



WPI

Worcester Polytechnic Institute



U.S. Army Research Laboratory
Contract #W911NF-10-2-0098

Through-Process Modeling of Cold Spray

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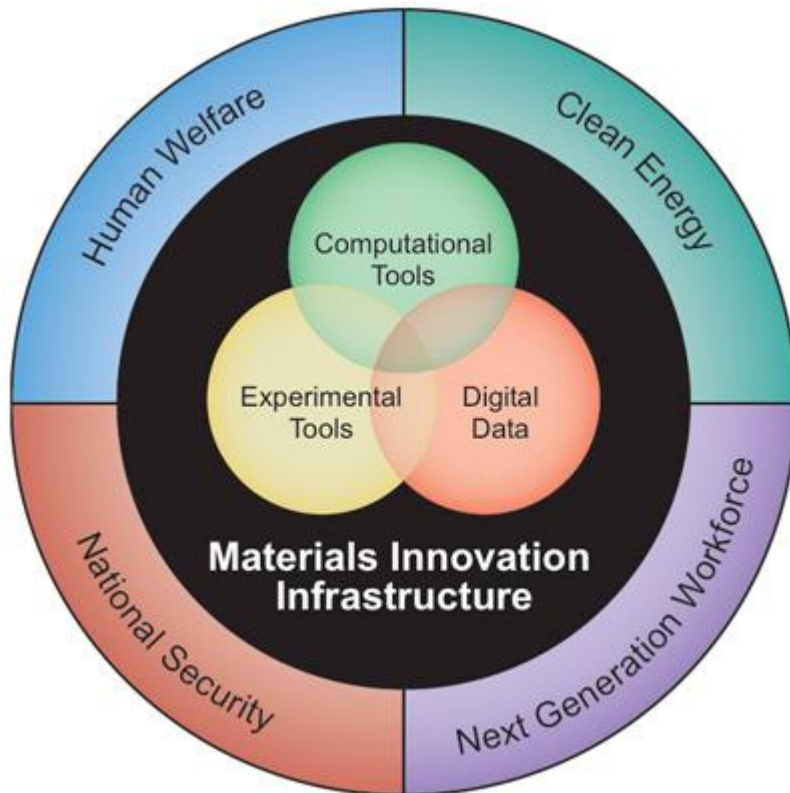
- Project Motivation
- Project Approach
 - Models
 - Characterization
- Summary

Materials Genome Initiative



"To discover, develop, and deploy new materials twice as fast..."

- President Obama, 2011

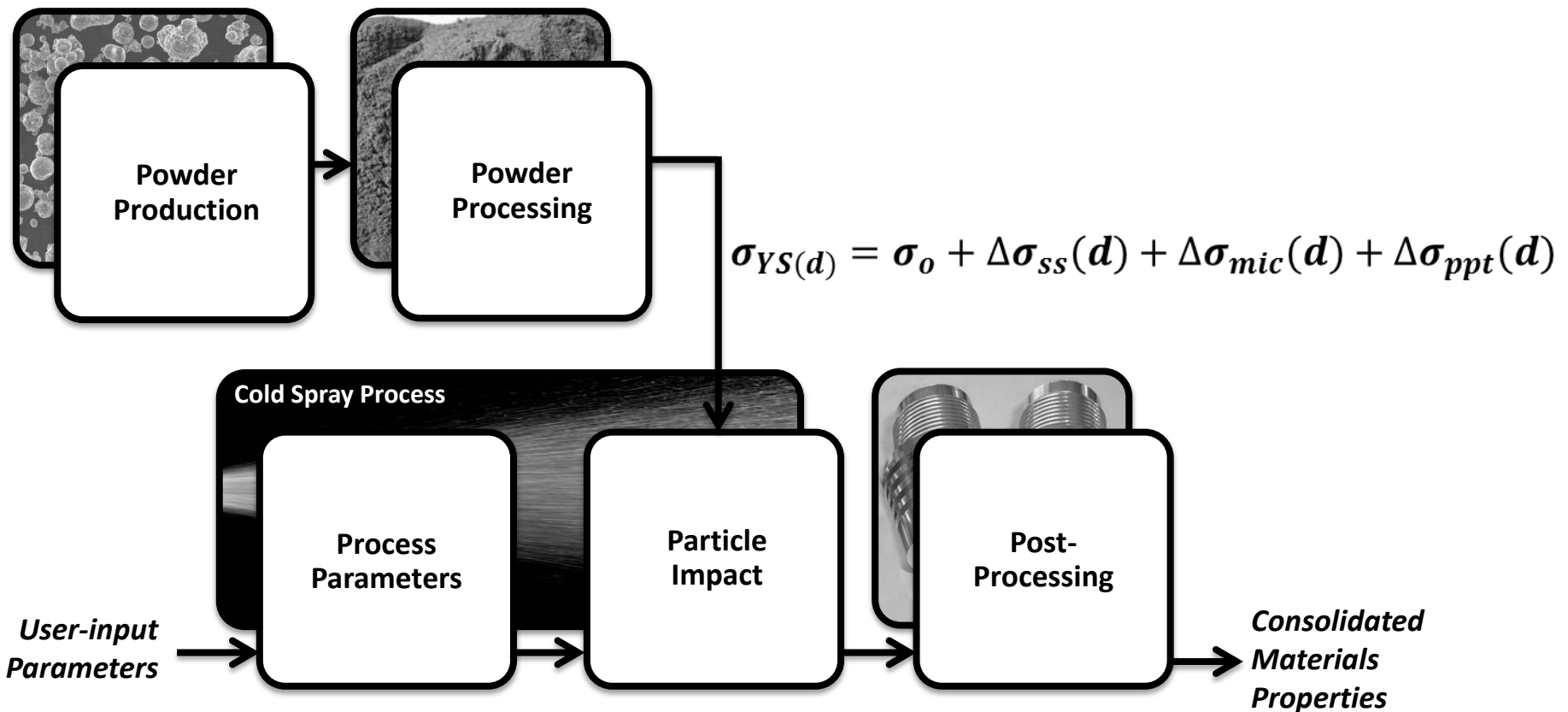
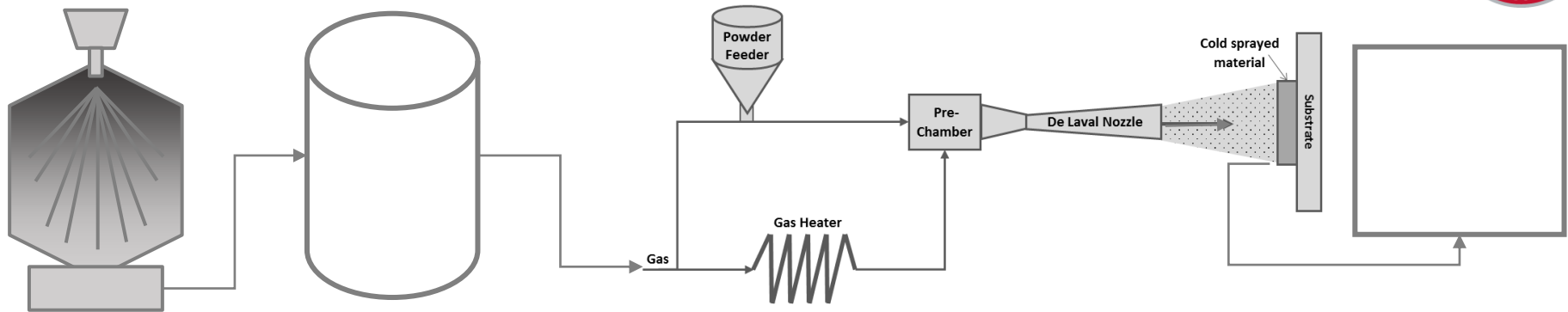


Meeting Societal Needs

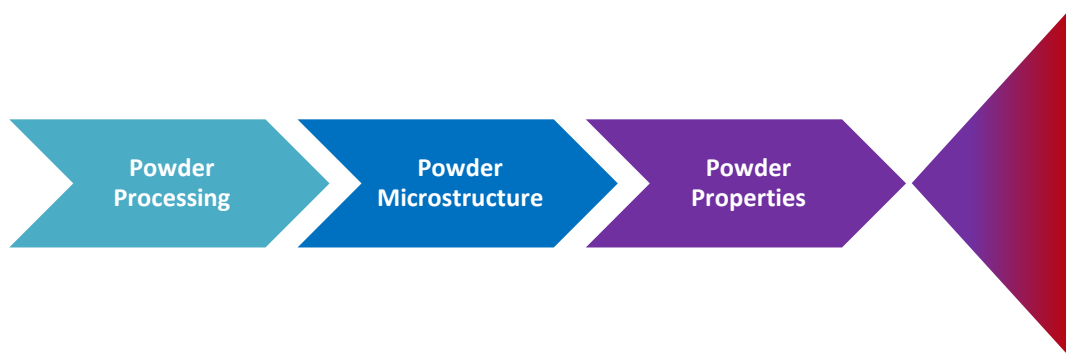
"The **lengthy time frame for materials to move from discovery to market** is due in part to the continued reliance of materials research and development programs on **scientific intuition** and **trial and error experimentation**. Much of the design and testing of materials is currently performed through time-consuming and repetitive experiment and characterization loops. Some of these experiments could potentially **be performed virtually with powerful and accurate computational tools**, but that level of accuracy in such simulations does not yet exist."

Materials Genome Initiative (2011)

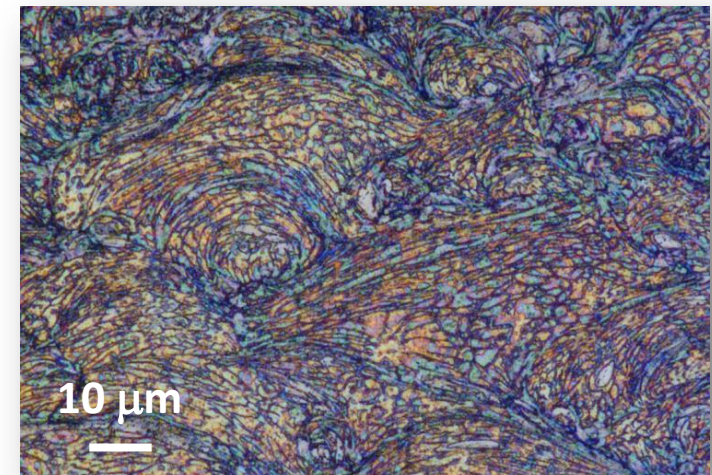
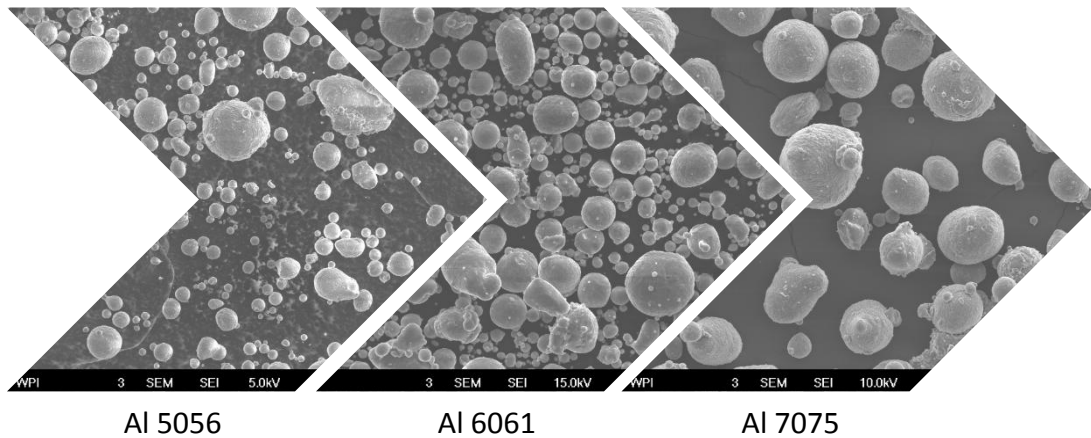
Through-Process Model



Powder Significance



Consolidated Material Properties



Additive Yield Strength Model



Function of: →

- Alloy composition,
- Powder particle size,
- T, t of heat treatment

Solid Solution Strengthening

$$\Delta\sigma_{ss} = \sum_i (G\varepsilon_s^{3/2} c^{1/2}) / 700$$

Substitutional Solid-Solution

Grain Size/Microstructural Influence

$$\Delta\sigma_{mic}(d) = k_{gs} \lambda^{-0.5}$$

Hall-Petch Behavior

Precipitation Strengthening

$$\Delta\sigma_{ppt} = \sum_i [\sigma_{Coherency,i} + \sigma_{Modulus,i} + \sigma_{Chemical,i} + \sigma_{Order,i}]$$

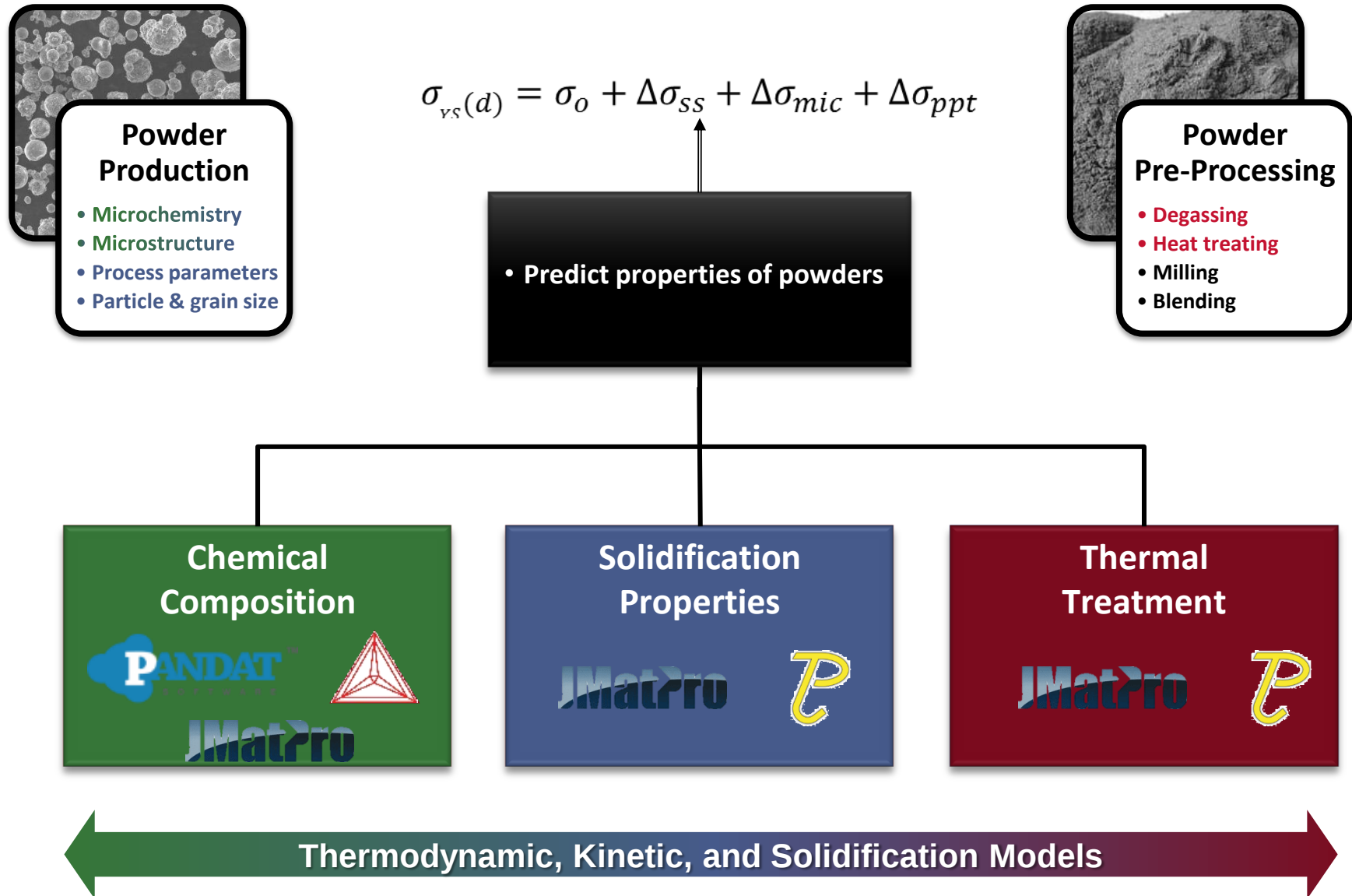
$$\Delta\sigma_{Coherency,i} = 7\varepsilon_{coh,i}^{3/2} G \left(\frac{rf}{b} \right)^{1/2}$$

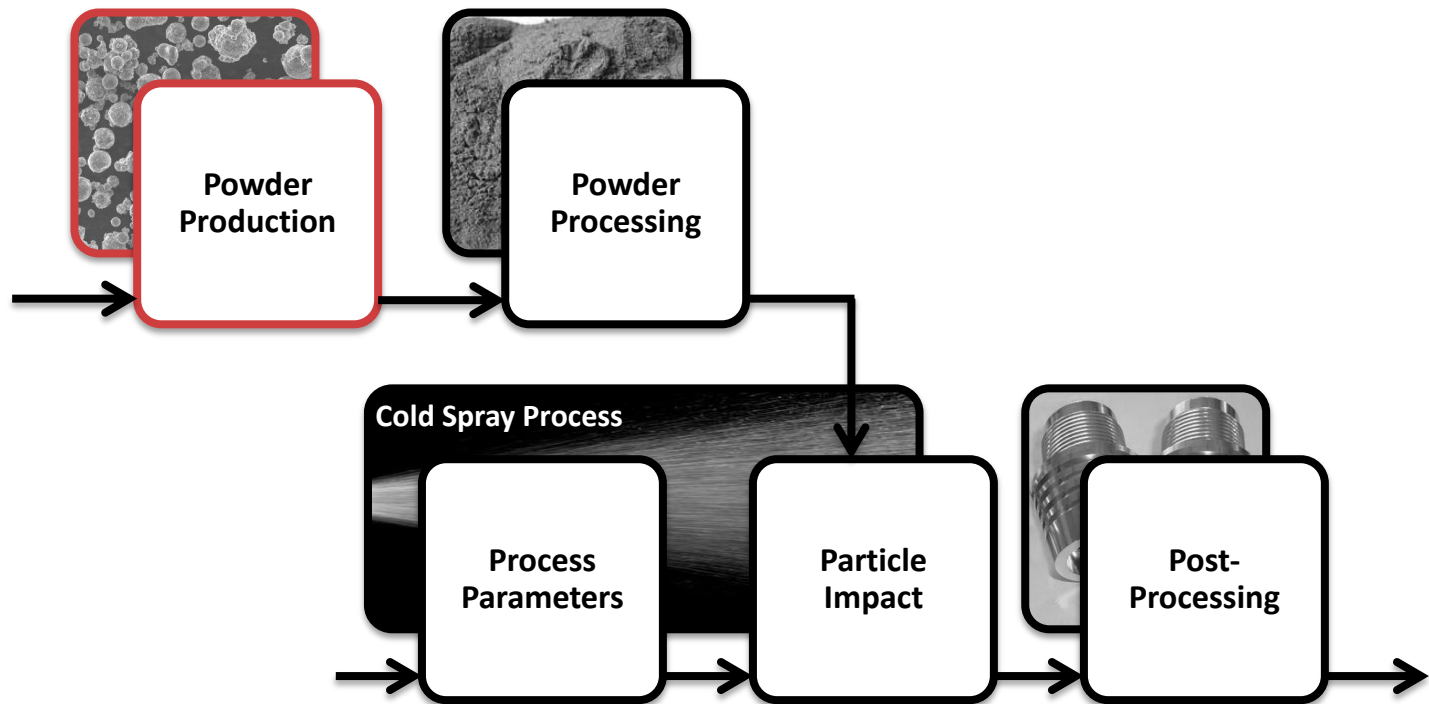
$$\Delta\sigma_{Modulus,i} = 0.01\varepsilon_{Gp,i}^{3/2} G \left(\frac{rf}{b} \right)^{1/2}$$

$$\Delta\sigma_{Chemical,i} = 2\varepsilon_{Ch,i}^{3/2} G \left(\frac{rf}{b} \right)^{1/2}$$

$$\Delta\sigma_{Order,i} = 0.7G \left[\varepsilon_{Ord,i}^{3/2} \left(\frac{rf}{b} \right)^{1/2} - 0.7 \right] \varepsilon_{Ord,i}$$

Modeling Approach





Powder Production

Thermodynamic & Solidification Models

Characterization: SEM & EDS

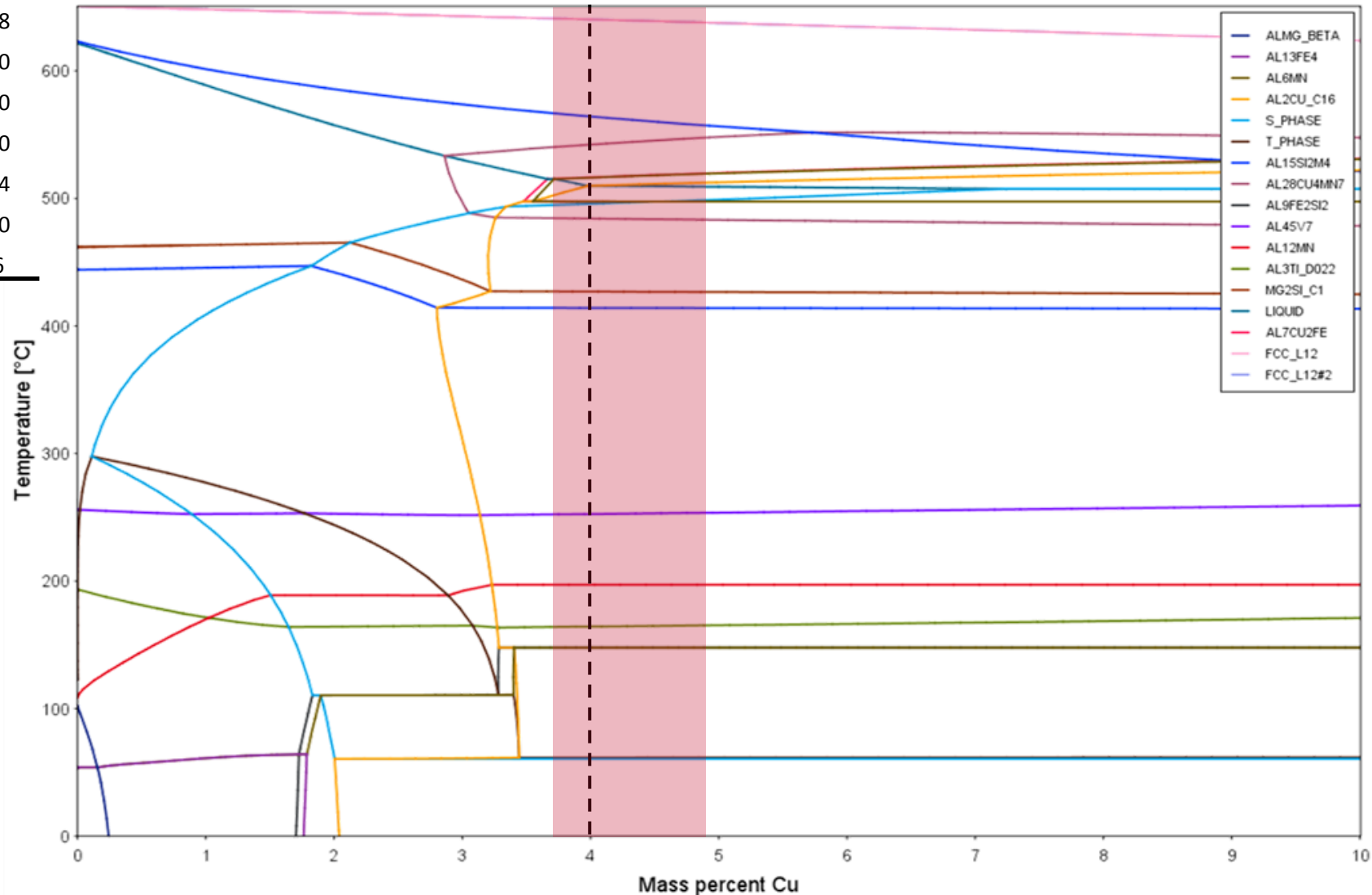
Thermodynamic Modeling



wt% Al 2024

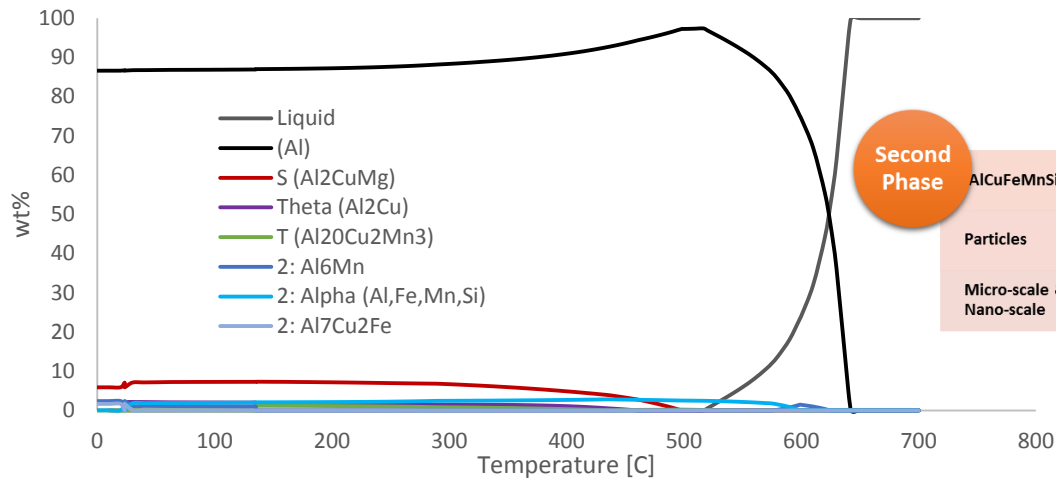
Cr	0.006
Cu	4.000
Fe	0.078
Mg	1.500
Mn	0.610
Ti	0.100
Zn	0.014
Si	0.130
Al	93.6

Al 2024



Al 2024

Thermodynamic Modeling



Second Phase

AlCuFeMnSi

Particles

Micro-scale & Nano-scale

S-Phase

Al2CuMg

Precipitates

Micro-scale

θ-Phase

Al2Cu

Precipitates

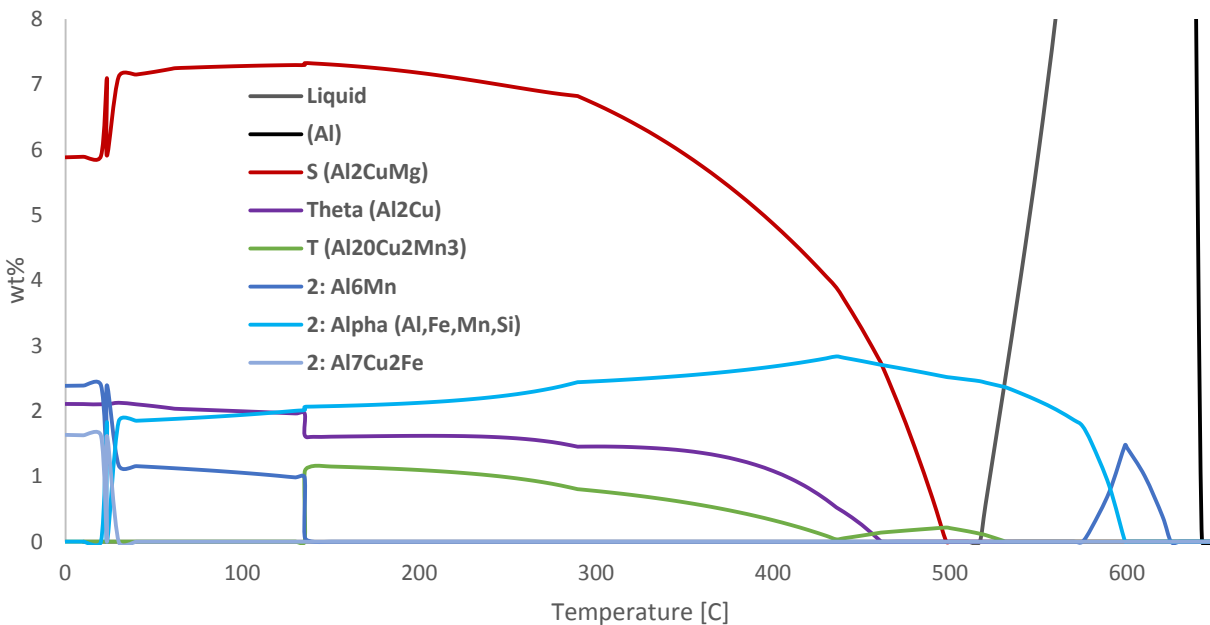
Micro-scale

T-Phase

Al20Cu2Mn3

Dispersoids

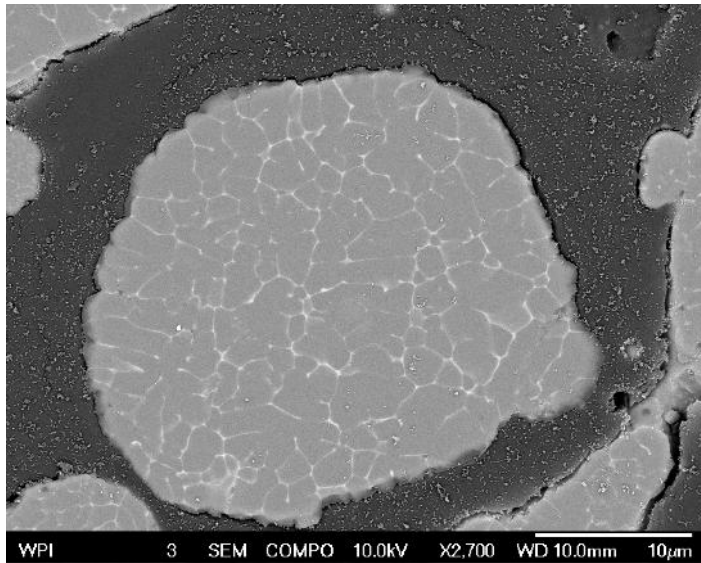
Nano-scale



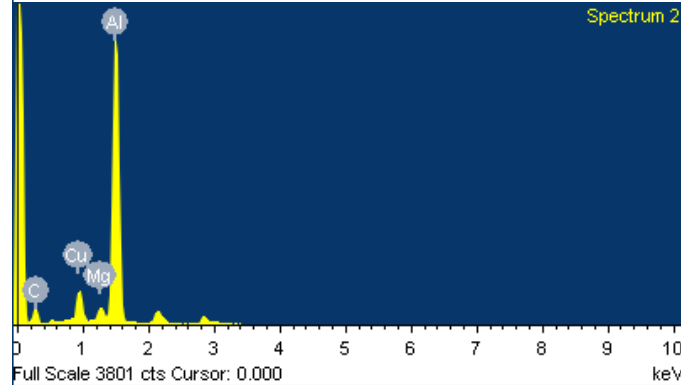
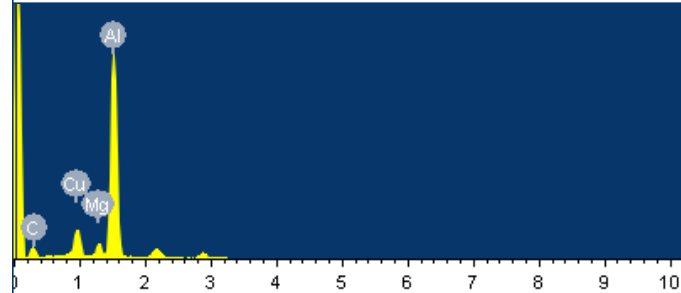
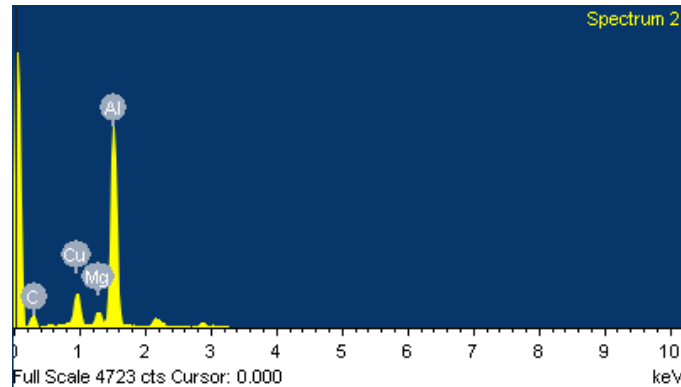
$$\Delta\tau_{Coherency,i} = 7\varepsilon_{coh,i}^{3/2} G \left(\frac{rf}{b} \right)^{1/2}$$

$$\sigma_{YS(d)} = \sigma_o + \Delta\sigma_{ss}(d) + \Delta\sigma_{mic}(d) + \Delta\sigma_{ppt}(d)$$

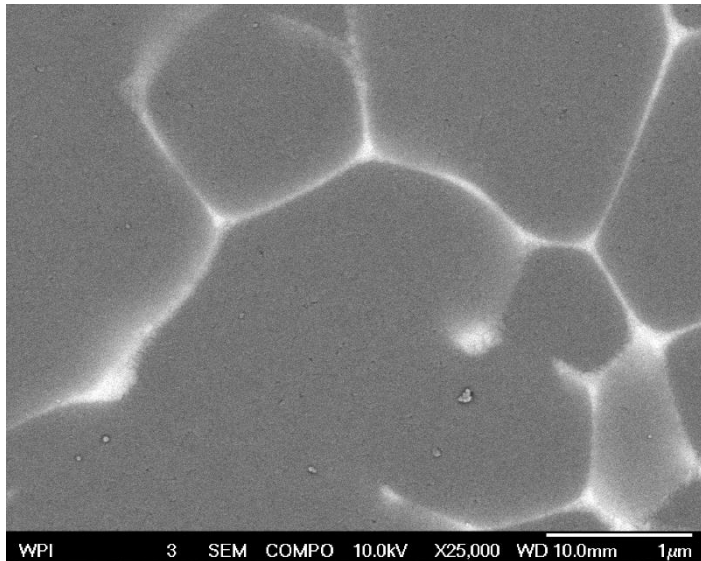
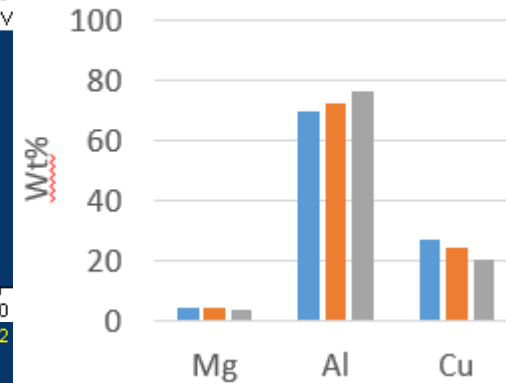
Thermodynamic Characterization – SEM/EDS



S-Phase & θ

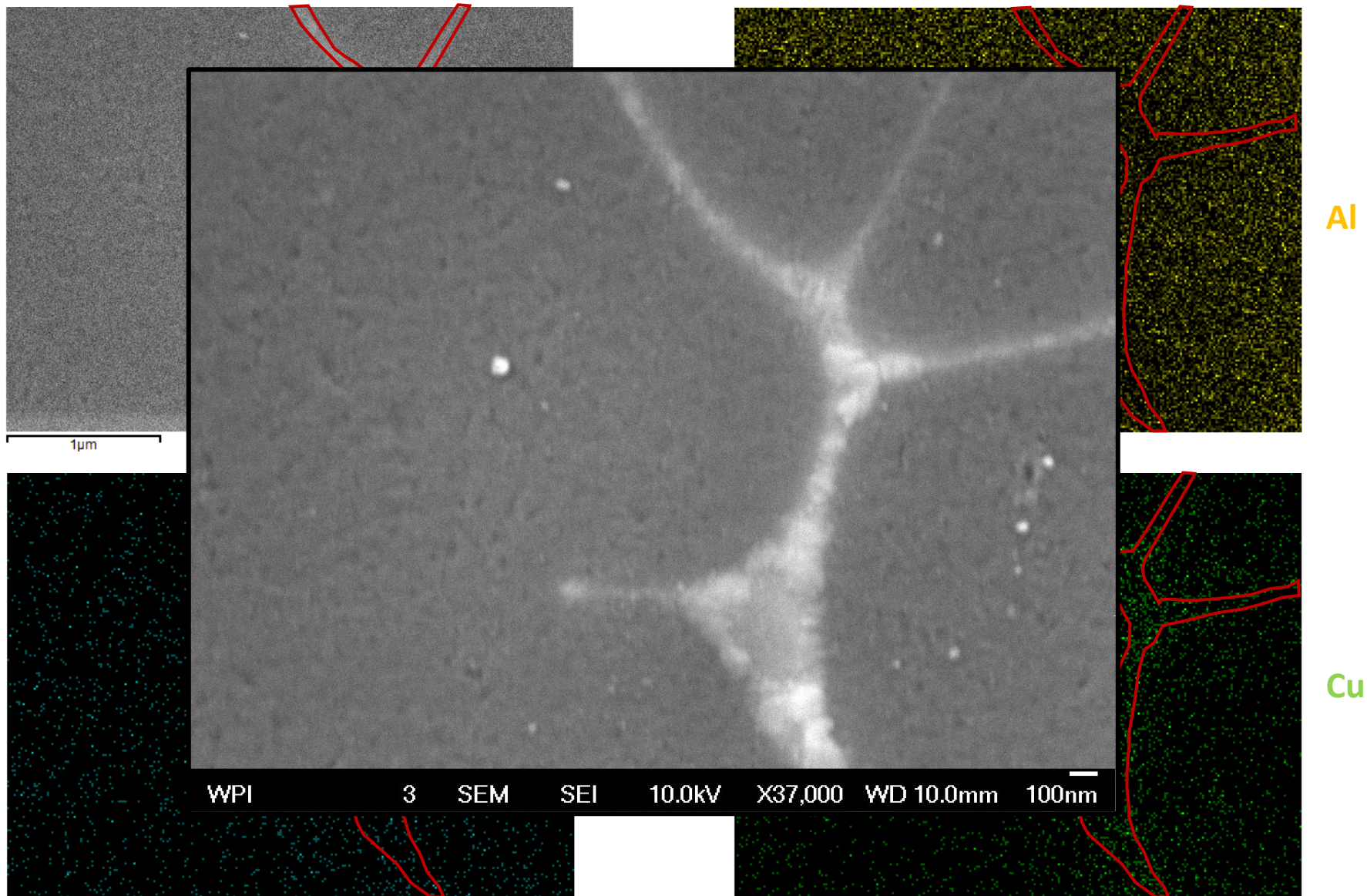


White Boundary



$$\sigma_{YS(d)} = \sigma_o + \Delta\sigma_{ss}(d) + \Delta\sigma_{mic}(d) + \Delta\sigma_{ppt}(d)$$

Thermodynamic Characterization – EDS Map



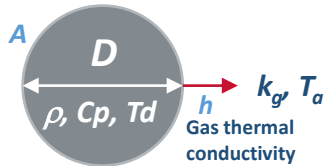
Al

Cu

Solidification Model



Heat Transfer Model Gas Atomization Process



Gas Atomization: Newtonian Heat Flow

- Heat transfer from droplet: forced convection
- Radiational cooling: neglected
- Heat conduction (w/in droplet): neglected (small size – Biot number < 0.1)

Heat balance,

$$-V \cdot \rho \cdot C_p \cdot \frac{dT_d}{dt} = h \cdot A \cdot (T_d - T_f) + \sigma \epsilon (T_d^4 - T_f^4)$$

$$h = \frac{k_g}{d} (2.0 + 0.6 \sqrt{R_e} \cdot \sqrt[3]{Pr})^2$$

$$R_e = \frac{U \cdot \rho_g \cdot d}{\mu_g}$$

$$Pr = (C_g \mu_g / k_g)$$

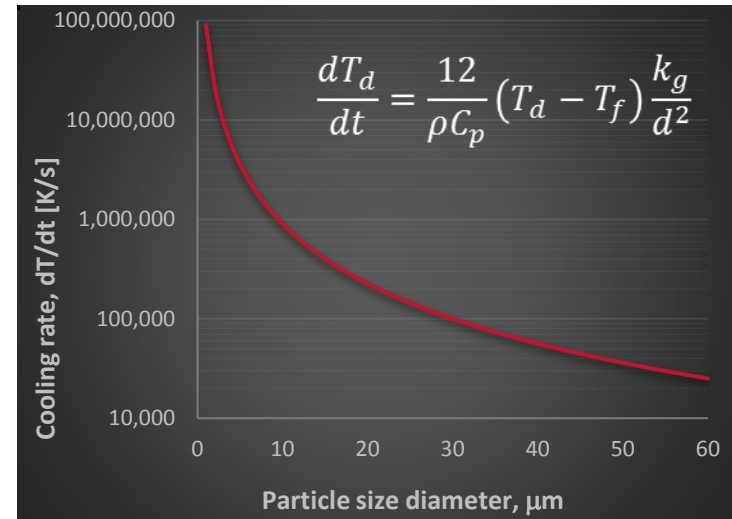
$$\left| \frac{dT_d}{dt} \right| = \frac{6}{\rho \cdot C_p} \cdot (T_d - T_f) \cdot \left(\frac{2.0 k_g}{d^2} + 0.6 \frac{k_g}{d} \sqrt{\frac{\rho_g}{\mu_g d}} \cdot \sqrt[3]{Pr} \right)$$

$$\left| \frac{dT_d}{dt} \right| = \frac{12}{\rho \cdot C_p} \cdot (T_d - T_f) \cdot \frac{k_g}{d^2}$$

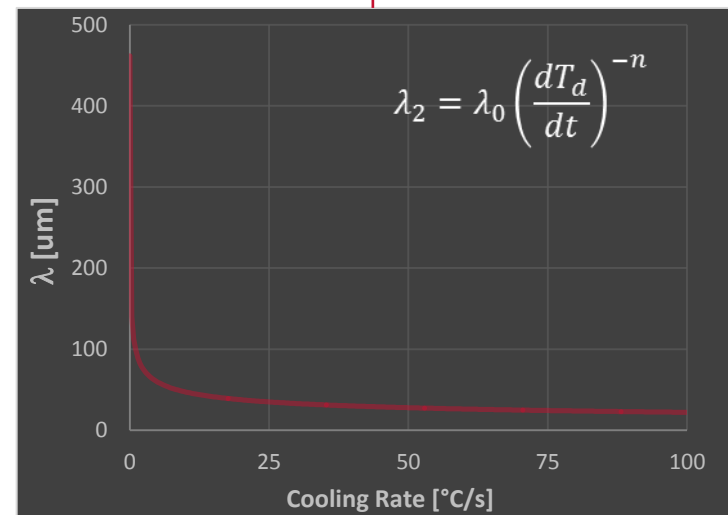
Thermophysical Properties of Al 6061¹

Ar Atomizing Gas		Molten Droplet		
T _f	K _g	ρ	C _p	T _d
[K]	[W/(mK)]	[kg/m ³]	[J/(kgK)]	[K]
300	1.79E-02	2380	1170	1473

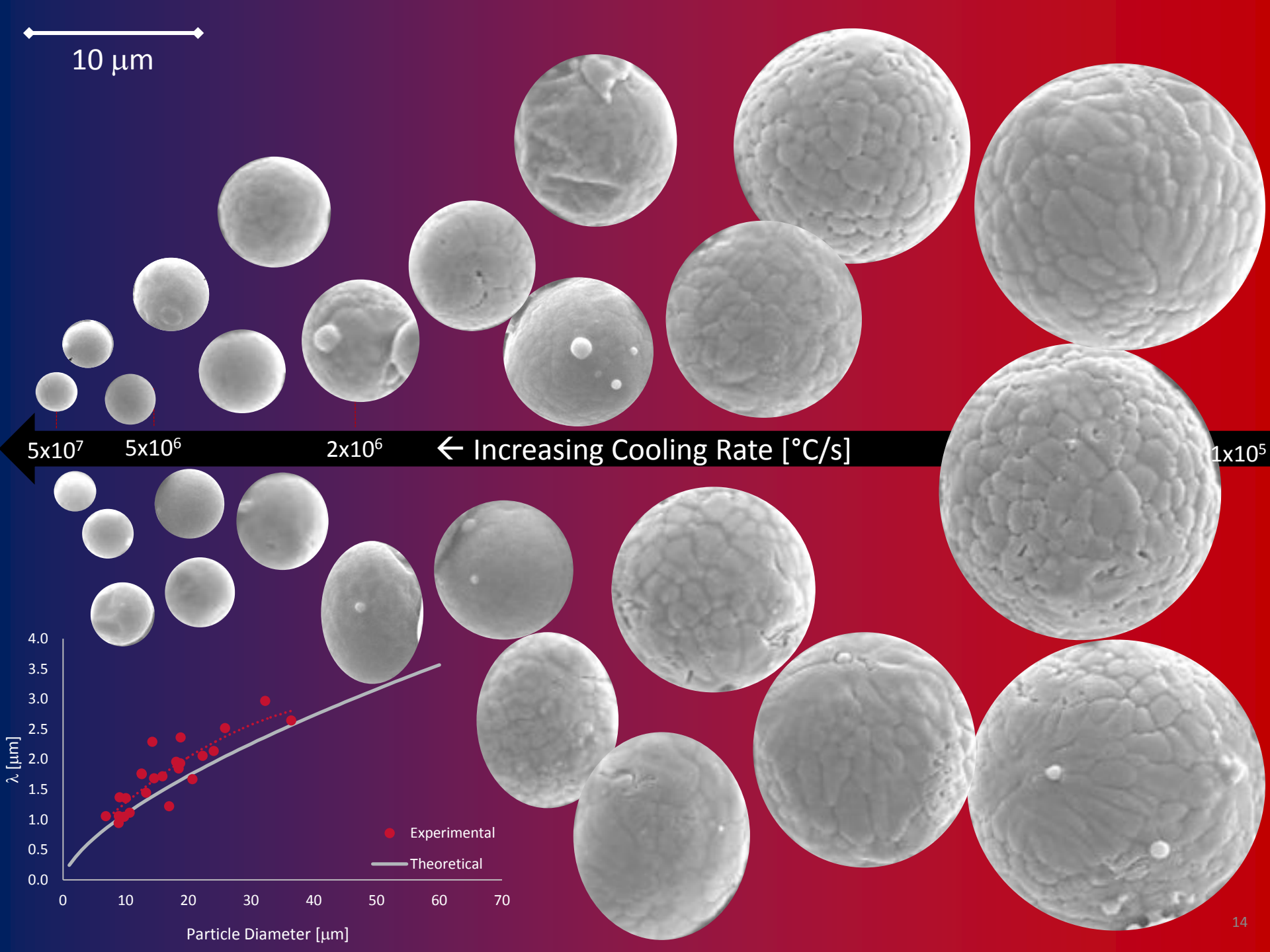
$$\sigma_{YS(d)} = \sigma_o + \Delta\sigma_{ss}(d) + \Delta\sigma_{mic}(d) + \Delta\sigma_{ppt}(d)$$



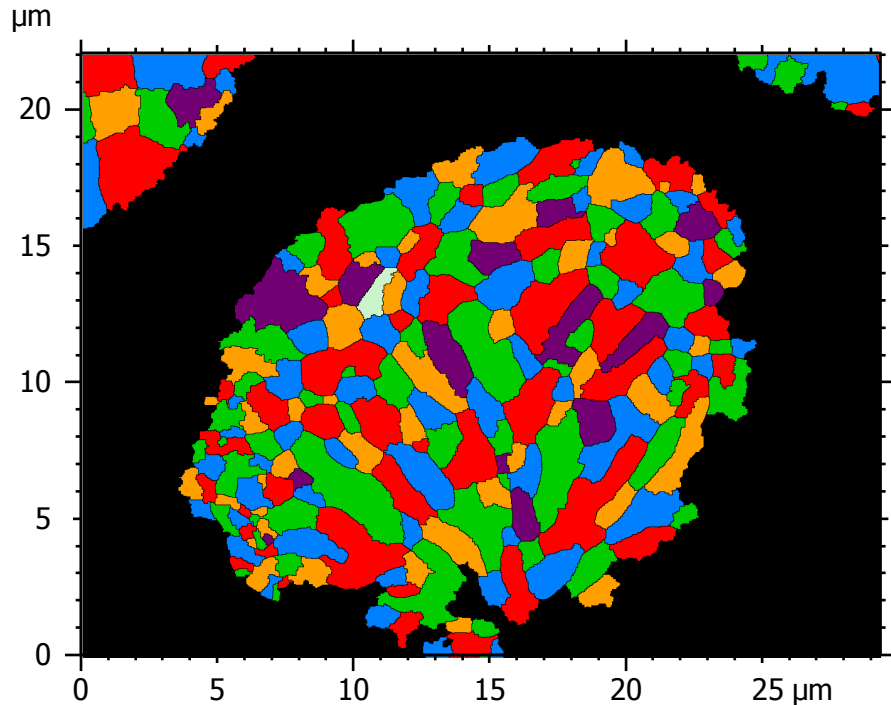
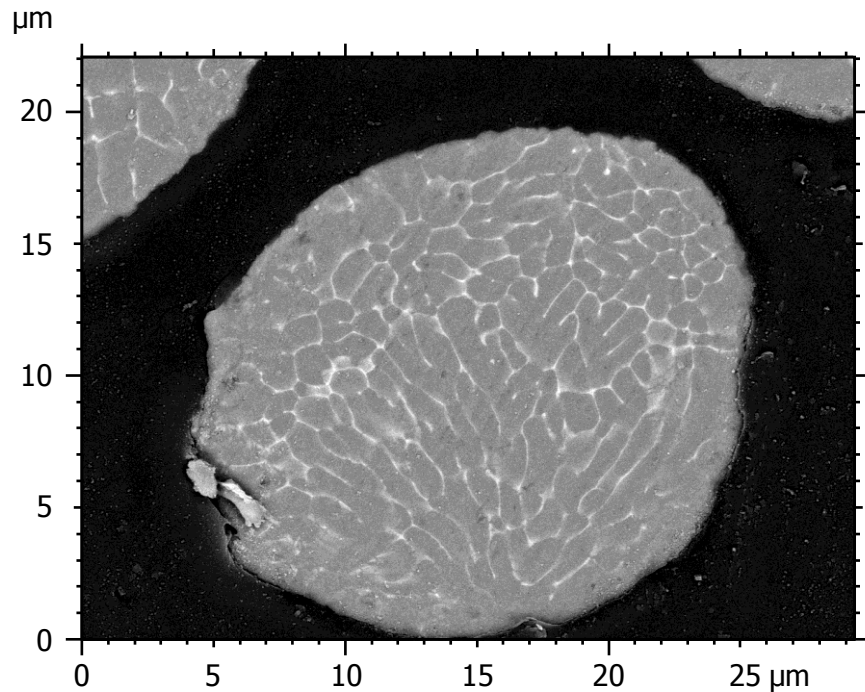
$$\lambda = \lambda_0 \left(\frac{12}{\rho C_p} (T_d - T_f) \frac{k_g}{d^2} \right)^{-n}$$



10 μm



Grain Size Characterization

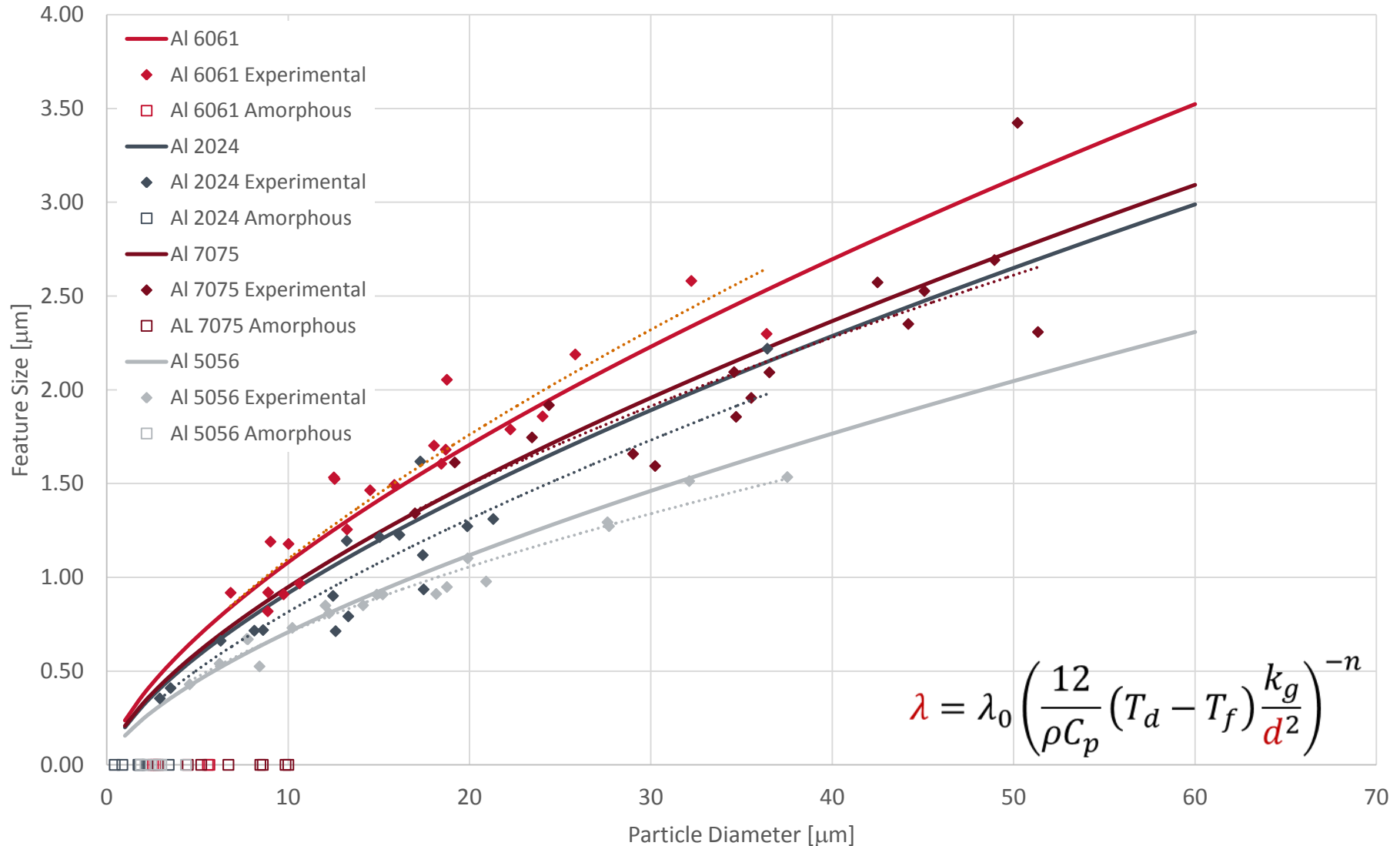


Statistics over all grains - Separated / merged				
Global information		Value		
Number of grains		227		
Total area occupied by the grains		281 μm² (43.4%)		
Density of grains		0.351 Grains/μm²		
Grain parameters		Unit	Mean	Std dev
Area		μm²	1.24	1.21
Perimeter		nm	5277	3007

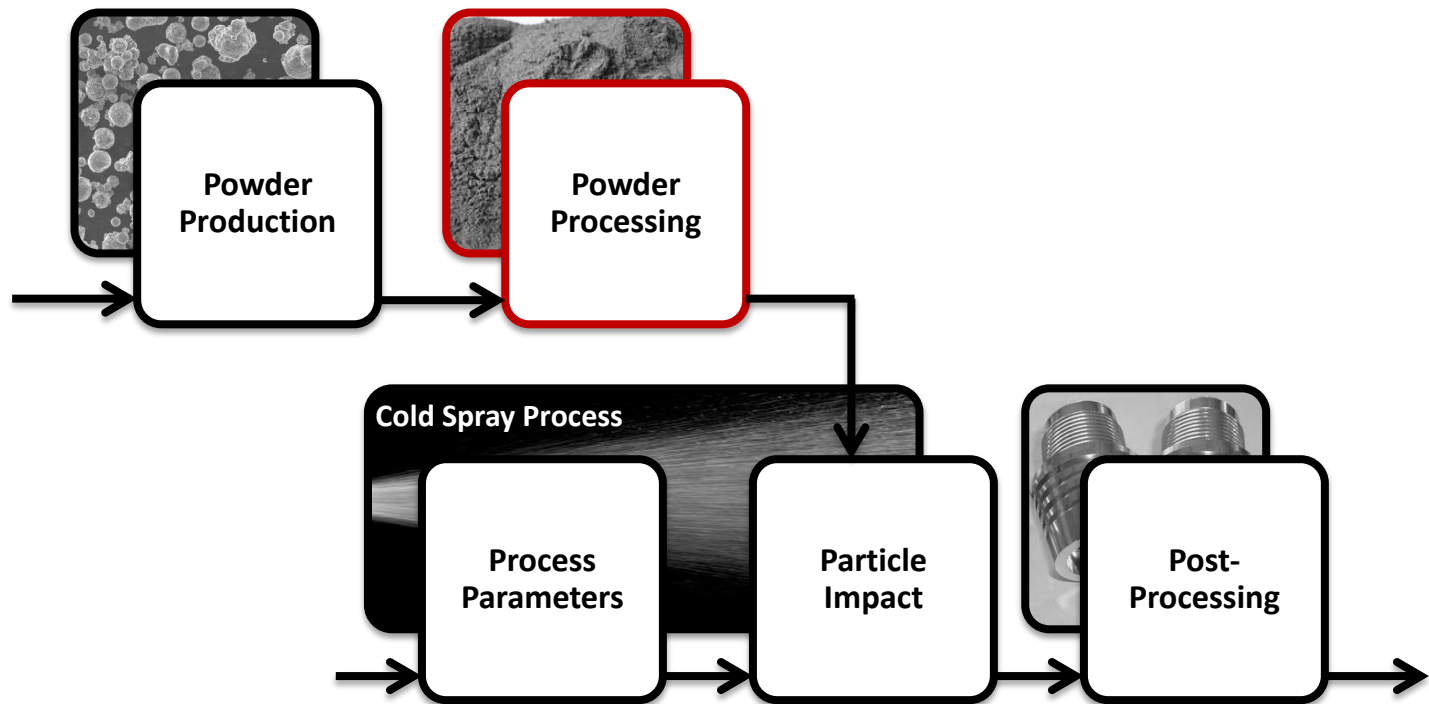
**Mountains®
by Digital Surf**

$$\sigma_{YS(d)} = \sigma_o + \Delta\sigma_{ss}(d) + \Delta\sigma_{mic}(d) + \Delta\sigma_{ppt}(d)$$

Grain Size Variation with Alloy



$$\sigma_{YS(d)} = \sigma_o + \Delta\sigma_{ss}(d) + \Delta\sigma_{mic}(d) + \Delta\sigma_{ppt}(d)$$



Powder Processing

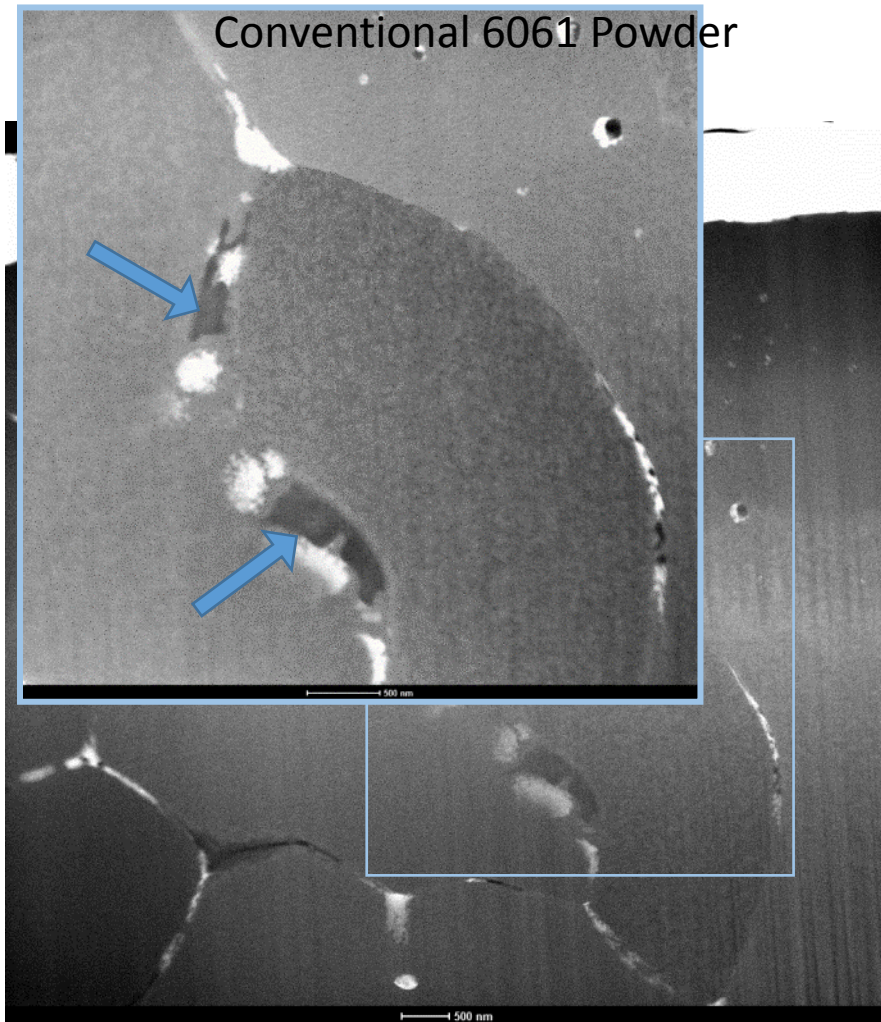
Kinetic Modeling: TTT, CCT

Characterization: STEM

Kinetic Modeling Characterization: STEM

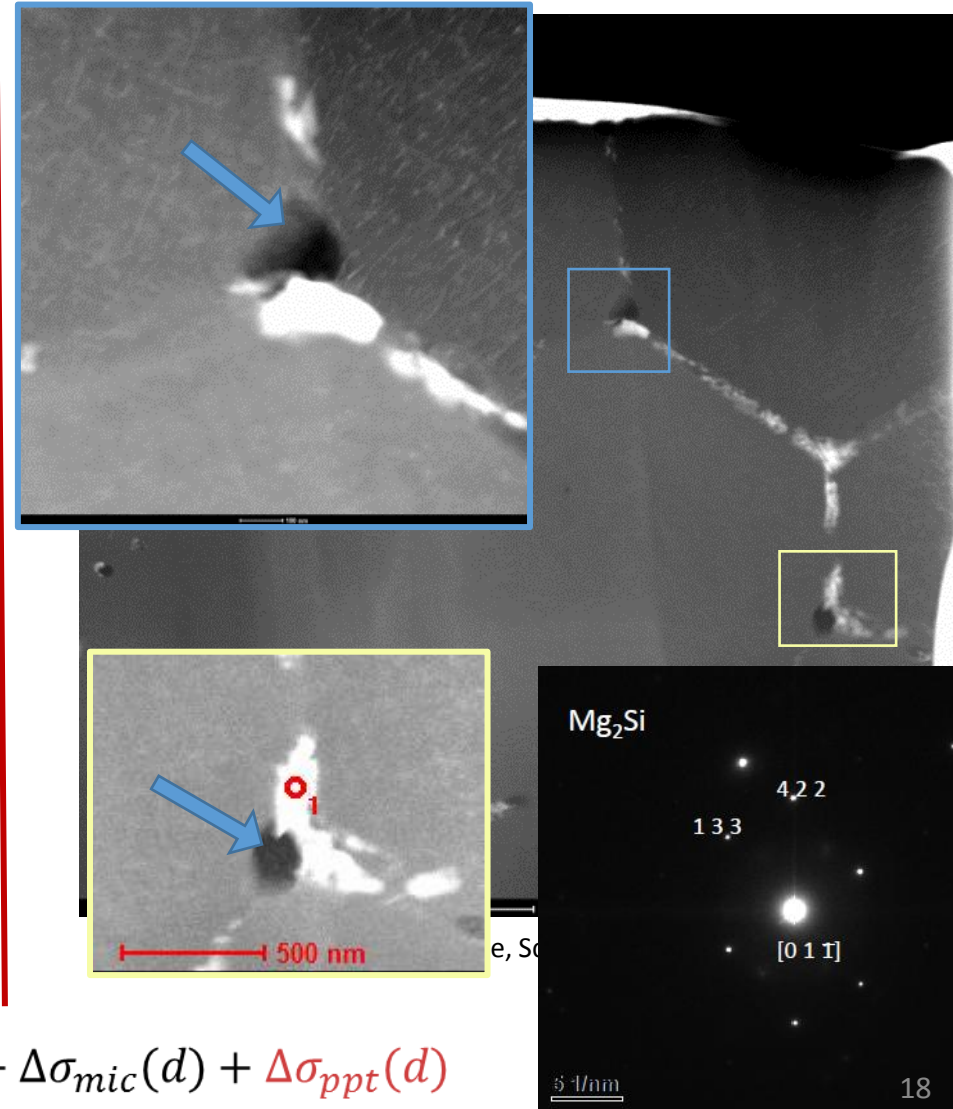


Conventional 6061 Powder



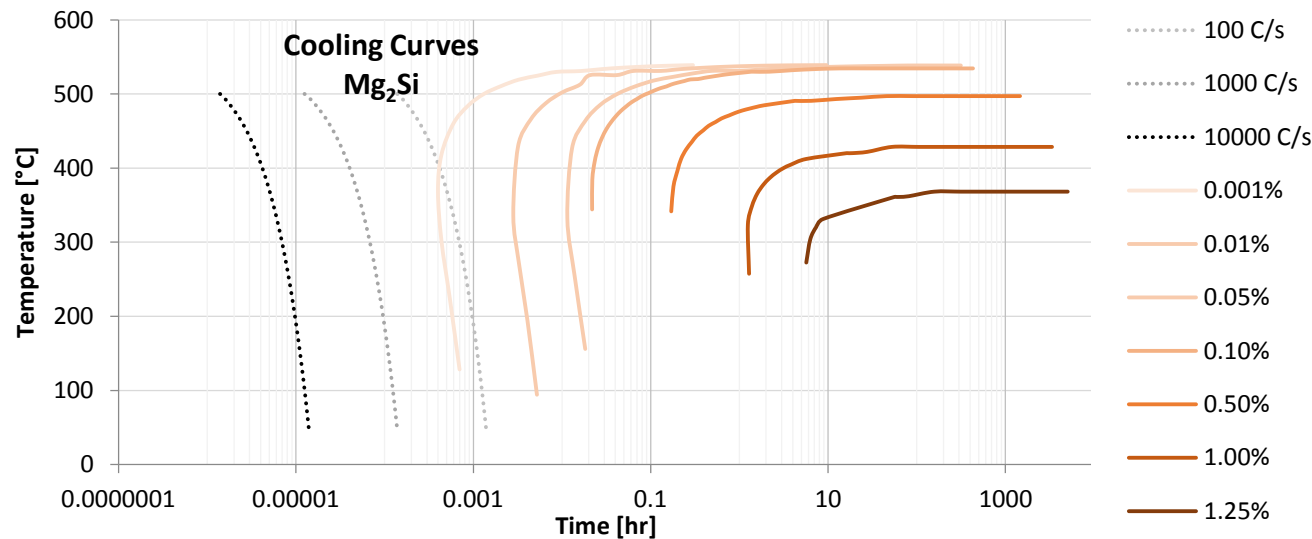
STEM DF Image, Scale Bar 500nm

Degassed 6061 Powder



$$\sigma_{YS(d)} = \sigma_o + \Delta\sigma_{ss}(d) + \Delta\sigma_{mic}(d) + \Delta\sigma_{ppt}(d)$$

Kinetic Modeling: CCT Diagram



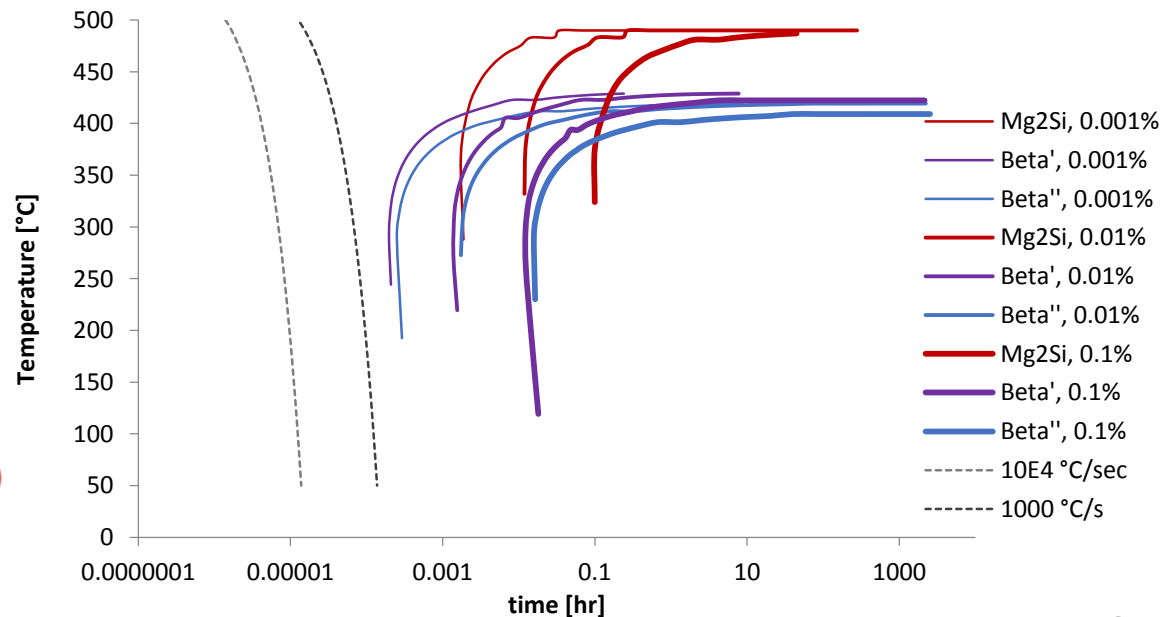
Gas atomization
cooling rates:
~10⁴-10⁵ °C/s

Metastable Mg₂Si Phases

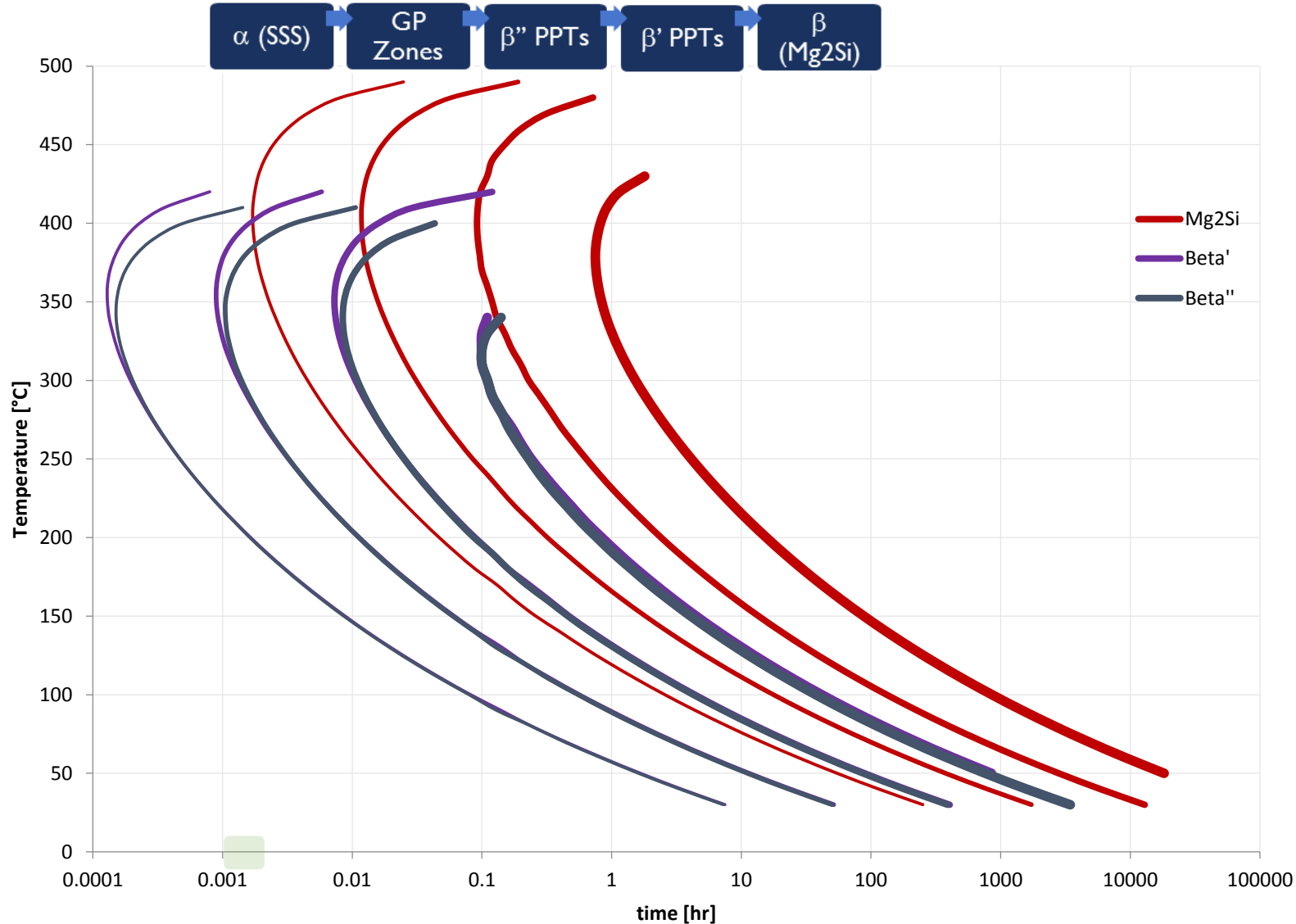


$$\Delta\tau_{Coherency,i} = 7\varepsilon_{coh,i}^{3/2} G \left(\frac{rf}{b} \right)^{1/2}$$

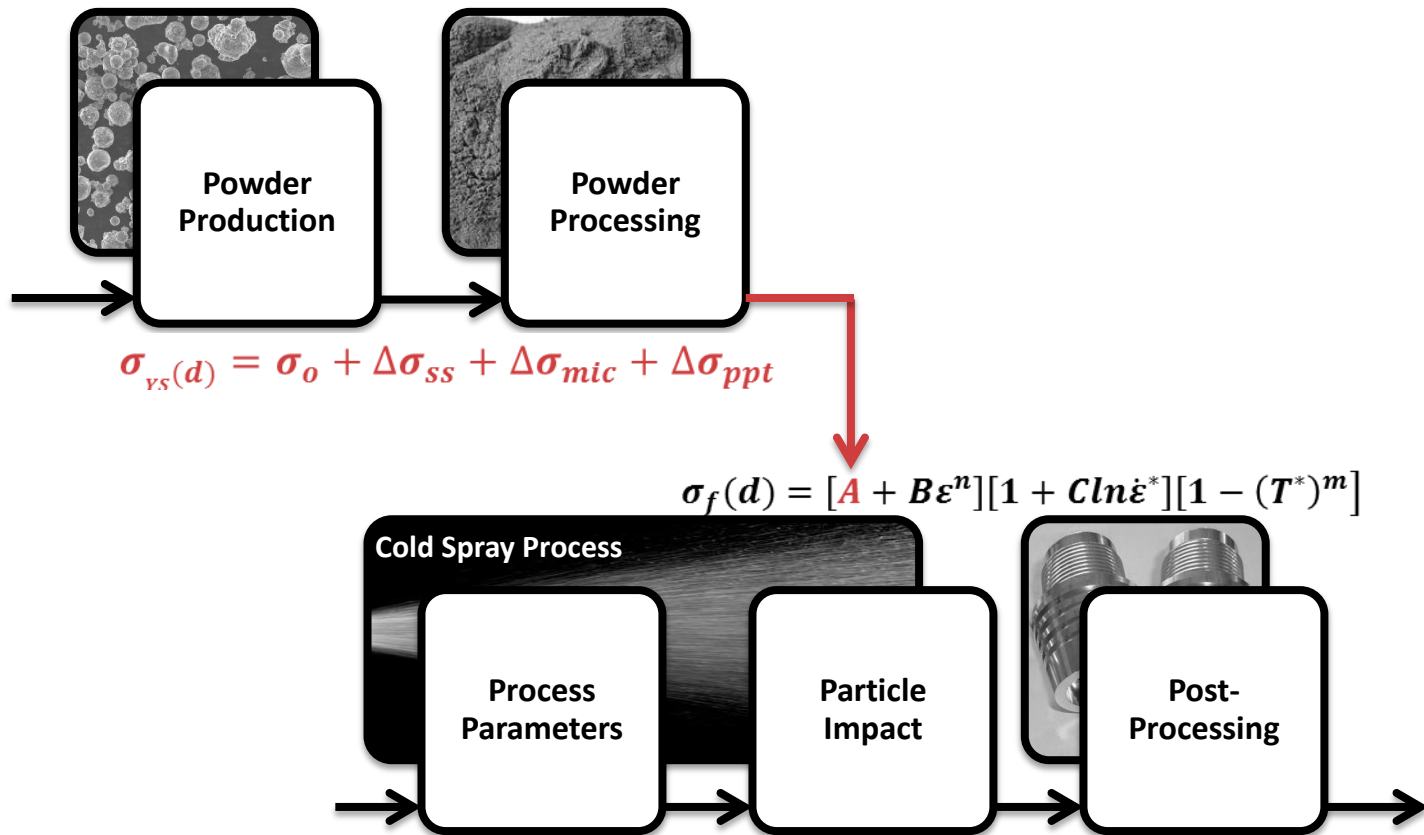
$$\sigma_{YS(d)} = \sigma_o + \Delta\sigma_{ss}(d) + \Delta\sigma_{mic}(d) + \Delta\sigma_{ppt}(d)$$



Al 6061 Kinetic Diagrams



$$\sigma_{YS(d)} = \sigma_o + \Delta\sigma_{ss}(d) + \Delta\sigma_{mic}(d) + \Delta\sigma_{ppt}(d) \longrightarrow \Delta\tau_{Coherency,i} = 7\varepsilon_{coh,i}^{3/2} G \left(\frac{rf}{b} \right)^{1/2}$$



Quantification for Integration

Additive Yield Strength Model

Characterization: Nanohardness

Additive Yield Strength Model



Function of: →

- Alloy composition,
- Powder particle size,
- T, t of heat treatment

Solid Solution Strengthening

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Substitutional Solid-Solution

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Hall-Petch Behavior

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$$\Delta\sigma_{Modulus,i} = 0.01\varepsilon_{Gp,i}^{3/2} G \left(\frac{rf}{b} \right)^{1/2}$$

$$\Delta\sigma_{Chemical,i} = 2\varepsilon_{Ch,i}^{3/2} G \left(\frac{rf}{b} \right)^{1/2}$$

$$\Delta\sigma_{Order,i} = 0.7G \left[\varepsilon_{Ord,i}^{3/2} \left(\frac{rf}{b} \right)^{1/2} - 0.7 \right] \varepsilon_{Ord} f$$

Additive Hardness Model



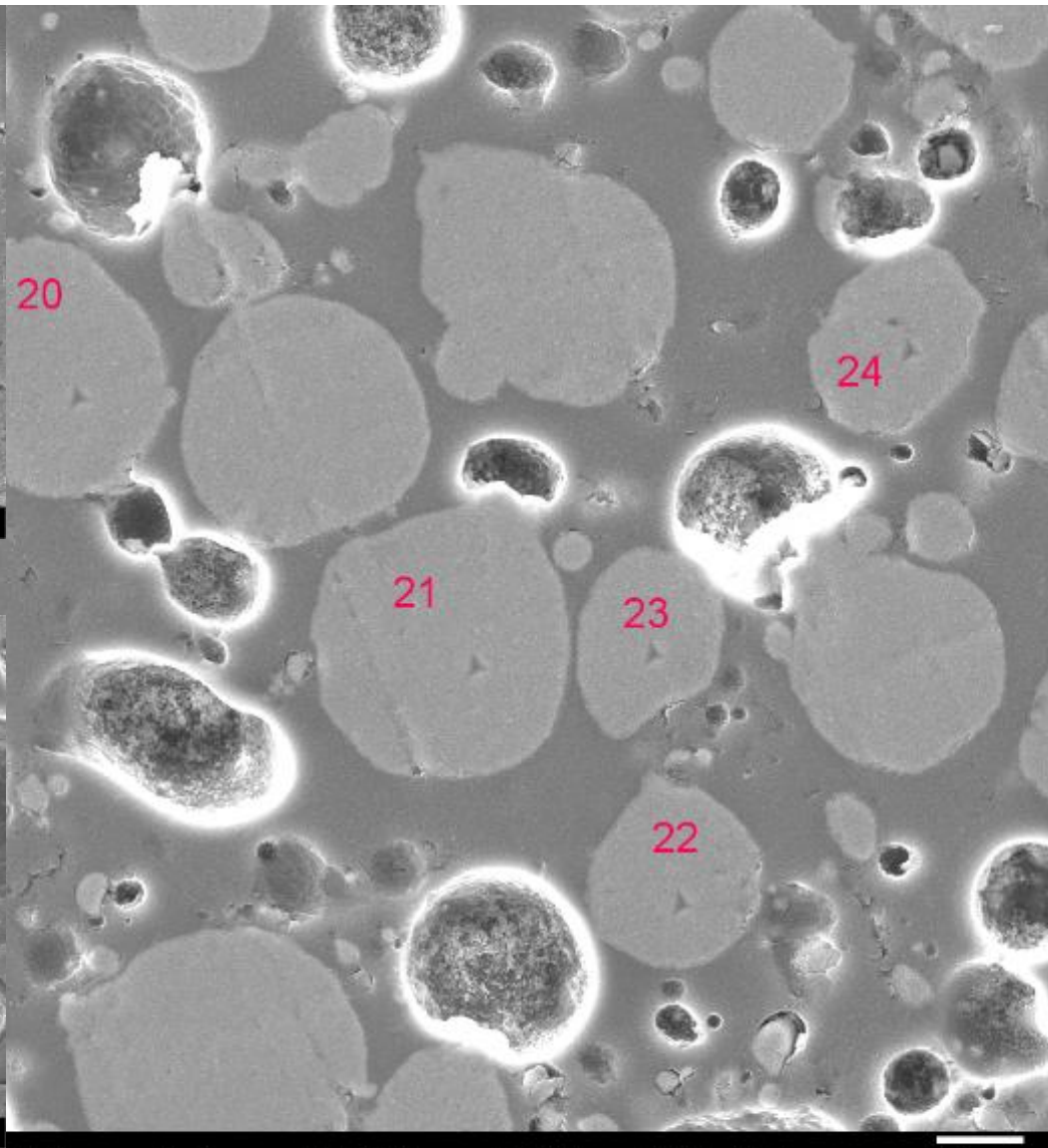
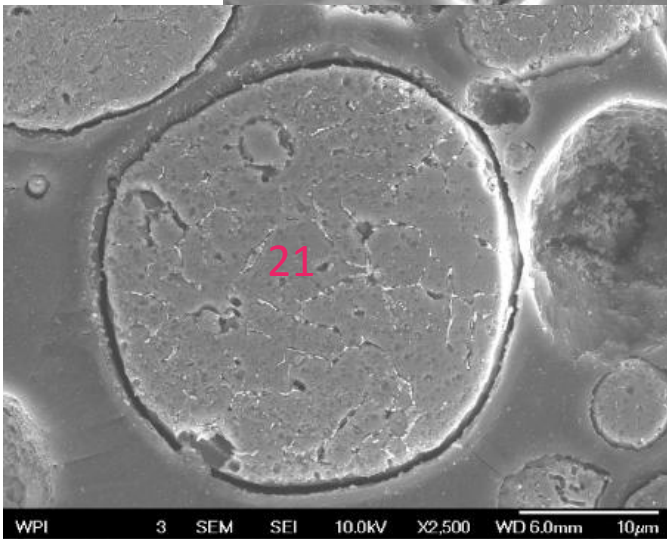
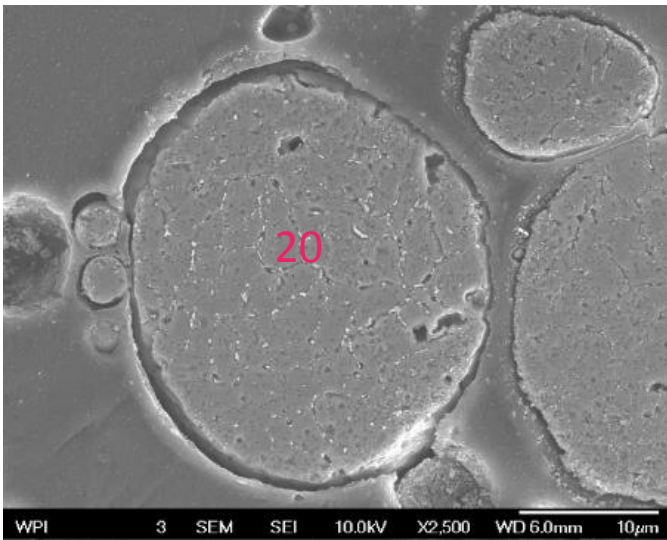
Al 6061

d)

50

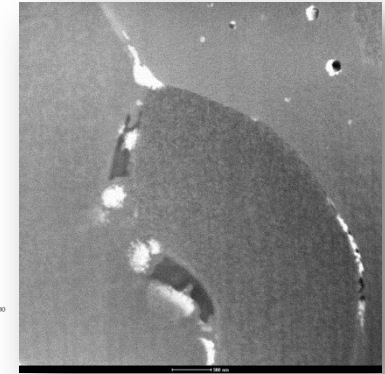
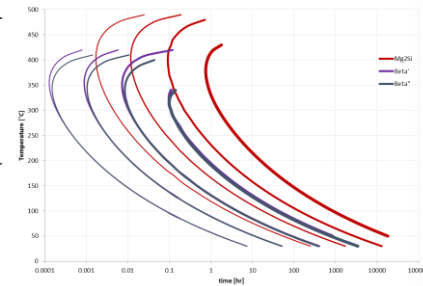
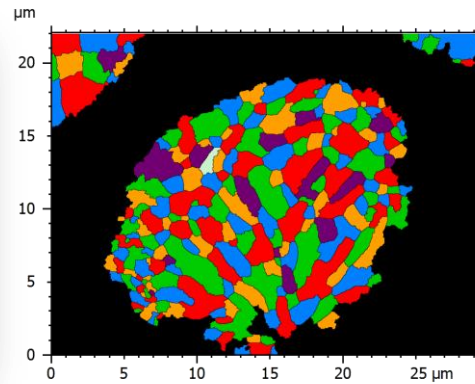
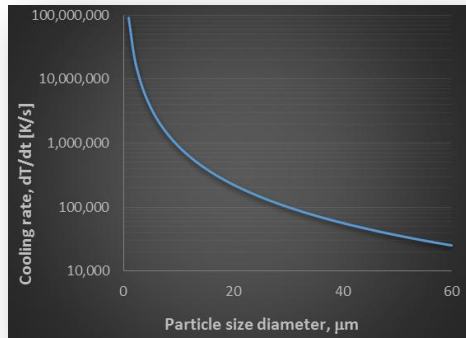
70

n]

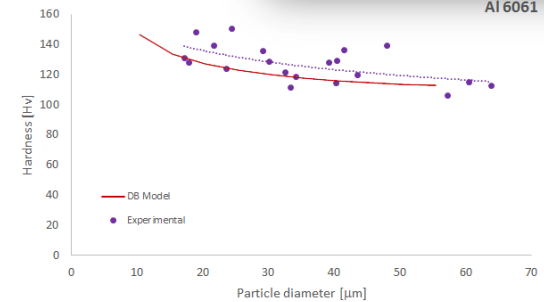


WPI 3 SEM SEI 15.0kV X700 WD 10.0mm 10µm

WPI Overview



Al 6061



Powder Production

Powder Processing

$$\sigma_{YS}(d) = \sigma_o + \Delta\sigma_{ss}(d) + \Delta\sigma_{mic}(d) + \Delta\sigma_{ppt}(d)$$

Cold Spray Process

Process Parameters

Particle Impact

Post-Processing

Acknowledgements:

Contact email:
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bamcnally@wpi.edu



U.S. Army Research Laboratory
Contract #: W911NF-10-2-0098
Victor Champagne, Jr.



**United Technologies
Research Center**



*Le Zhong
Yongho Sohn*

