



### **CSAT Meeting: WPI, Worcester, MA**

# B1 Bomber-FEB Panel Repair by Cold Spray

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Victor Champagne, Ph.D.
Army Research Lab







### **Project Team**



- Repair, Refurbish, and Return to Service Center (R3S) –
  a SD Governor funded 2010 Center of Excellence at the South
  Dakota School of Mines and Technology (SDSMT)
  - Director, Christian Widener, Ph.D.
- HF Webster Engineering Services, Inc.
  - Mr. Rob Hrabe
- Air Force Engineering Technical Services Ellsworth AFB and Ph.D. student SDSMT
  - Mr. Brian James
- Army Research Lab
  - Dr. Victor Champagne
- Life Extension of Navy Weapon Systems Project managed by ACI Technologies, Inc. – Navy Mantech Benchmarking and Best Practices Center



Ms. Rebecca Morris







### **Problem Statement**



- Aluminum aircraft external access panels are typically secured to the airframe with steel TRIDAIR fasteners.
- The fasteners are designed to sit flush with the panel to enable laminar airflow over the fastener head.
- Repeated access to these panels wears and enlarges the holes in the panel.
- As wear increases, the fastener sits further and further below the surface of the panel, resulting in turbulent airflow, vibration of the panel, and eventual pull through and loss of the fastener in flight...









### **Problem Statement**



- Integrally stiffened bonded panel composite metal hybrid structure
- Currently, no acceptable permanent repair exists
- Furthermore, new repair technologies are not systematically incorporated into maintenance supply processes.
  - Organizational barriers prevent implementation of new technology into aging weapon systems
  - Very little funding is available for developing repair processes on legacy weapon systems
- Replacement Cost >\$200K each, but parts are not even available...Fleet liability of approx. \$50M.



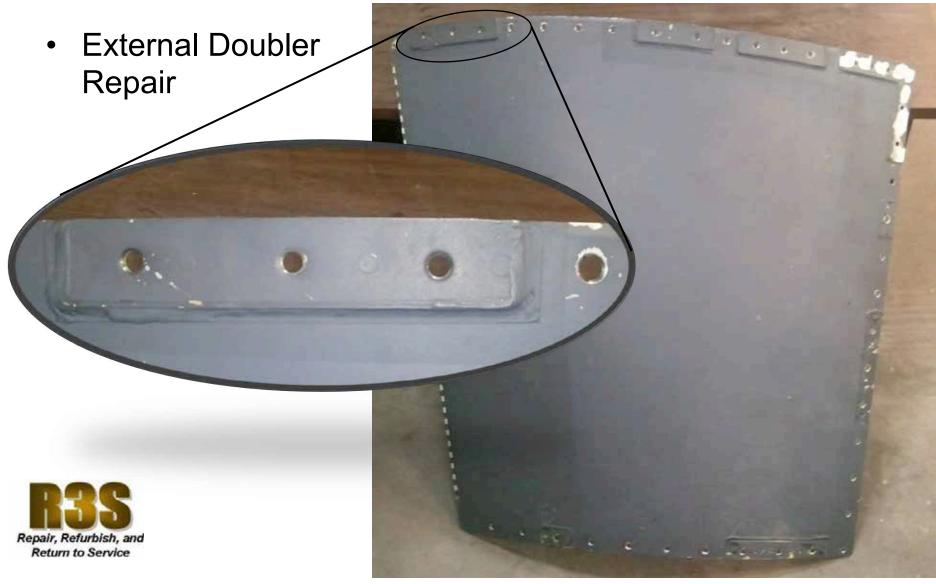
A cold spray repair solution has been developed... ROI > 10:1





## AMP Panel Selected for Refurbishment







## Example: Worn Fastener Holes













### **Grit Blast**



 Each hole was grit blasted prior to cold spray to remove paint from the area and to enhance bonding to the surface.





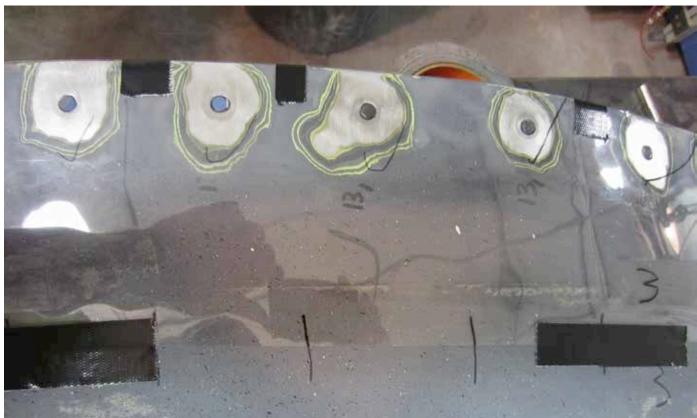




### Template



 Templates were created on Mylar from the existing fastener holes prior to performing the cold spray repair.









### Thermocouple Data



- Temperatures on the back side of the panel were monitored by thermocouple and did not exceed 100°C.
- Max. observed transient temp during repair was 153°F, but 137°F shown here was typical (<63°C).</li>

There is no detrimental effect to the 2024 or composite material substrate at these temperatures.









## Gen II Prototype CS System





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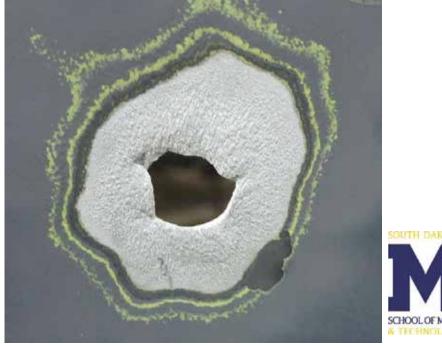


### Cold Spray



- HP cold spray depositions were added by hand to the surfaces of the worn fastener holes.
- Gen II prototype HP CS system
- 350 psi, 350°C, A0027 Centerline powder –Ultralife™ nozzle





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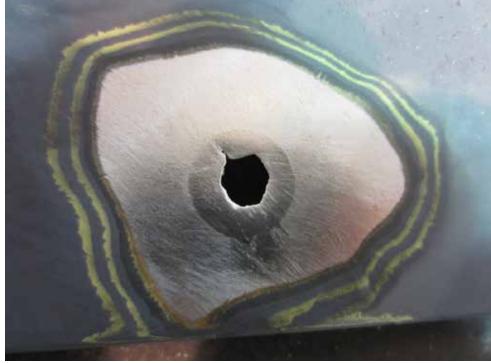


### Fine Polish



 After grinding, the holes were polished with fine scotch brite discs.











### Hole after Micro-Stop



 Final machining was performed using a micro-stop tool to cut the proper chamfer for the Tridair fastener.









### After Micro-Stop



Final repair before painting.



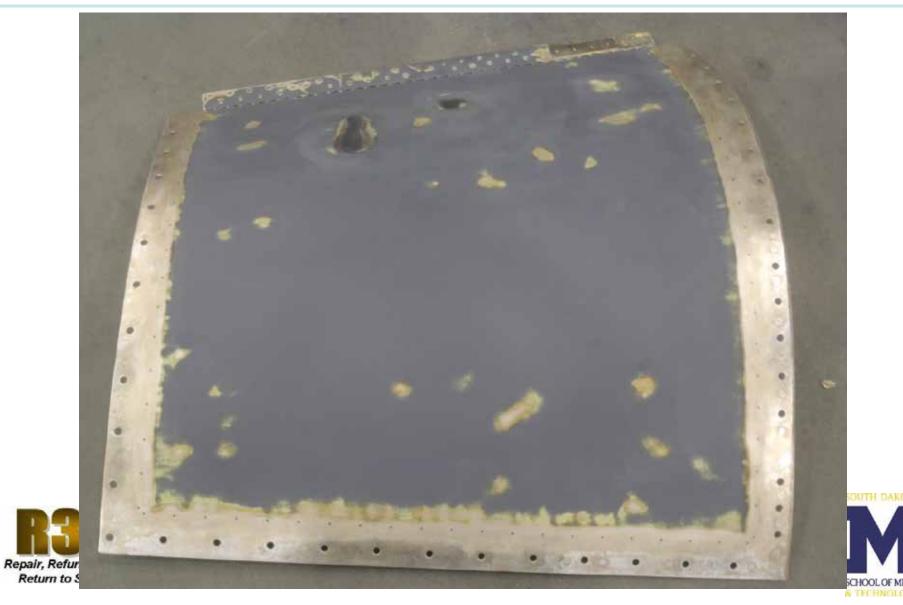






## AMP A5083 FEB Door - Paint Prep (Alodined)







### A5083 FEB Door - Primed

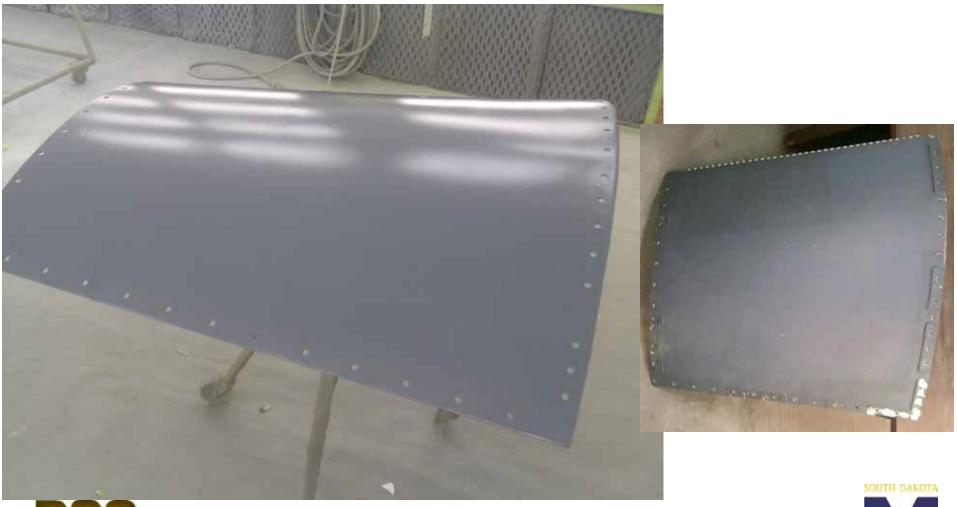






## AMP A5083 FEB Door - Top Coat applied





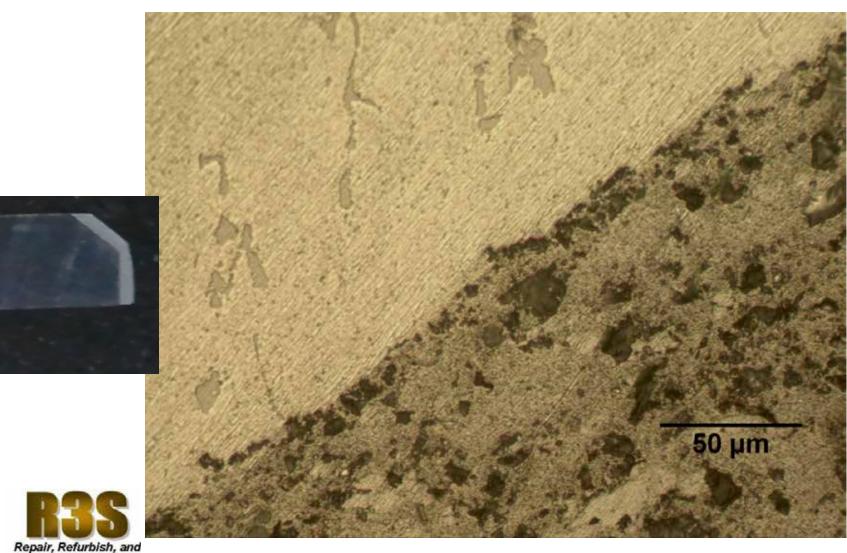






## AMP Cold Spray Interface Macro







Return to Service

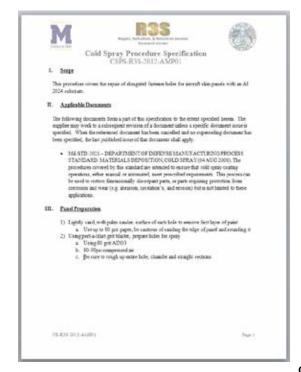


### **Procedure**



- Sprayed at SDSMT using a Gen II System
- A procedure for the repair of the fastener holes using cold spray was prepared by the R3S Center at SDSMT: CSPS-R3S-2012-AMP01.
  - The specification covers the repair of elongated fastener holes in 2024 aluminum sheet for aircraft skins.
  - The repair was documented using a cold spray process control sheet.

M	Repair, Returboli, & Retu Research Cont	er .			
	ay Process Co	ntrol Sheet			
VENDOR: SDSMT-R3S Co	eshe:		Sheet of		
DEPOSITION #: VENDORPROCESS #:		OFF THE O LT	ON: MA Sec. 30.		
PURCHASE OF DER NUMBI	m.	CHRIDICAL	ON: 518-510-51.		
PART NUMBER:	ur.	SN:			
AREA TO RECEIVE DEPOSI	TION:				
PART MATERIAL:					
COLD SPRAY MANUFACTU	RER:	R: NOZZLE:			
	PART PREPAR	ATION			
METHOD OF CLEANING:					
MASKING INFORMATION:					
GRIT TYPE AND SIZE:					
GRIT BLAST PRESSURE:					
PRIMARY GAS:	7 10 10	TEMPERATURE:			
MAIN GAS PRESSURE:	1	FEEDER GAS PRESSURE:			
	COATING POV				
POWDERMATERIAL:		POWDER SIZE:			
SUPPLIER:		MATERIAL LOT #:			
	COATING D.	ATA			
TIME BETWEEN SURFACE	FREP AND SPRAY:				
POWDER FEED RATE:					
POWDER WHEEL SPEED:	100				
NOZZLE TO WORK DISTAN		ero ce			
TRAVERSE RATE PREGLATIONE:		INCREMENT: METHOD OF PREHITAT:			
F 1100 F 100 F 10 F 100	2-00 F11-7	DOFPERENT:			
DEPOSITION THICKNESS A		Taxa man or	LANCE.		
NUMBER OF PASSES PER L METHOD OF COOLING:	ATER	NUMBER OF	EATER:		
NOTES:					
NOIS.					
COLD SPRAY OPERATOR:	AY OPERATOR:		Dute:		
APPROVAL:	AL:		Date:		



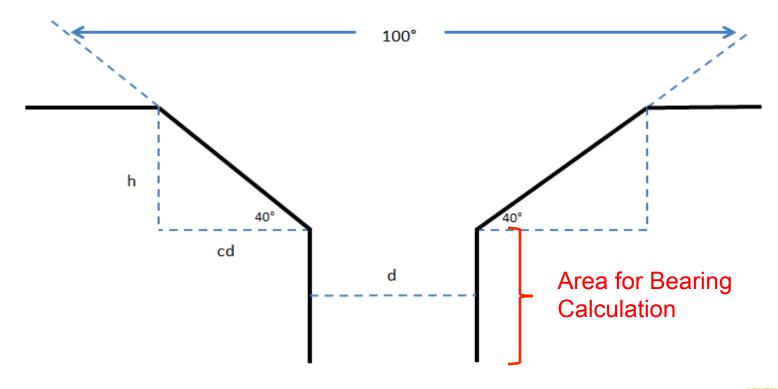






### Counter-Sink Schematic











### **Bearing Load Calculation**



- Based on Mil-HDBK-5H guidelines, section 1.4.7, calculated bearing load depends on straight section thickness.
- Measured panel thickness of 0.147-in. leads to a max load of 3369 lbs.

$$P = Fbry*(t-h)*d$$

$$h = \tan(40^{\circ})*(cd-d/2)$$

#### t=0.095-in. bearing surface

Edge Distance	е	1.25	in
Hole Diameter	D	0.375	in
e/D	3.333333		
<b>Bearing Yield Stress</b>	Fbry	95000	psi
			·
Hole Diameter	d	0.375	in
Thickness	t	0.147	in
Countersink Depth	h	0.052	in
Load	Р	3369	lbs







### **Testing Procedure**



- Guided lap shear
- Fastener torque applied = 40 in-lbs
- Carried full Mil-HDBK fastener bearing yield load of 3400lbs.
- Tested up to failure at 5600 lbs no delamination at failure











### **Mechanical Testing**



### **Cold Spray Adhesion**

- Three lug shear testing
- >5000 psi avg. interface strength (Avg. 5681 psi ± 729)









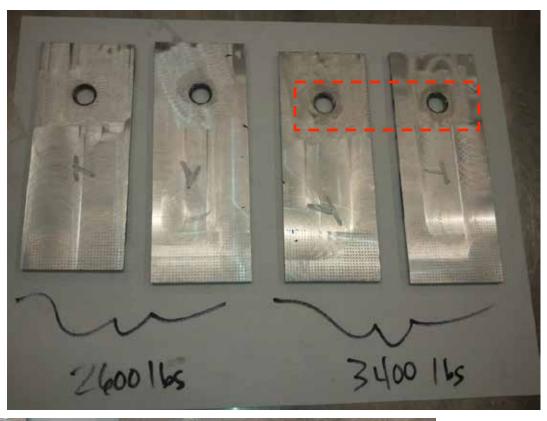
### **Testing Results**



No evidence of cold spray material failure observed up to full bearing yield.











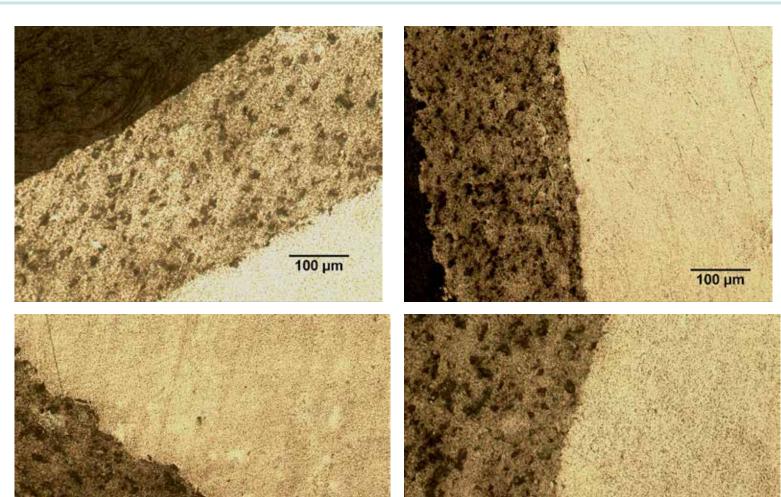




### **Tested Coupon Micrographs**



100 µm





100 µm



### Failure Load Testing



 Even tested up to failure at 5600lbs, the cold spray material did not separate from the coupon.





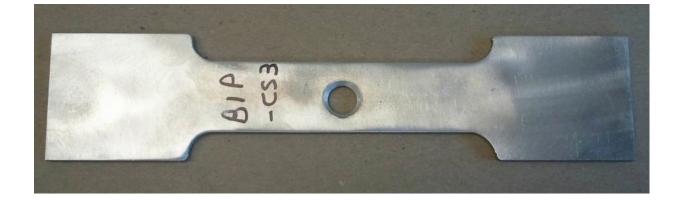
### **Mechanical Testing**



### **Fatigue Testing**

- Open hole fatigue testing
- Coupons prepared per CSPS-R3S-2012-AMP01
- Testing performed per ASTM E466
- R=0.1
- At 15 ksi tensile stress (typical upper end for aircraft skin design loads) coupons lasted approx. 500,000 cycles.









### Conclusions



- Panels can be restored to their full form, fit, and function.
- Cold Sprayed coupons met or exceed the required bearing loads for the parent material and fastener type for this application.
  - Even when tested to failure (greater than 1.5 x bearing yield) the cold spray material did not separate from the panel.
- The repair is expected to have an acceptable lifetime in service, and represents minimal risk of failing in service.
- The coating could even be reapplied if needed, since the process does not overage the substrate material.
- The repair is currently flying on a B1 under an ETAR (since August 2012).







### **Future Efforts**



- The process is now being licensed by MOOG, and has potential application on other DoD and commercial aircraft
- A broad collaborative effort is also being initiated with the support of Tinker AFB to do a much larger qualification program to consider making it a part of the approved repair procedures for the B1.
  - Full qualification testing protocol, including spray parameters & powders
  - Identify opportunities on other aircraft
- Continue development of VRC-Gen III HP Hybrid Cold Spray System...

