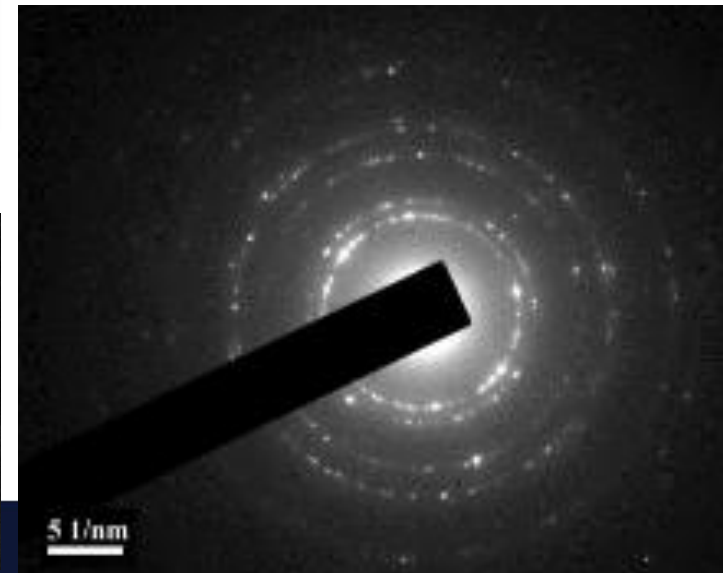
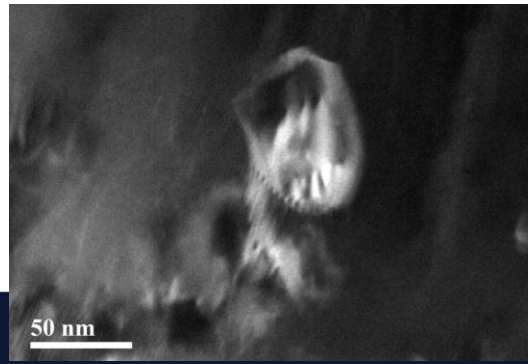
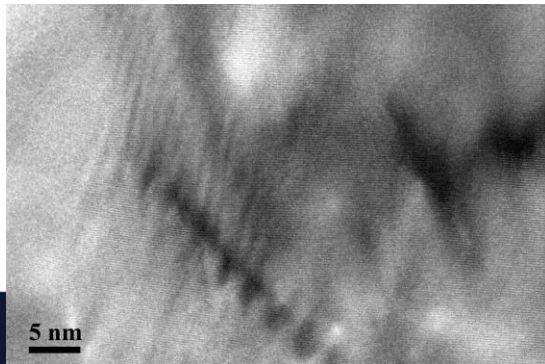
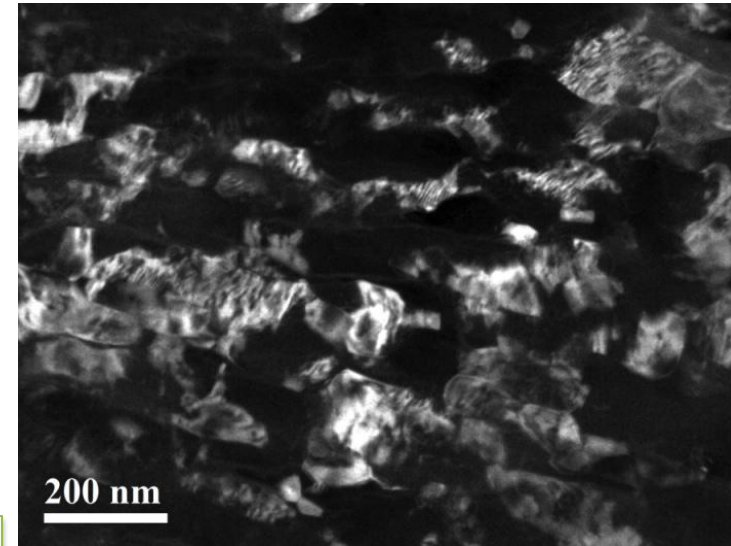
- ✓ Solute segregation at the grain boundaries
- ✓ Demonstrates powder condition is retained in the deposition



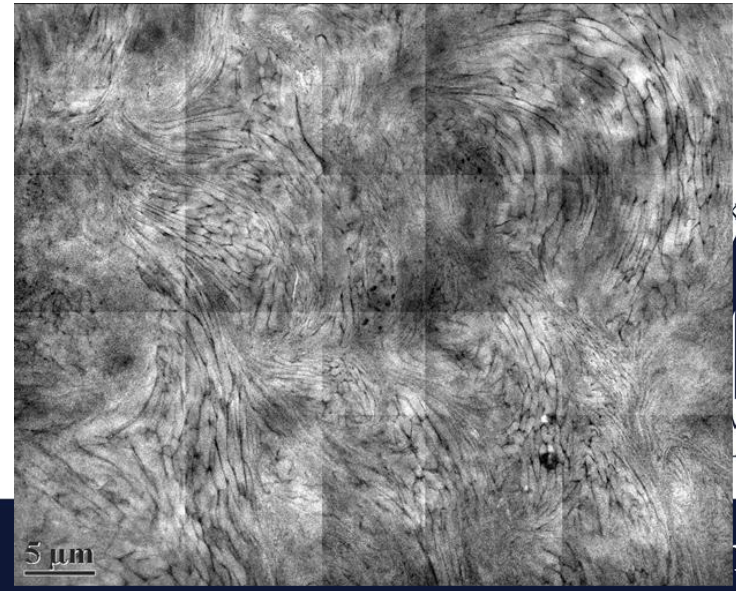
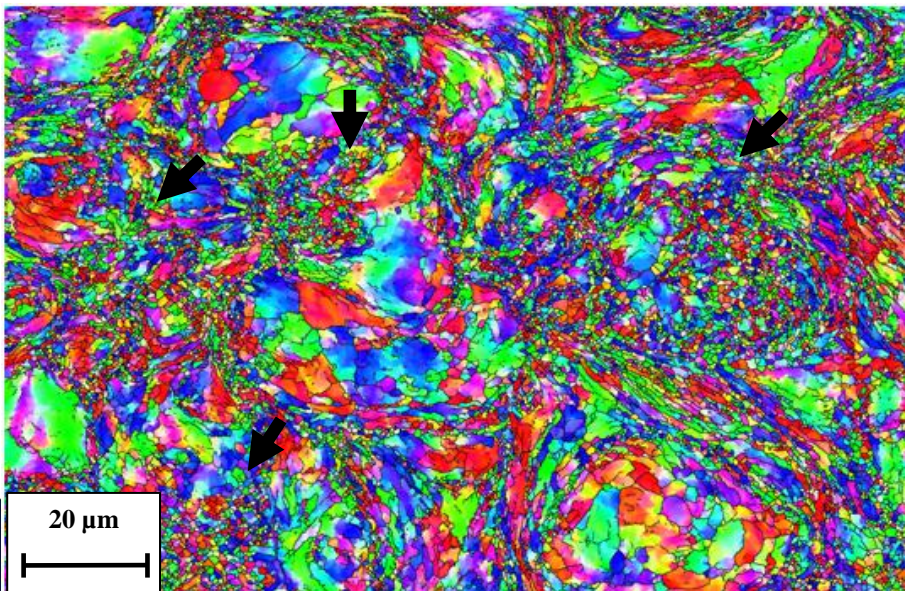
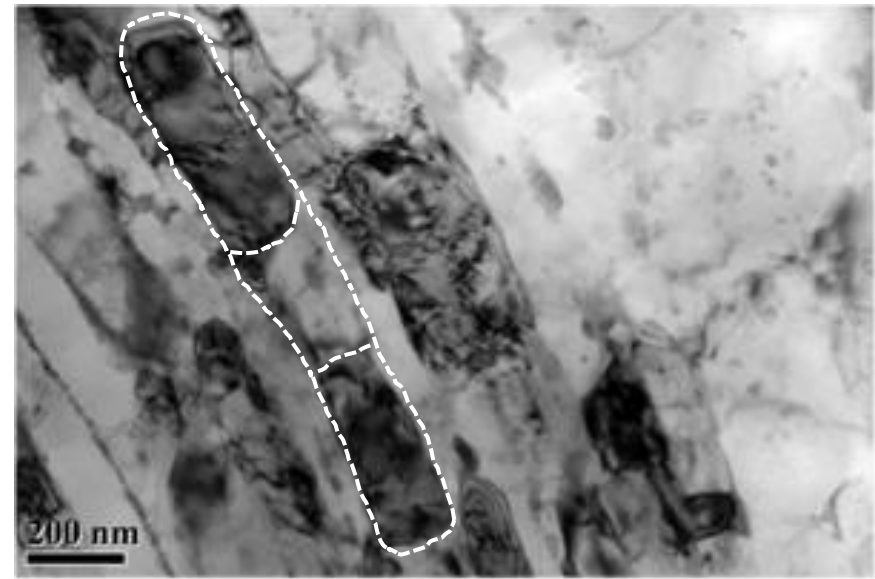
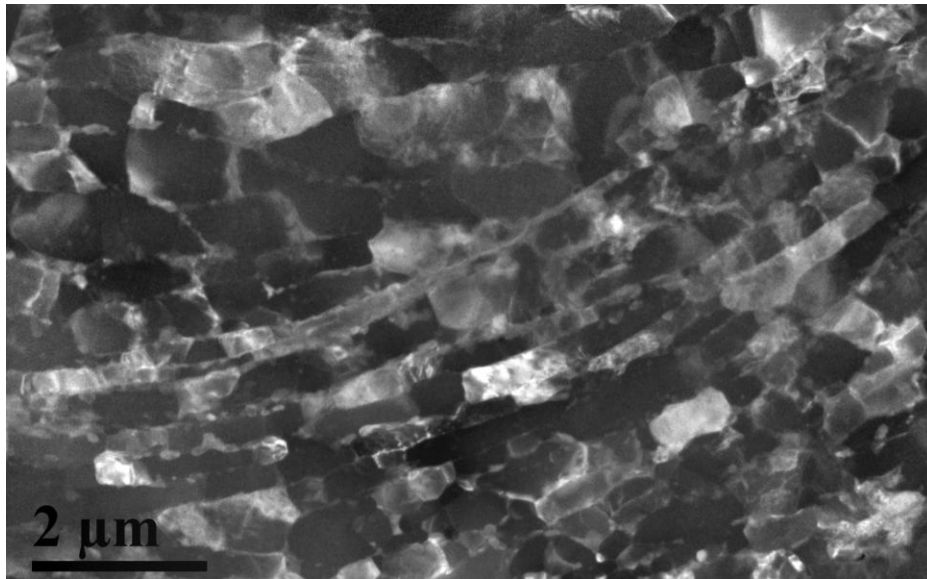
# TEM study of the powder

- Internal UFG and even nano structures in powder particles
- Residual stress shown in SADP
- Moderate dislocation density, concentrated near

Studying the powder helps to better interpret the microstructures in CS

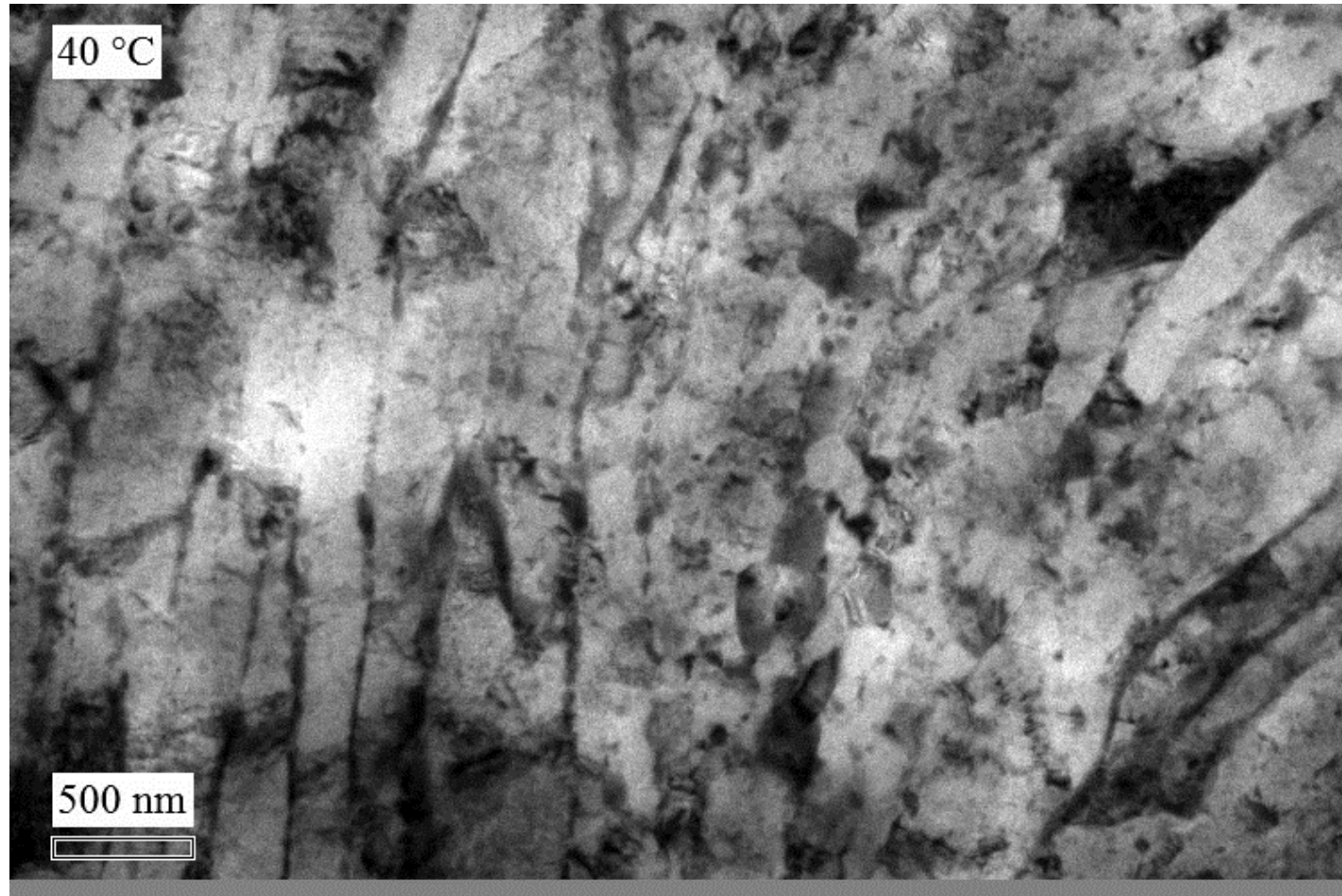


# In-depth Characterizations



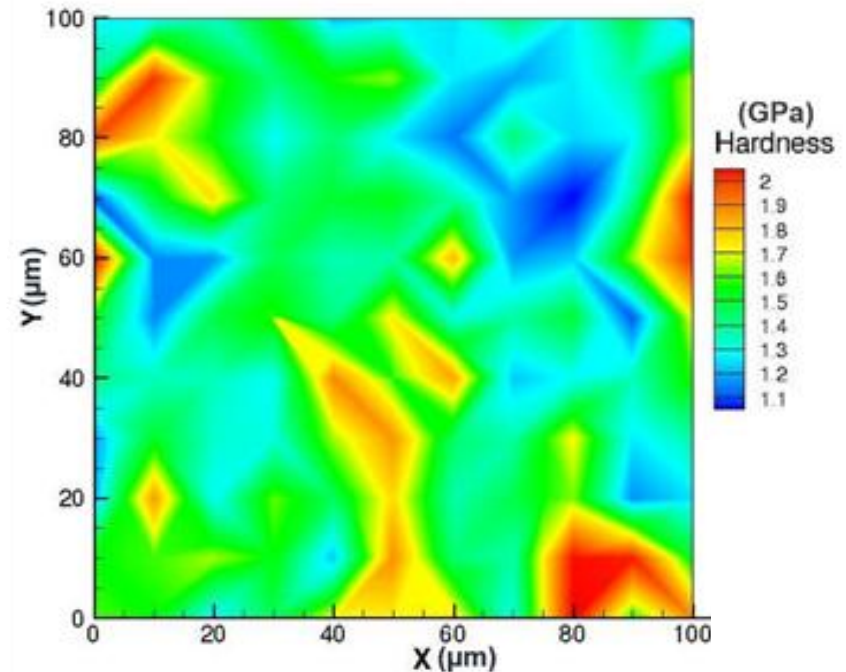
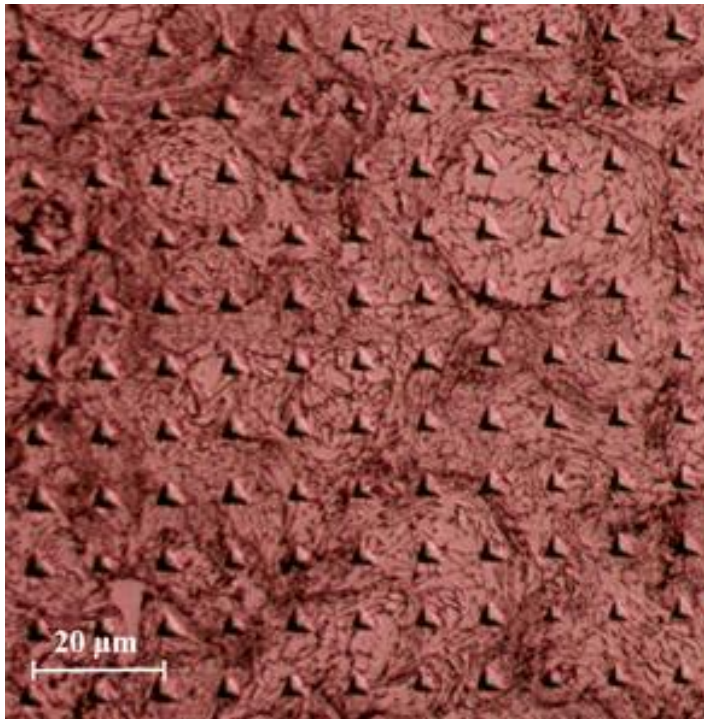


# Non-isothermal HT



Microstructural Characterization Work Performed by  
SDSM&T Ph.D. Graduate – M. Reza Rokni

# Nanoindentation



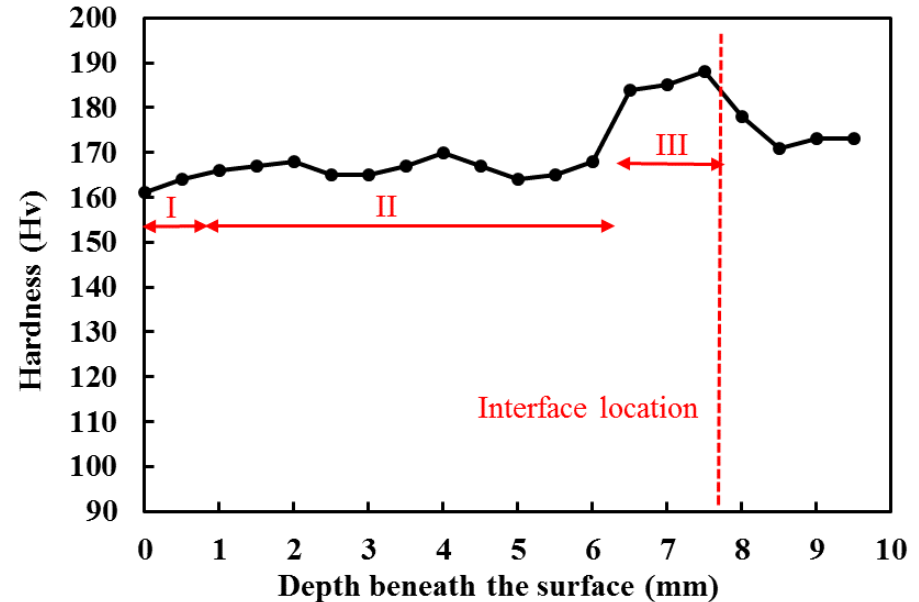
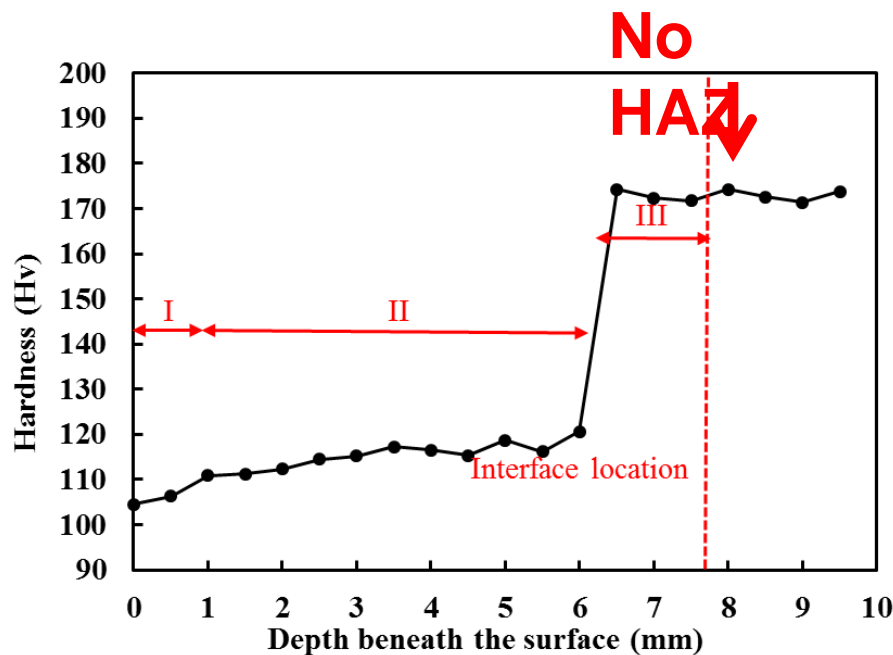
- ✓ 100  $\mu\text{m}$  square array of nanoindentations (121 indents)
- ✓ Regions of high and low hardness associated with particle impacts

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Material	CSP 7075	
Hardness (GPa)	particle interior	particle interfaces
	$1.53 \pm 0.30$	$2.01 \pm 0.09$



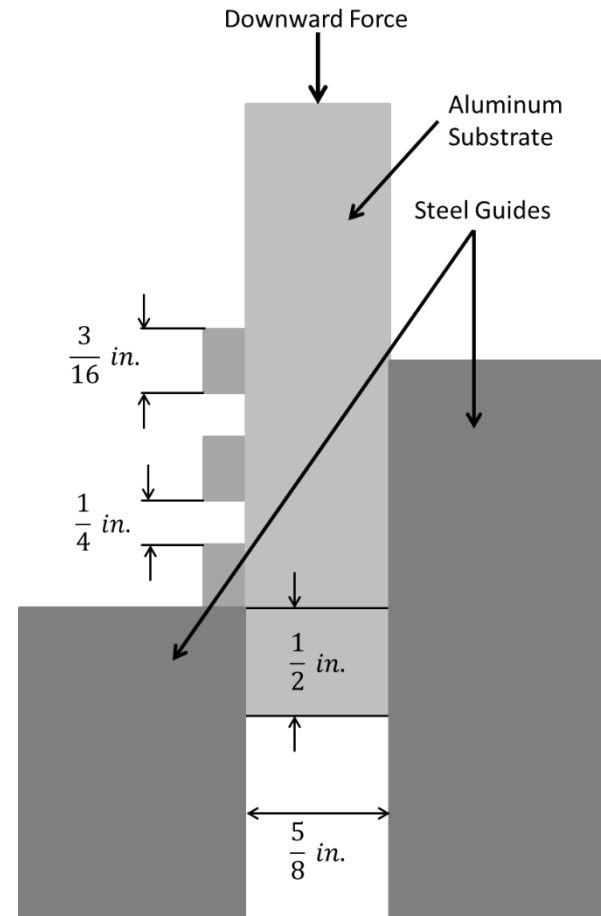
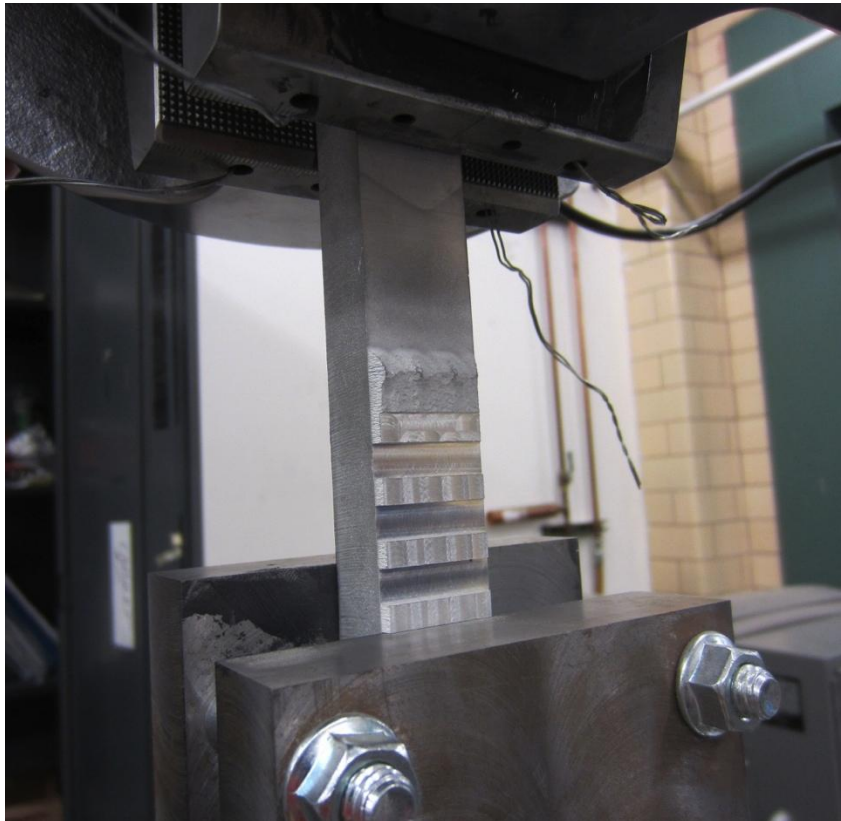
# Al 7075 Cold Spray with PWAA



- Vickers microhardness distribution from the top of the CSP 7075 layer to the substrate: before T-73 heat treatment (left) and after T-73 heat treatment (right).
- The dashed red line represents the location of the deposit/substrate interface.

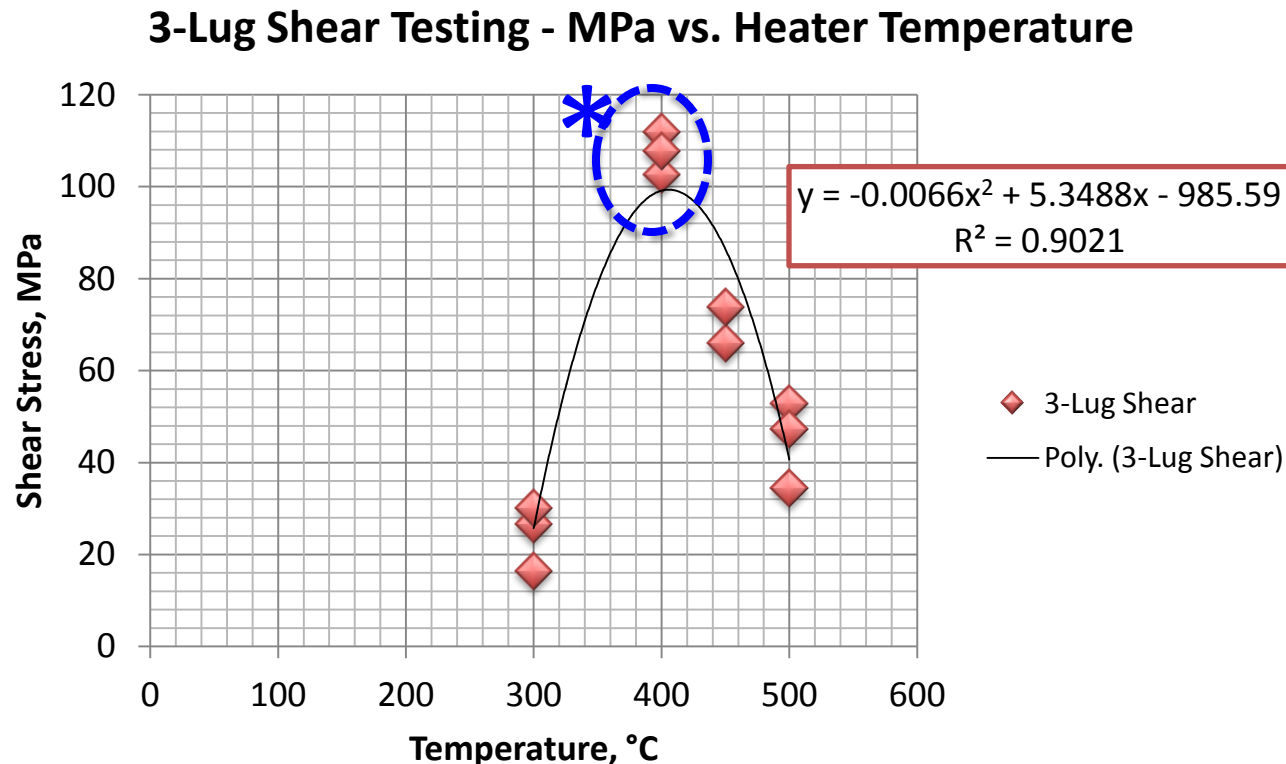
# Mechanical Testing

- 3-Lug Shear Testing – per *MIL-J-24445A*



# AI 6061 Mechanical Testing – Internal Bore Application

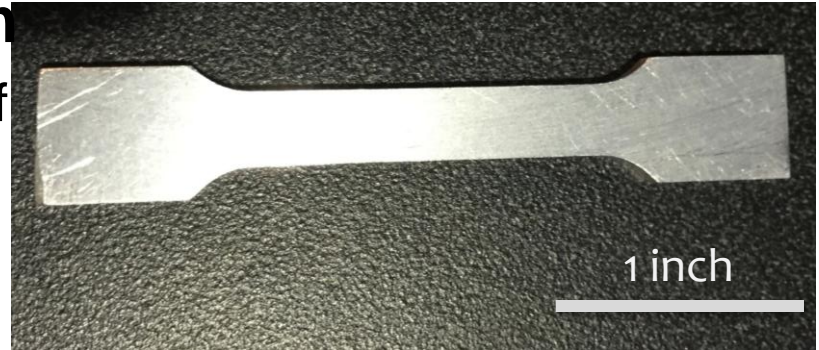
- ASTM C633 Testing – Masterbond EP15 – glue failures >10 ksi
- Three Lug Shear =  $107.4 \pm 4.60$  Mpa
- Lower, but still very high strengths were achieved with the shear (see graph).



# Tensile Strength

- **ASTM E8 – Subscale Coupon**

- Machined from a large build-up of cold spray material.
- Substrate material is not included



- **Al 6061**

- Yield Strength =  $35.5 \pm 1.05$  ksi
- UTS =  $45.4 \pm 0.37$  ksi
- %EL =  $5.5\% \pm 0.77\%$
- Hardness = 90 HV

- **Al 2024**

- Yield Strength = 45.9 ksi
- UTS = 50.1 ksi
- %EL = 5.5 ksi
- Hardness = 167 HV

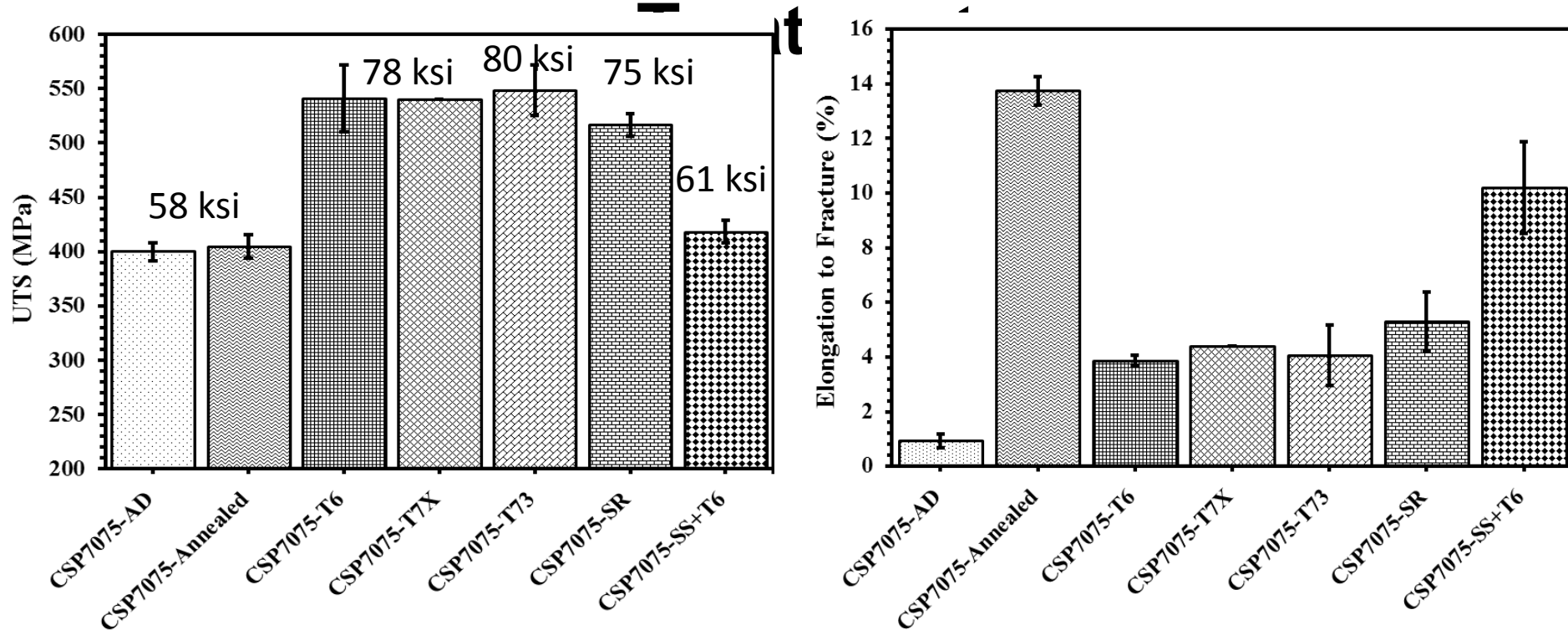
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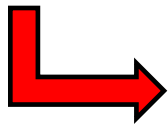
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# Al 7075 Mechanical Properties vs. Heat



- ✓ Superior mechanical properties in the heat treated conditions (samples were microtensiles 10mm x 1mm x 1mm)



Due to grain boundary strengthening and metallurgical Bonding

# Fluid Dynamics Modeling

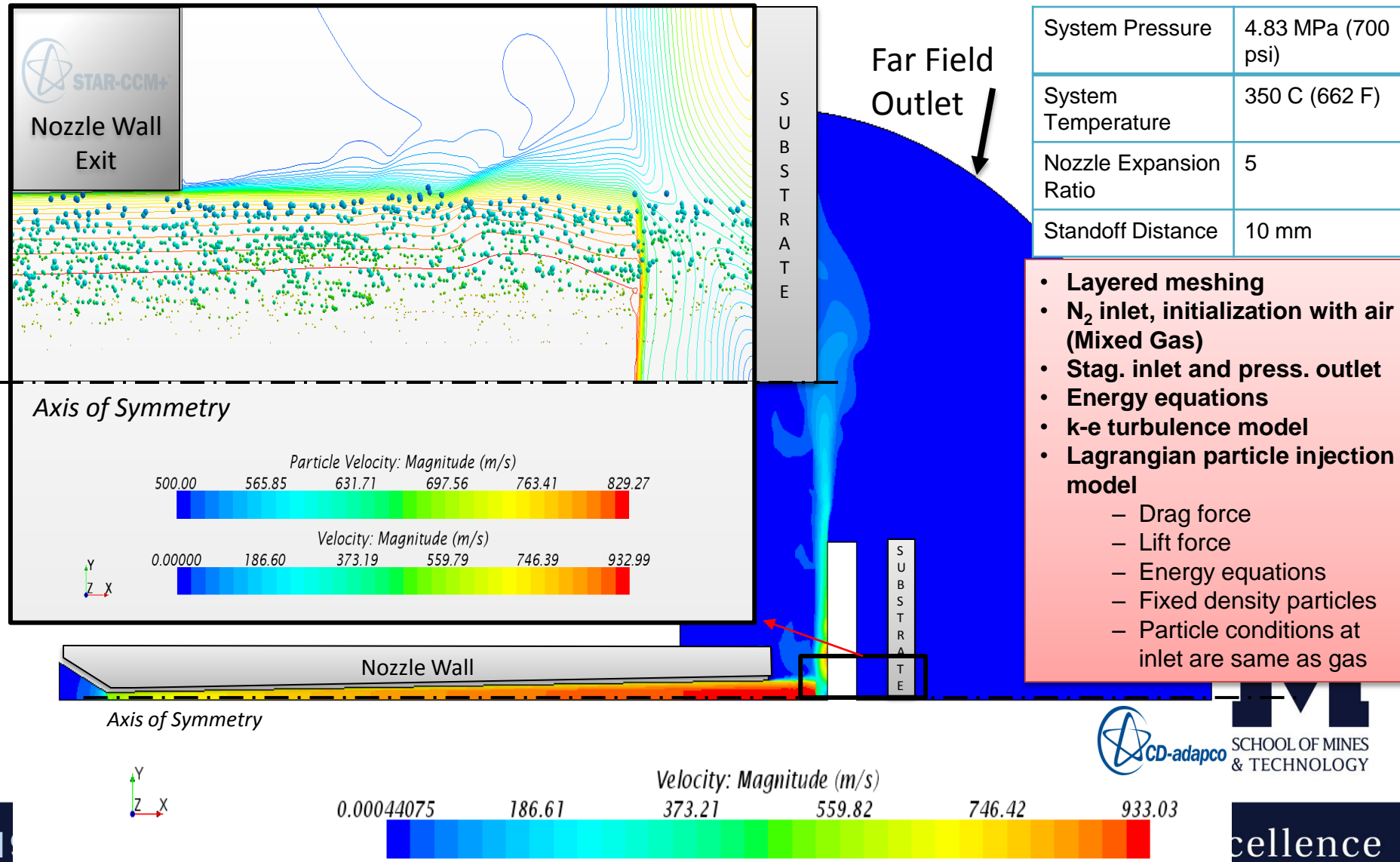
1. **Process modeling is maturing.**
2. Particle **velocities and temperatures** can be **accurately predicted** for a range of process conditions.
3. **Still requires experimentation**, and bonding is not just a function of process parameters, but much better than a shot in the dark.

Modeling Work Performed by SDSM&T Ph.D. Candidate –  
Ozan Ozdemir

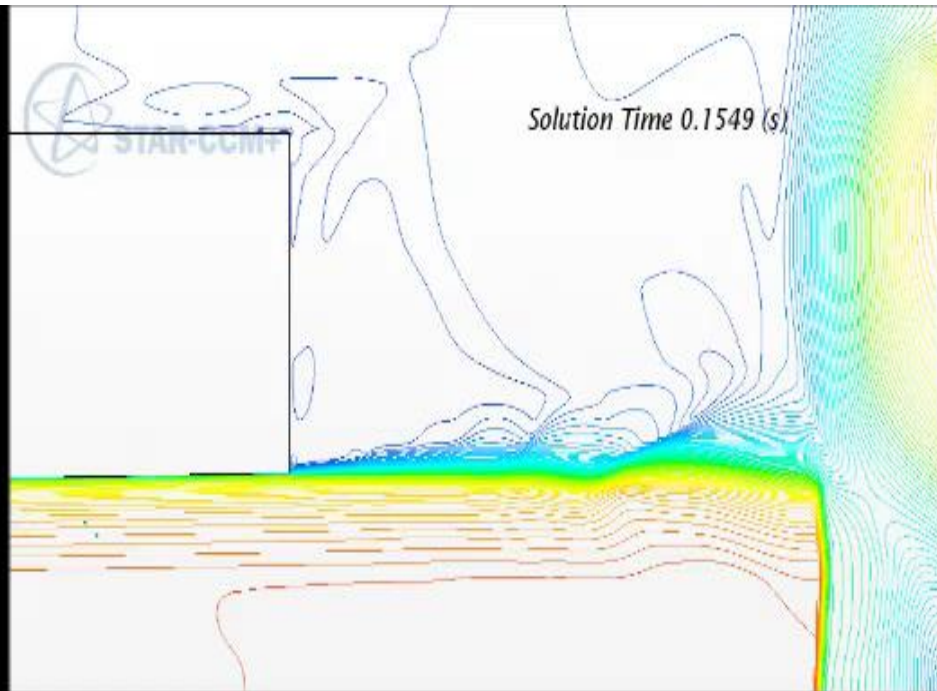


# 2D Axisymmetric CFD Model

## Variability of Particle Impact Velocity



# Transient Behavior of Particles



Particle Velocity: Magnitude (m/s)

500.00	580.00	660.00	740.00	820.00	900.00
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Velocity: Magnitude (m/s)

0.00000	186.60	373.19	559.79	746.39	932.99
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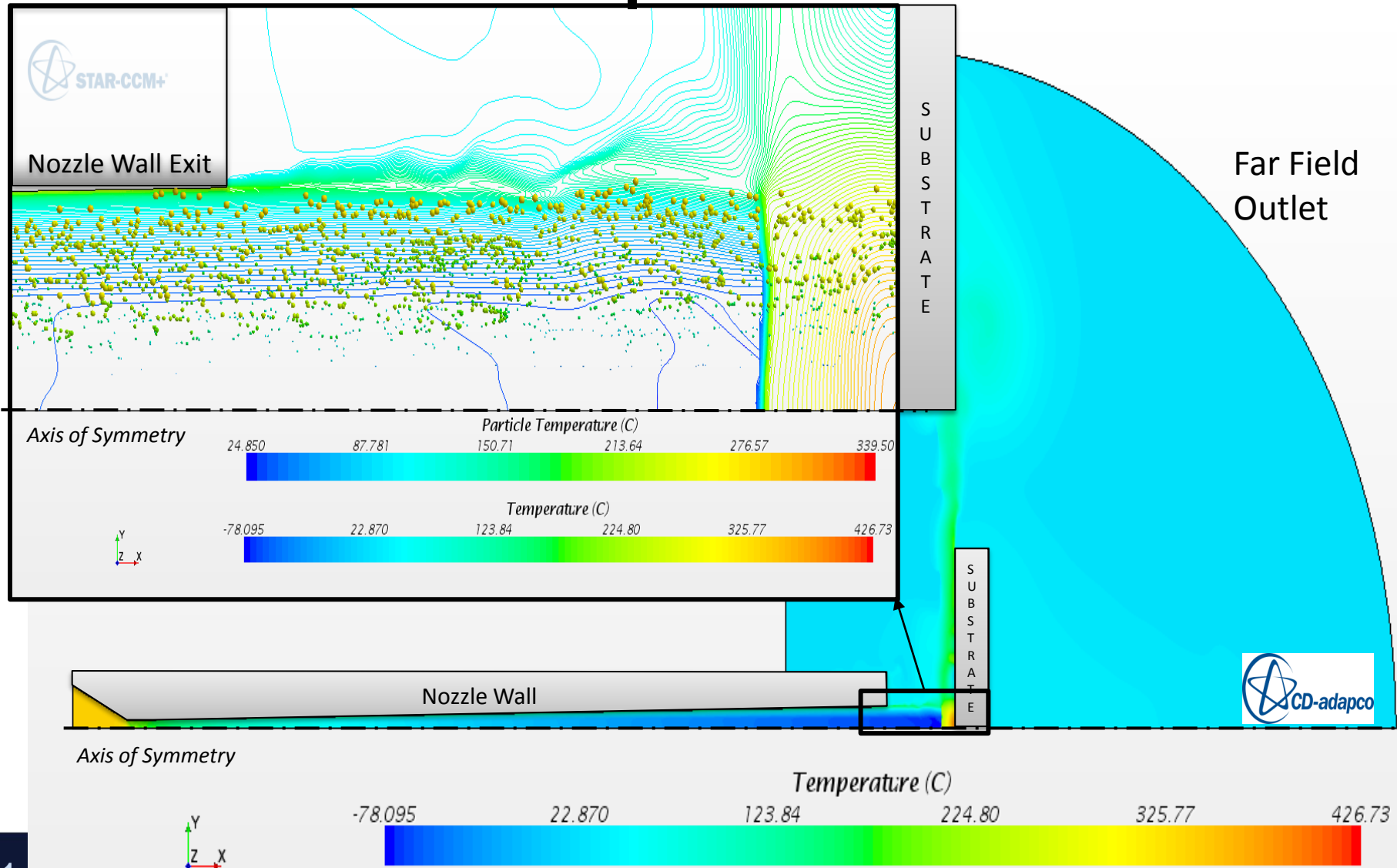
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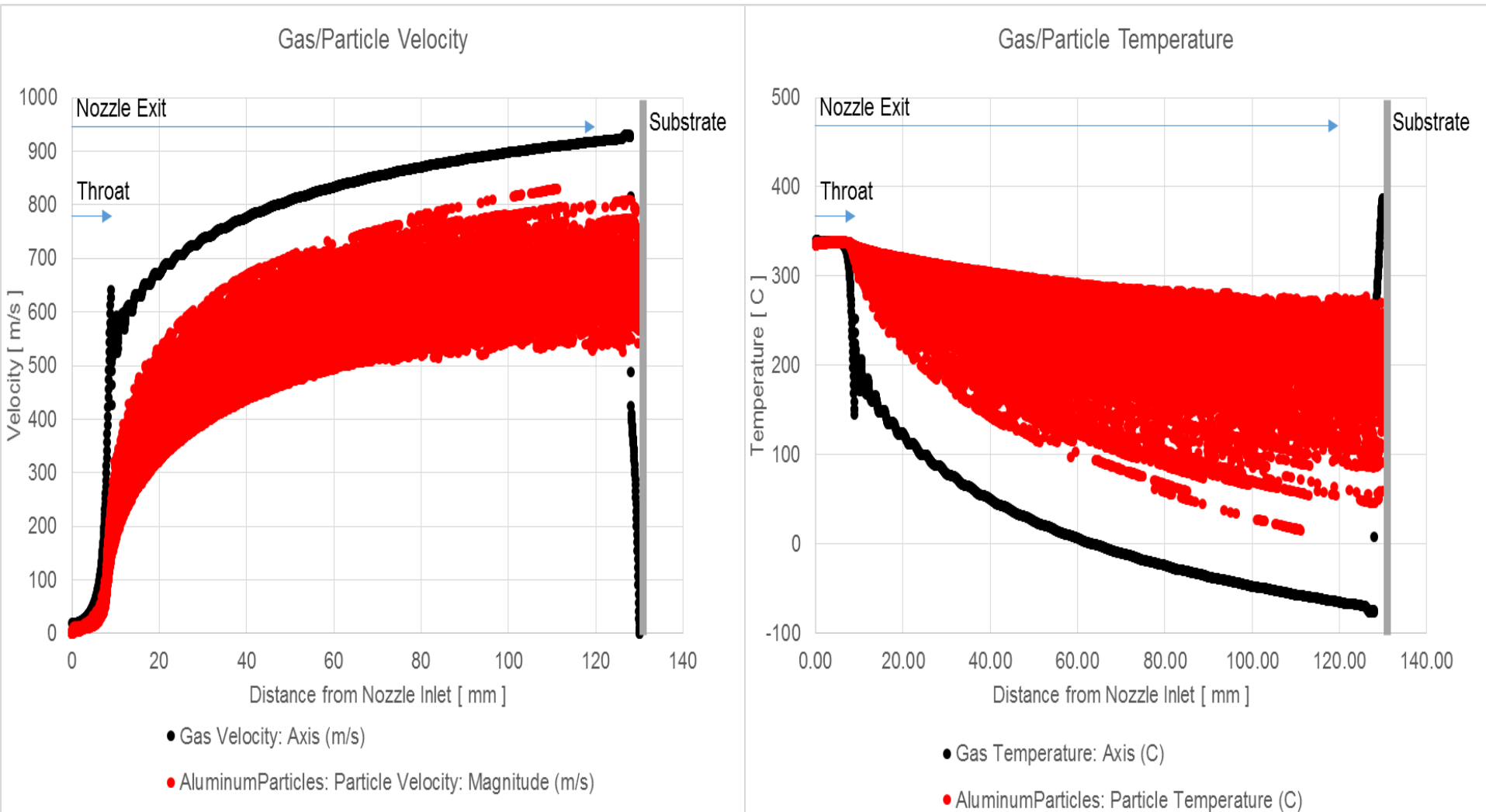
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# Variability of Particle Impact Temperature



# Velocity and Temperature Variation Plots Injection to Impact



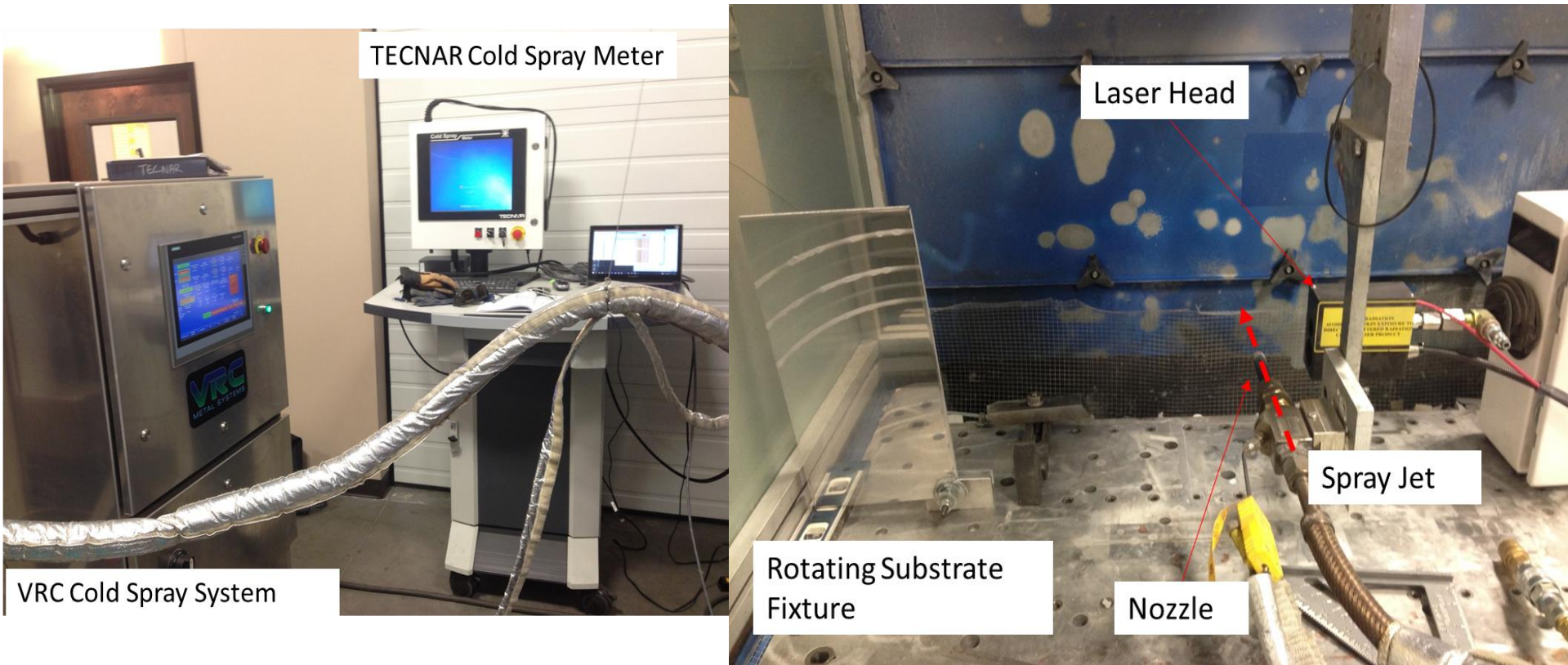
# Preliminary Calculations

## Selection of Spray Condition

*Select a system pressure and temperature He mixing can improve.*

T [C] \ P [ psi ]	500	600	700	800	900	1000
300	0.00%	0.00%	0.00%	0.00%	0.00%	0.00%
350	0.00%	0.00%	0.00%	0.00%	0.00%	0.10%
400	52.56%	63.80%	73.22%	82.13%	86.71%	91.12%
450	92.52%	96.82%	98.56%	99.54%	99.93%	99.93%
500	100.00%	100.00%	99.97%	99.97%	99.97%	99.97%

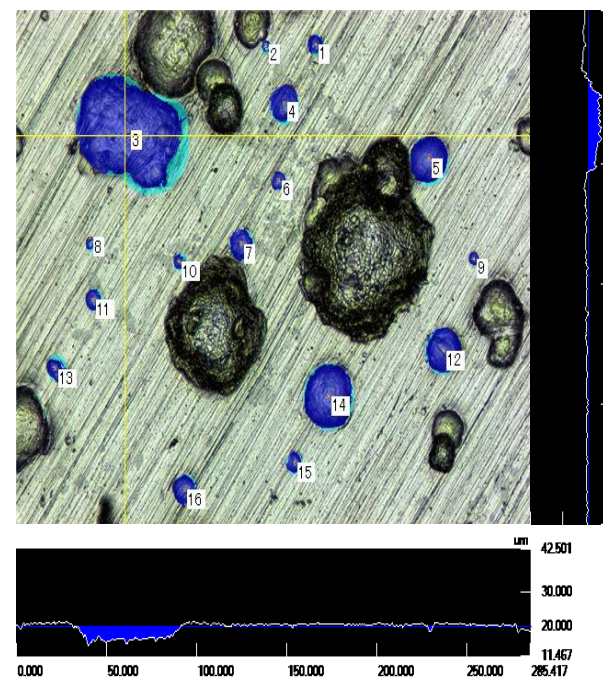
# Experimental Setup



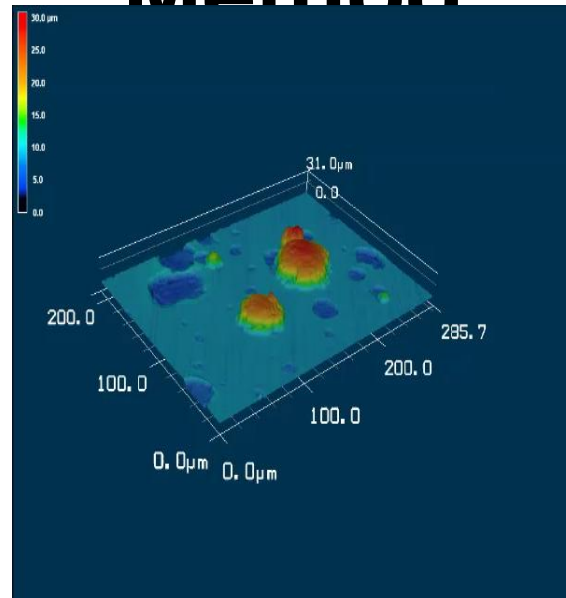
5 Different Conditions  
0% - 70% Helium Mixing into Nitrogen



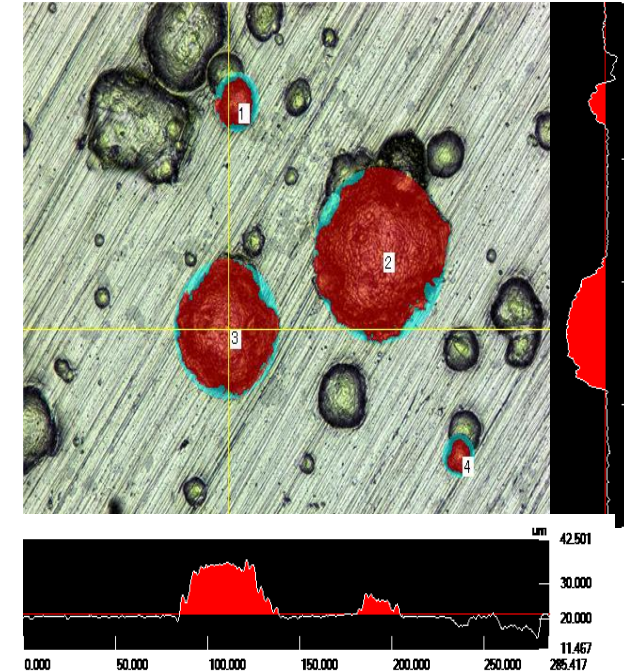
# Deposition Efficiency Measurement Method



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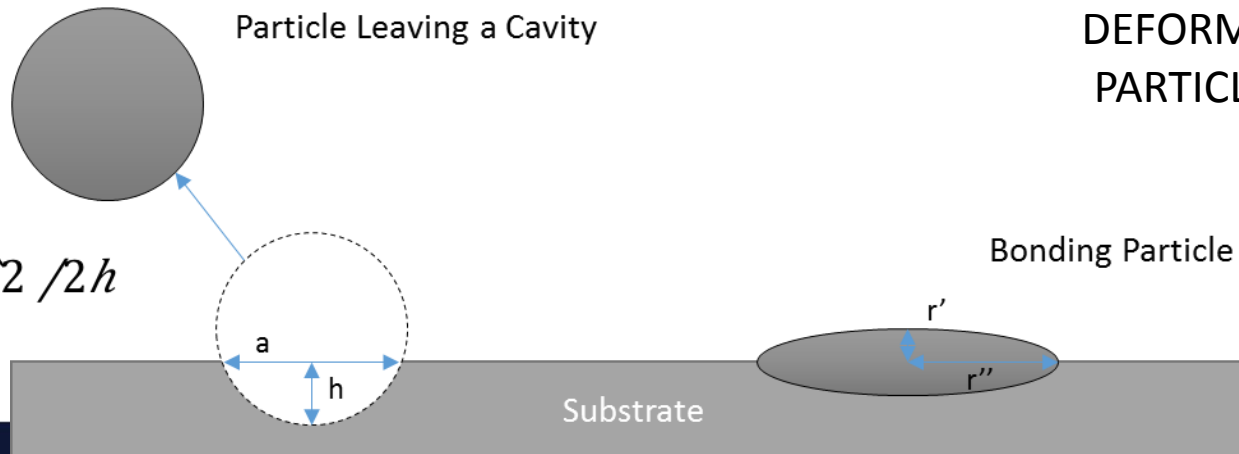


Particle Leaving a Cavity

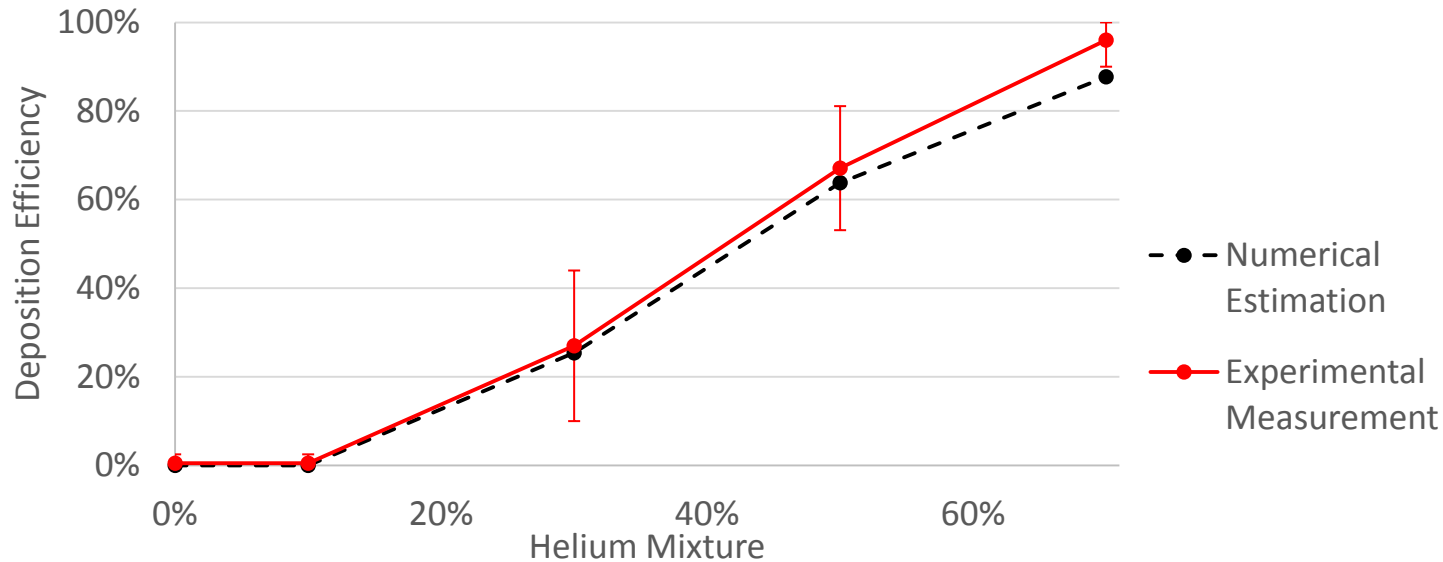


DEFORMED PARTICLES

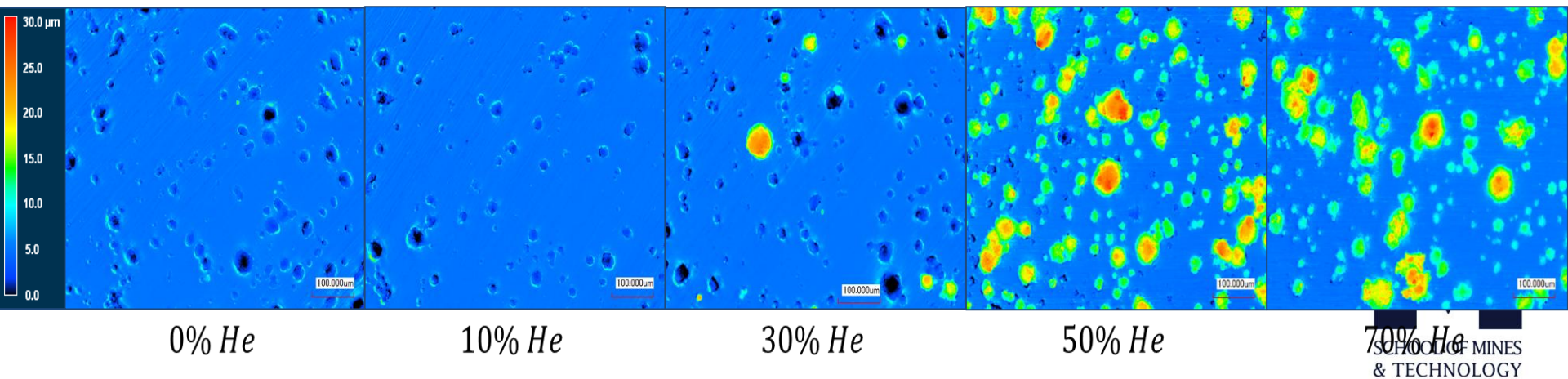
$$r = \sqrt{a^2 + h^2} / 2h$$



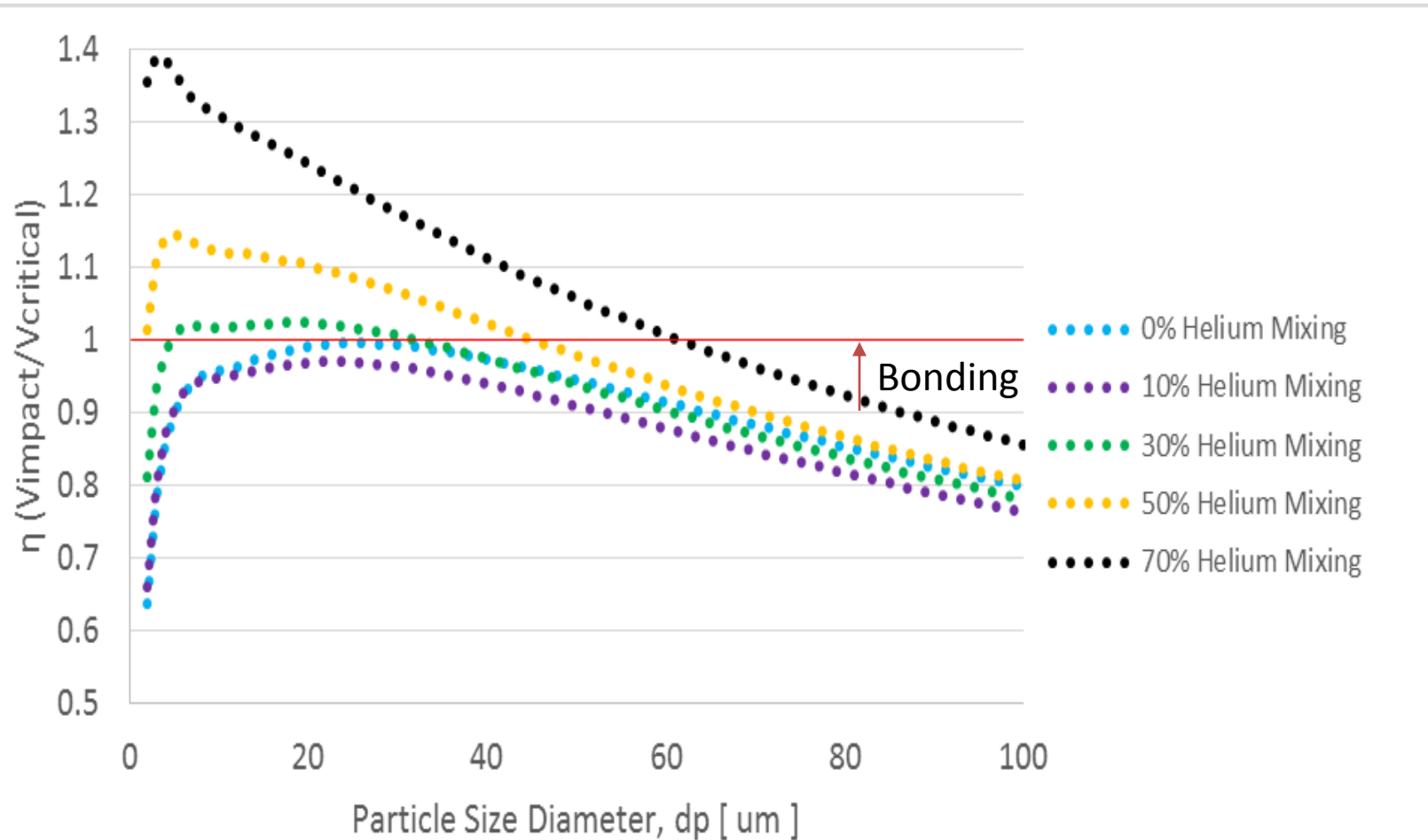
# Improving Deposition Efficiency with Helium Mixing



**METLAB**  
MATERIALS EVALUATION AND TESTING



# What does Helium Mixing in N<sub>2</sub> Do?



# Equipment Development

- **Efforts Underway**

1. VRC Gen III

- Gas mixing
- 1000 psi for Nitrogen is helpful
- Shorter nozzles for internal bores & confined areas
- Upstream feed option for particle heating

2. Supporting Equipment:

- Motion Systems
- Powder Processing



# VRC Gen III Cold Spray System

## Hand-Held Capable



- Working with VRC Metal Systems to develop cold spray equipment solutions
- The Goal is to support and accelerate cold spray implementation for suitable applications.
- Operates at 1000 psi to enable more with N<sub>2</sub>.

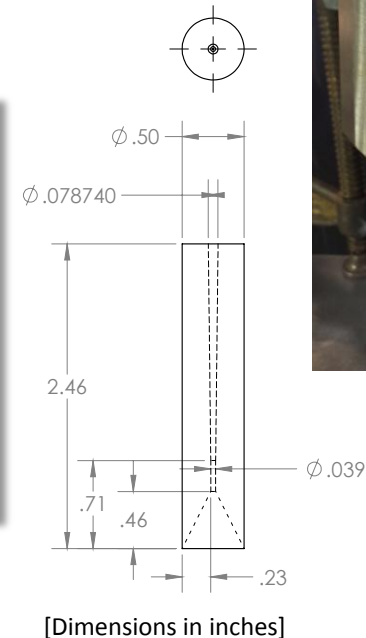




# Development for Internal Bores



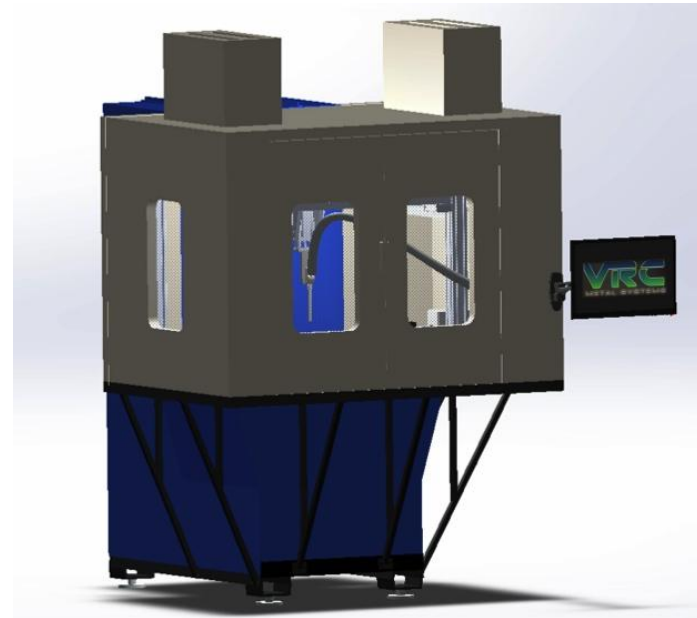
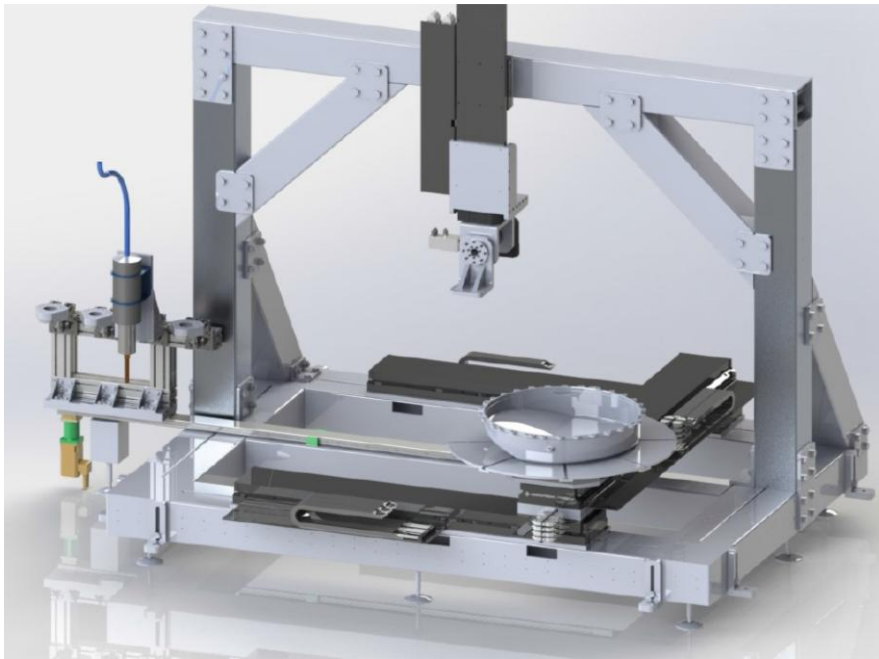
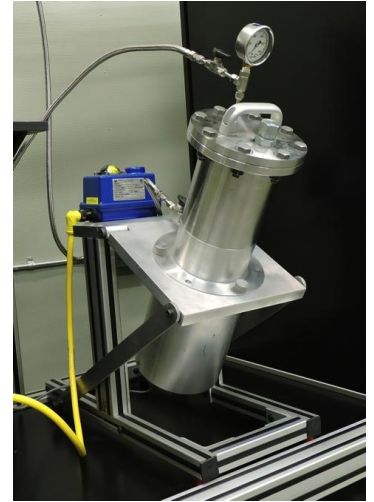
- Worked with ARL and MOOG to develop a repair process for a valve body internal bore.
  - Made a shortened nozzle (75 mm) with internal bore 45° gun
  - Turn table rotating at 60 rpm with 3-axis robot with



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# Other Equipment

- Powder Processing
- Motion Systems



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# Application Development

- **Lessons Learned**

1. Repair is a great ROI opportunity.
  - Many replaced for form/function defects not failure.
  - Minimal impact to finished part with repair.
2. Need to understand microstructures and properties.
3. Modeling is a valuable development tool.
4. Some applications will require custom equipment solutions
5. Requirements should be based on repair zone needs, not material spec minimums.

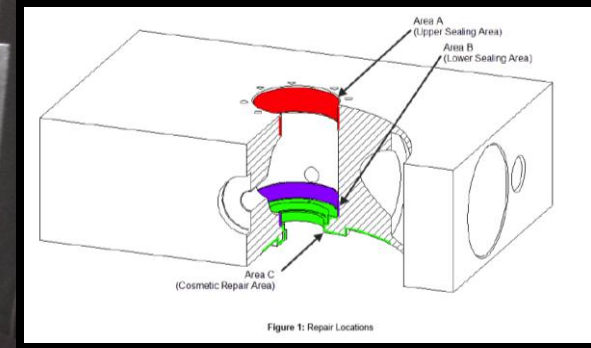
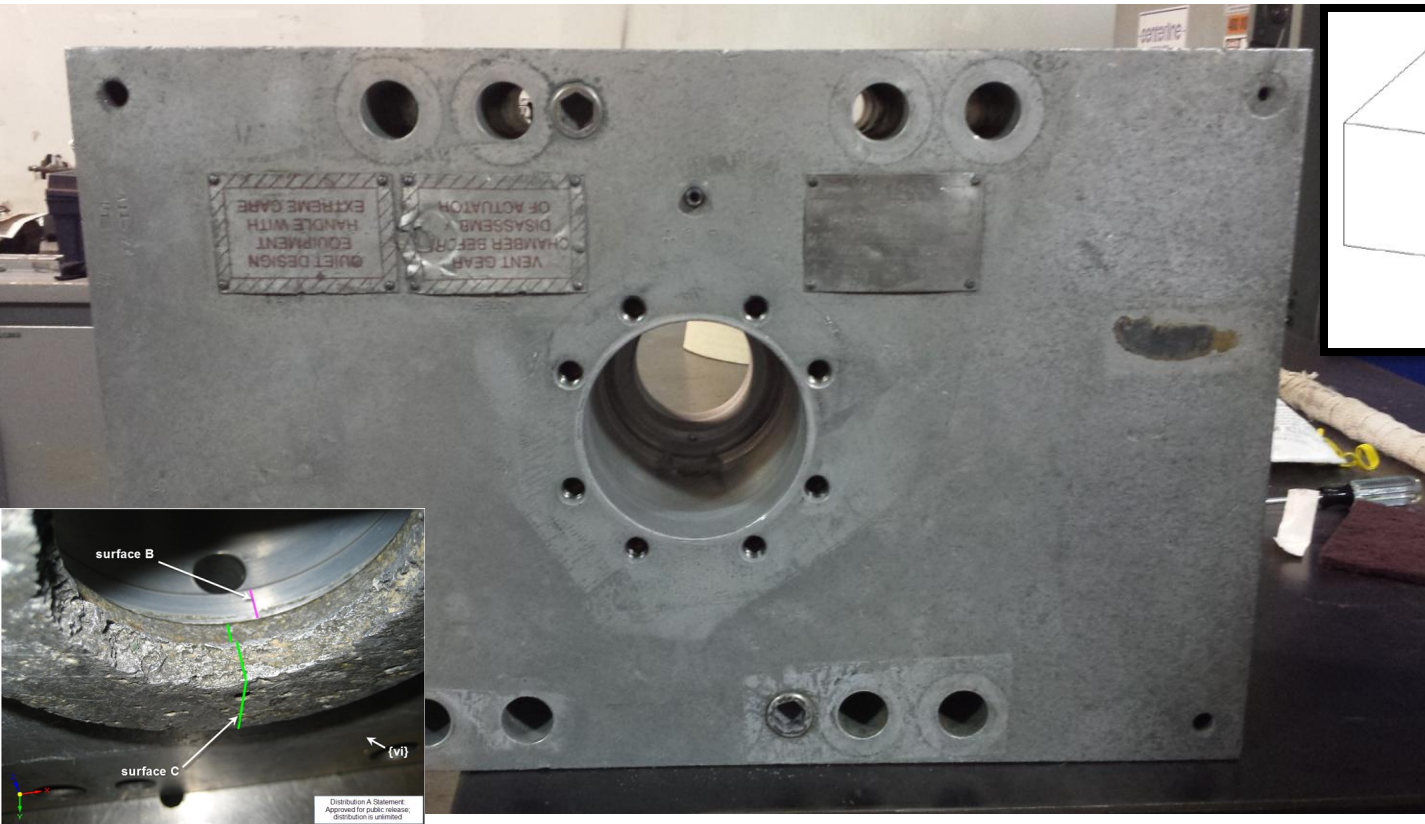
# Implications for Repair

- Ideal for parts that are heat sensitive
  - can avoid creating a heat-affected zone
- Powder microstructure is essentially preserved
- Some applications may require pre or post-heat treat
  - to achieve a desired microstructure in the deposited





# Corrosion / Sealing Surface Repair



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**VTRC**  
METAL SYSTEMS

**MA**  
Mid-America  
AVIATION

**MOOG**

**ARL**

# Mechanical Testing

## Requirements

1. Min. 10 ksi adhesion
2. <5% Porosity
3. Machinable

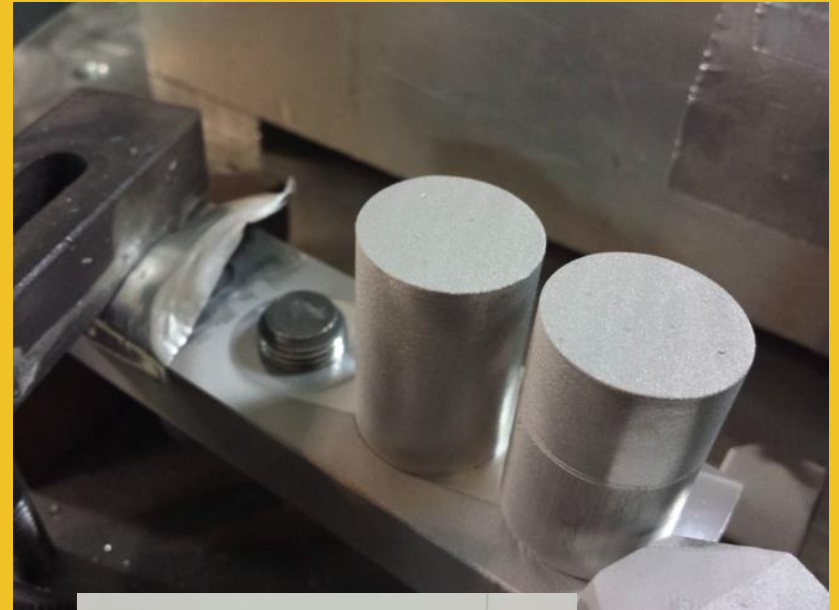
Average  
Porosity =  
2.9%  $\pm$

2.10%

Critical  
Surface  
Porosity <  
1%



**ASTM C633 – Adhesive Bond Test**  
✓ Avg. >10 ksi (glue failures)

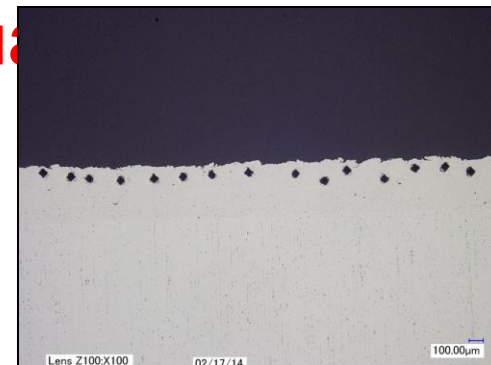


# Other Mechanical

- **ASTM E8 Tensile Strength**

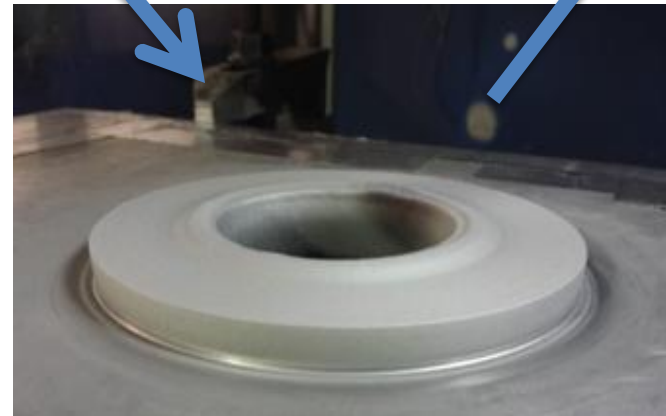
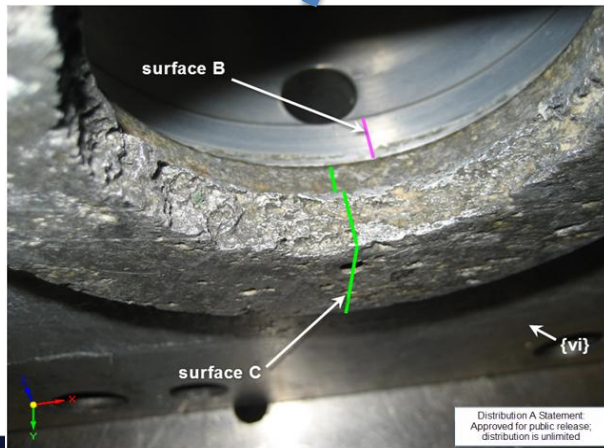
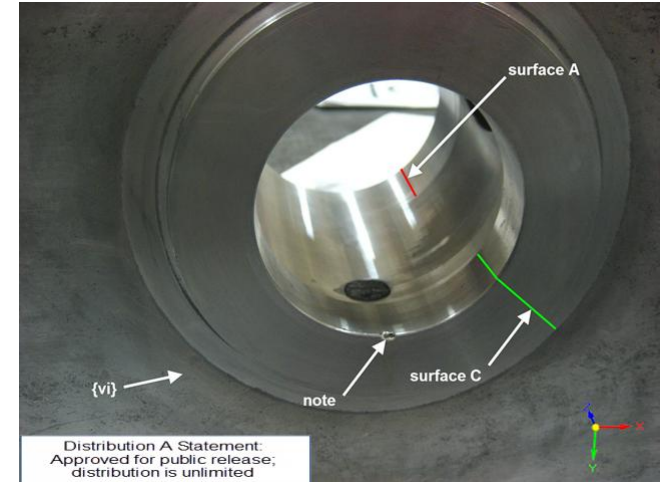
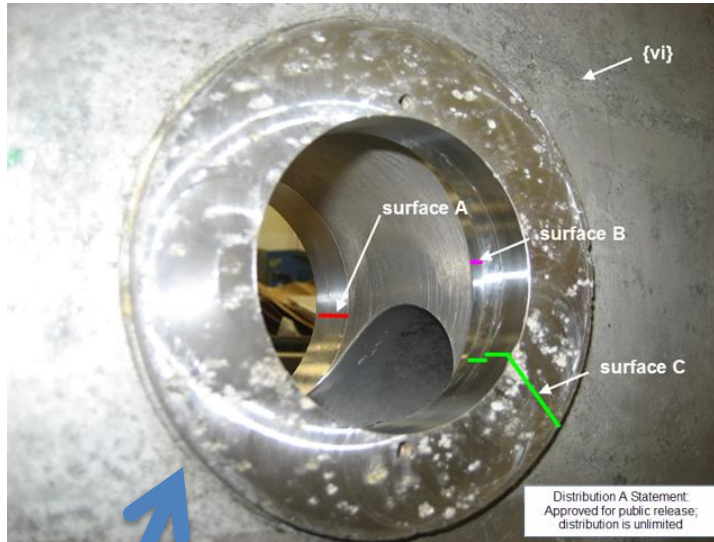
Sample #	UTS (MPa) [ksi]	% Elongation
1	272	2.91
2	251	3.02
<b>Average</b>	<b>261.5 [37.9]</b>	<b>2.97</b>

- On a 2<sup>nd</sup> set Puget Sound measured avg. = 247 MPa
- **Min tensile strength of the actual = 251 Mpa**
- Microhardness =  $87 \pm 3.3$  HV





# Repairing Non-Critical Corrosion





# Internal Bore Repair

Solid  
Maskin

g

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Note: Masks removed by machining,  
otherwise damage to cold spray can occur.

The Pursuit of Excellence

# Repair Application Example

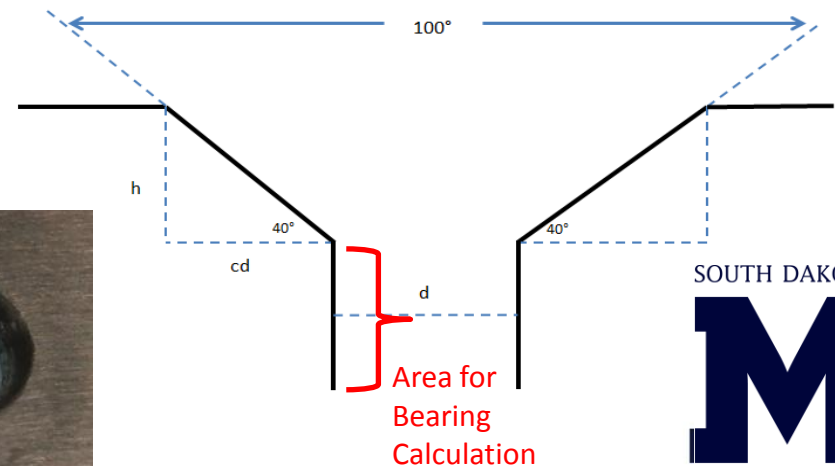
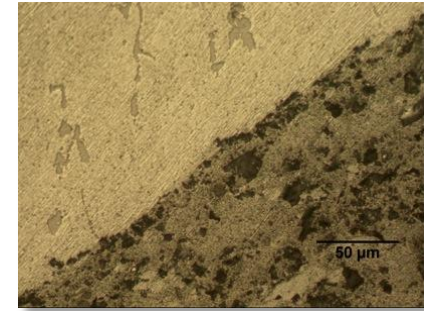
- **B1 Bomber Skin Panel Repair**
  - Wear at fastener holes
  - Replacement Cost >\$200K each (Fleet liability: \$50M)
  - Access panel not designed to be load carrying
  - Part lead time > 18 months



**A cold spray repair solution has been developed... ROI > 10:1**

# Mechanical Testing

- Realistic requirements developed with Tinker AFB cognizant engineer
- Fatigue
  - 500K Cycles At 15 ksi
- Three lug shear testing
  - (Avg. 5681 psi  $\pm$  729)
- **Static Guided lap shear**
  - Carried full Mil-HDBK fastener bearing yield load of 3400lbs.
  - Tested up to failure at 5600 lbs – **no delamination at failure**



SOUTH DAKOTA



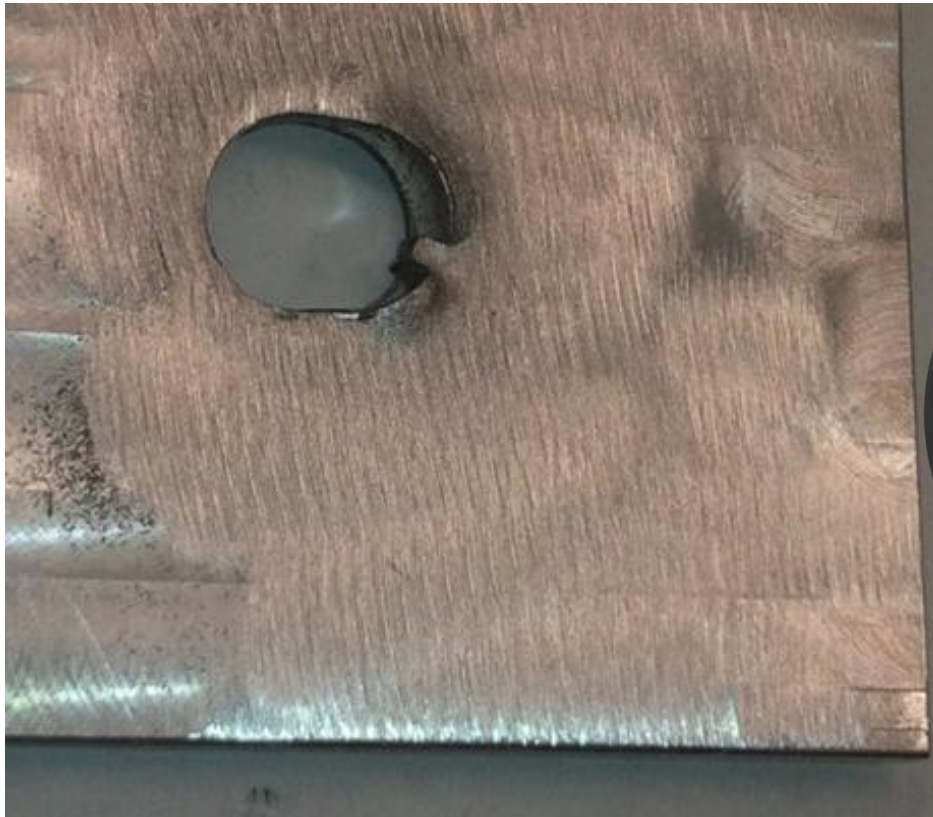
SCHOOL OF MINES  
& TECHNOLOGY

**No evidence of cold spray material failure observed up to full bearing**



# Failure Load Testing

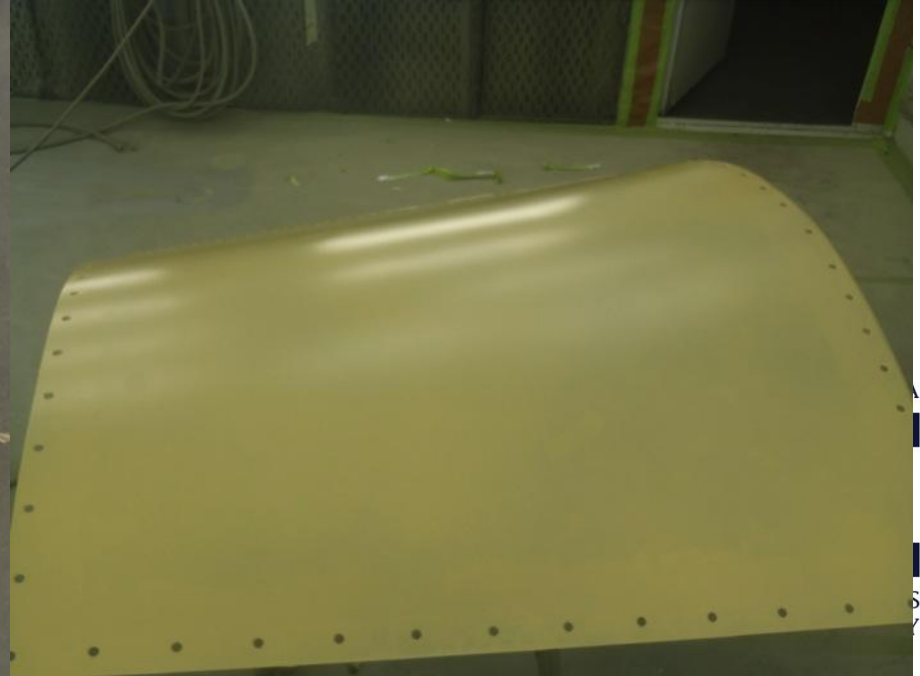
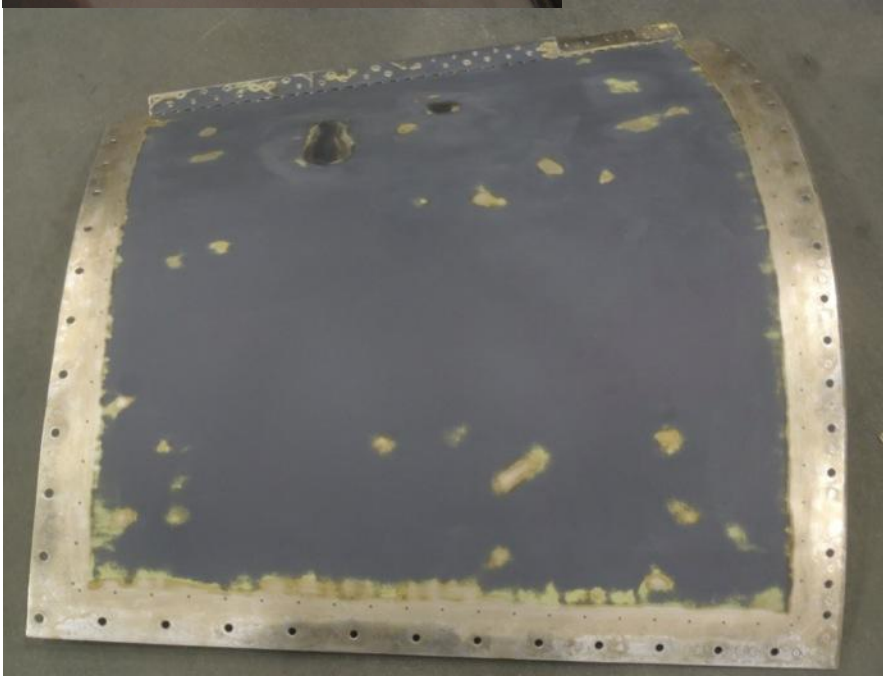
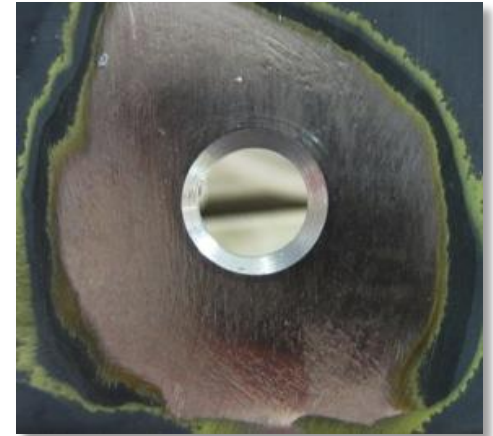
- Even tested up to failure at 5600lbs, the cold spray material did not separate from the coupon.





# Repaired Panel

Panel  
temperatures  
did not  
exceed 100°C.



# Fully Restored Panel vs. Legacy Repair



- *The repair is currently flying on a B1 under an ETAR (August 2012)*
  - Still no sign of degradation or repair failure
- Total development time (with Tinker AFB support): 250 days
- Repair time: 2 weeks --- Savings >\$200K + Availability

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# Thank you for your attention!

- **Dr. Christian Widener**

- Director/ Associate Professor  
Arbegast Materials Processing Lab  
South Dakota School of Mines & Technology  
Ph. 605-394-6924

Email: [christian.widener@sdsmt.edu](mailto:christian.widener@sdsmt.edu)

<http://www.sdsmt.edu/amp>

- Chief Technical Officer  
VRC Metal Systems

<http://www.vrcmetalsystems.com>

