



Advanced Computational and Experimental Methods in Cold Spray

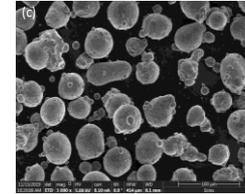
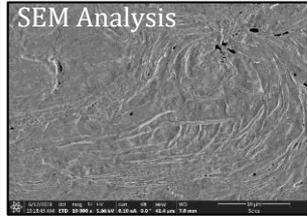
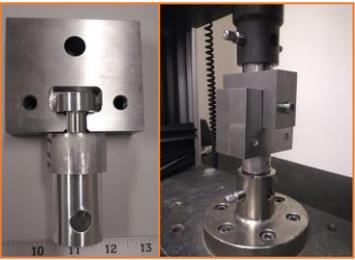
Northeastern University
Cold Spray Additive Manufacturing Laboratory

Ozan C. Ozdemir, Enqiang Lin, Qiyong Chen, Lauren Randaccio, Joseph
Conahan, Joseph Lynch, Patricia Schwartz, Teiichi Ando, Taskin Padir,
Mohammad Taslim, Sinan Muftu

Cold Spray Action Team Meeting
Online
06/24/2020

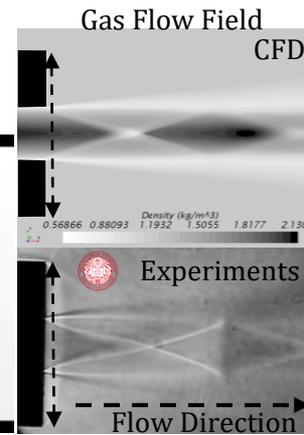
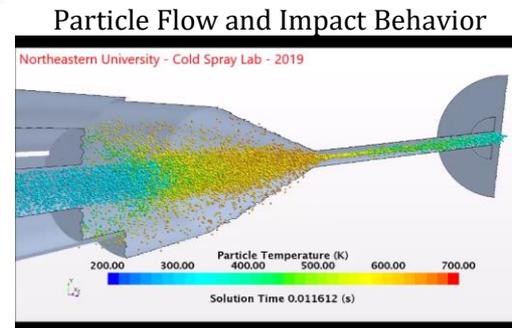
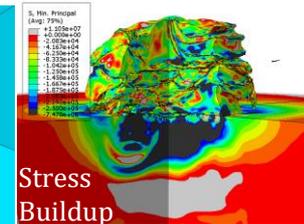
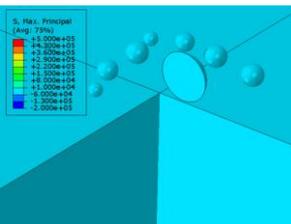
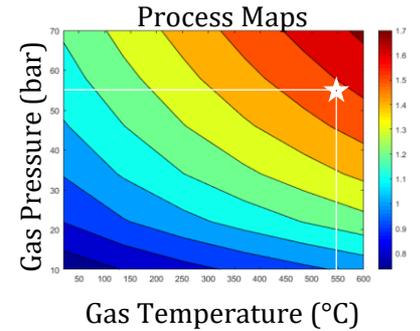
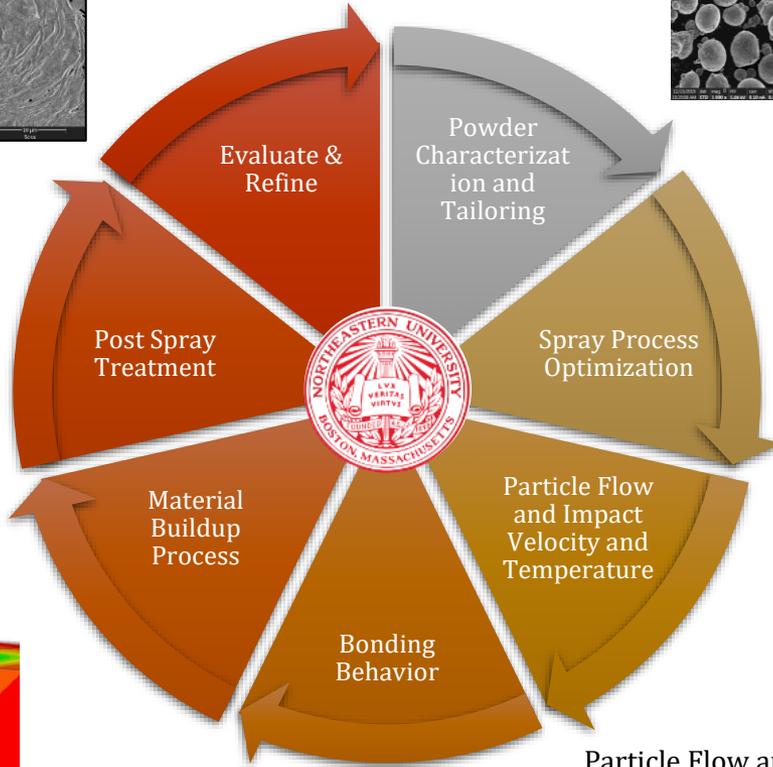
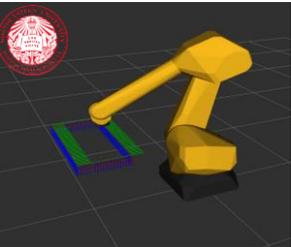


Model Guided Materials & Process Development



Powder Characterization

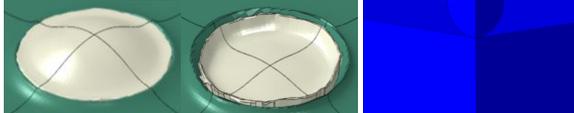
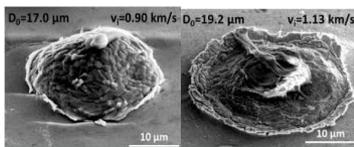
- Metallurgical
- Microstructural
- Mechanical
- Size distribution
- Shape distribution



W. Xie, J.-H. Lee, UMASS

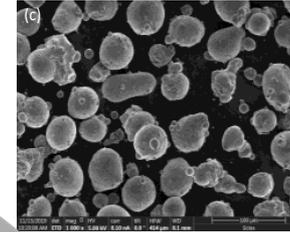
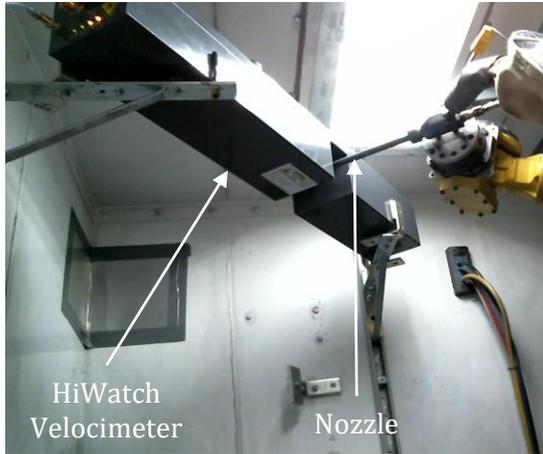


O. Chen, et al., NU



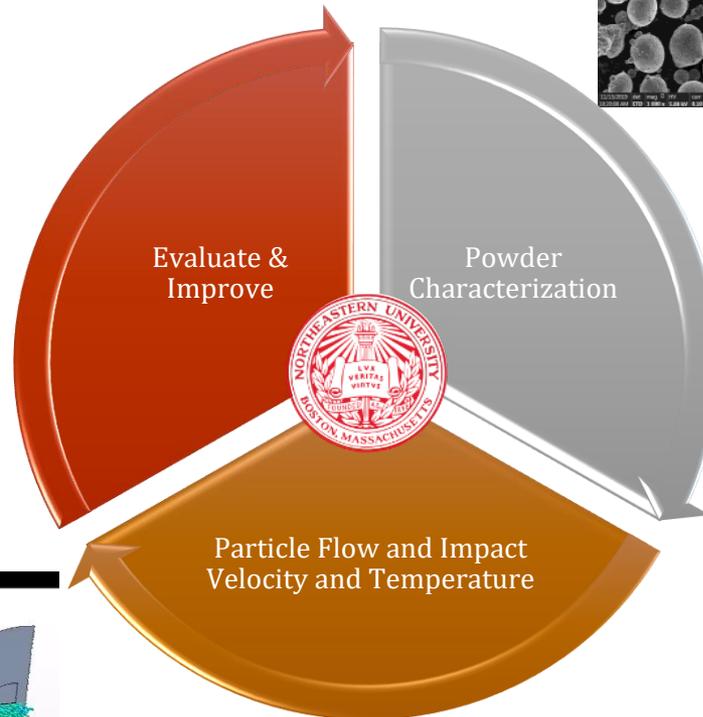


Today's Focus: Factors Affecting Particle Flight and Impact Behavior

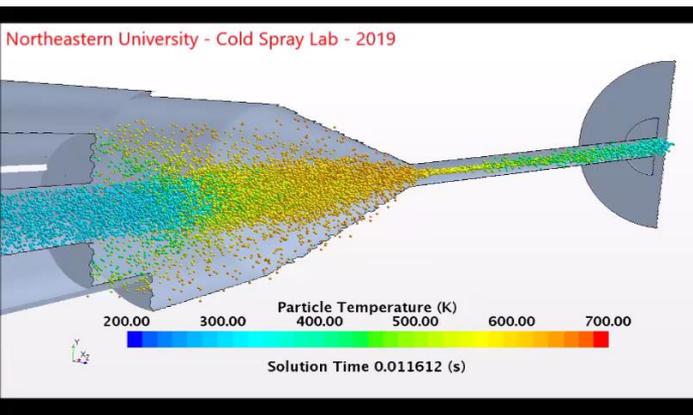


Powder properties of interest

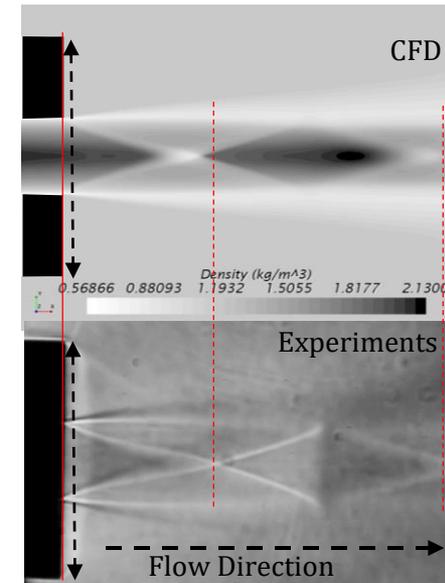
- Metallurgical
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Determining Particle Impact Conditions

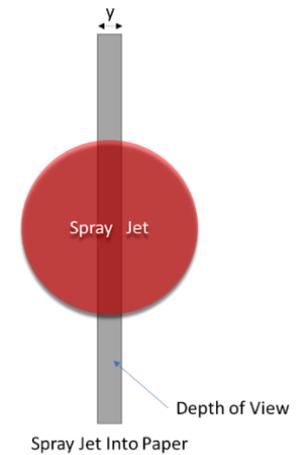
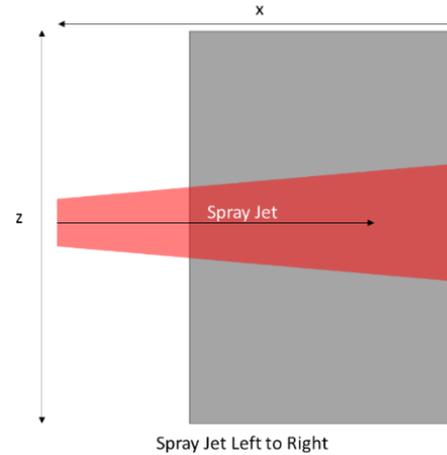
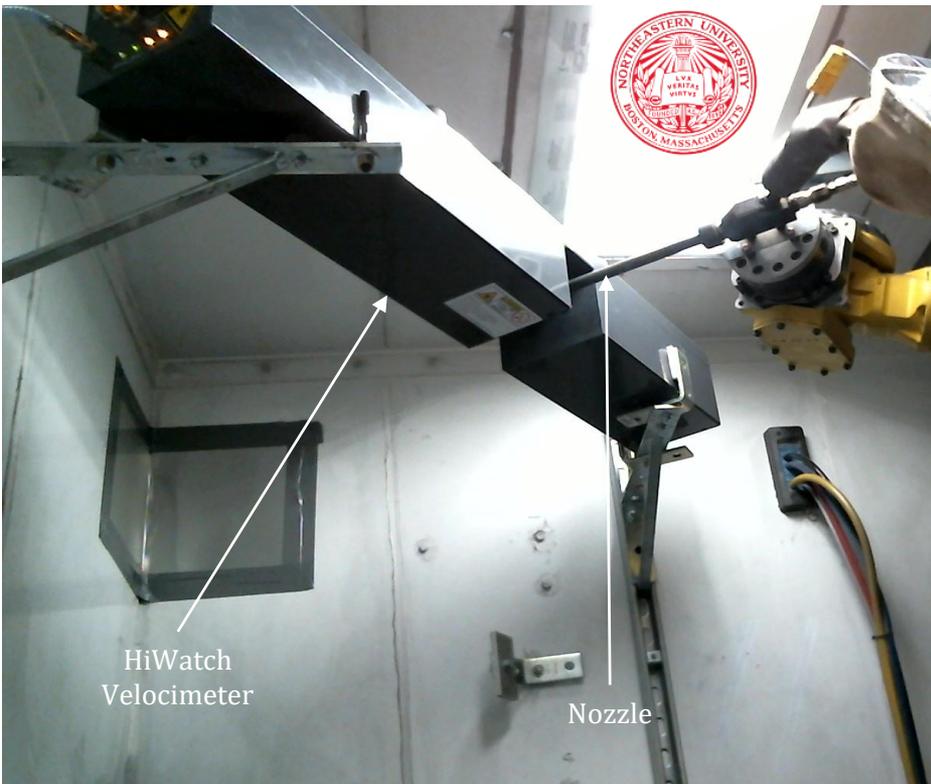


Gas Flow Field Analysis

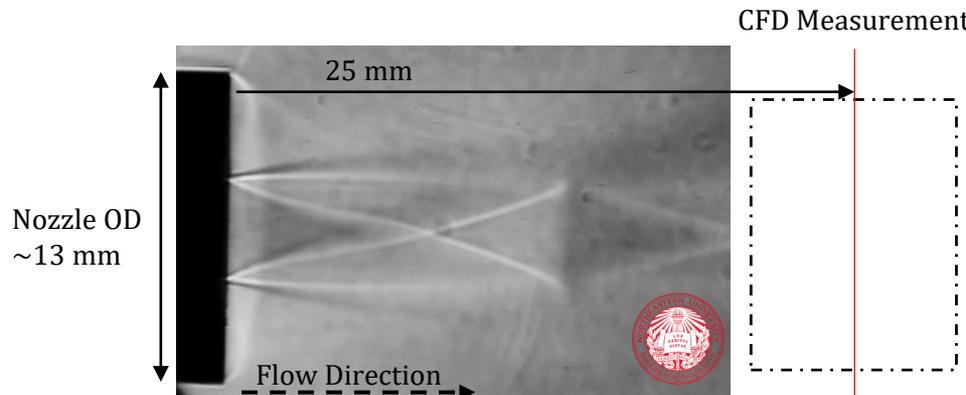




Particle Flight Velocity Measurements and Mismatch with CFD Simulations



Measurement Limitations
Max Velocity: 1,400 m/s
Max d_p : 5 μ m
Particle size distribution different than actual



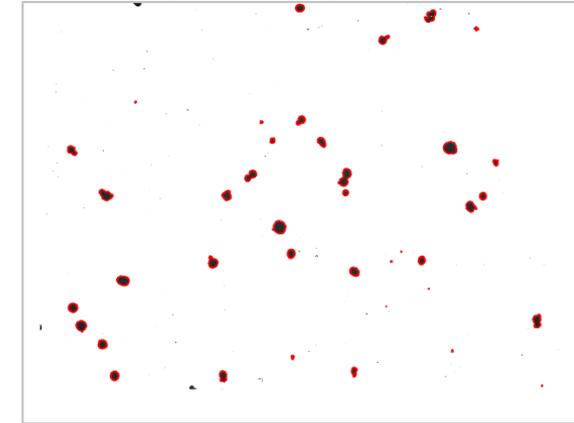
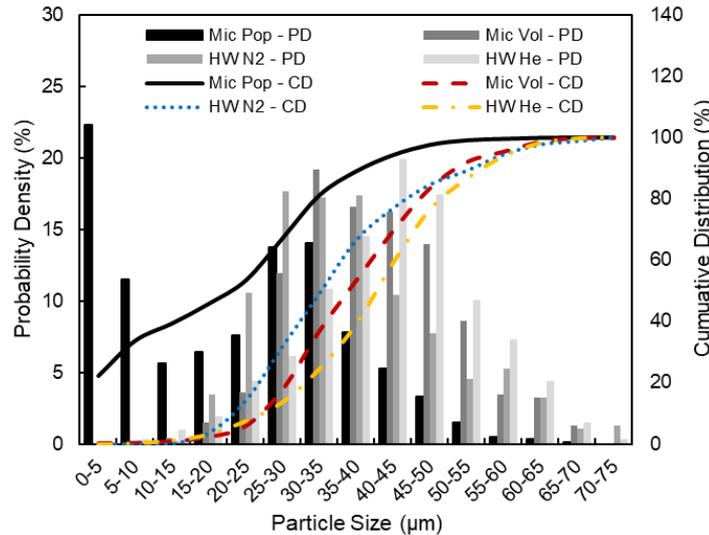
Schlieren Image Taken at NU Showing Shock Diamonds



Particle size distribution for Al and Cu through transmission microscopy.

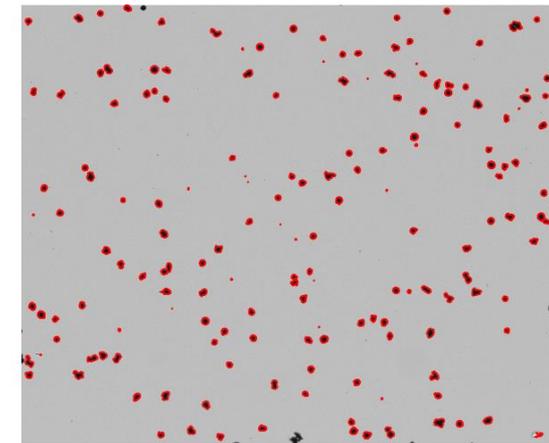
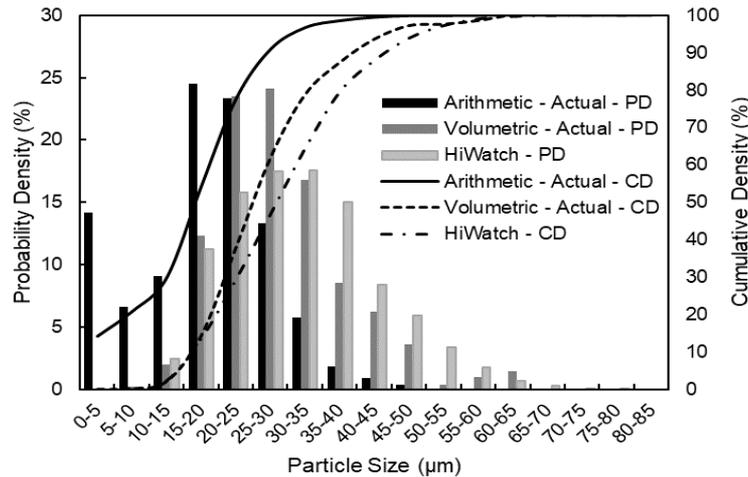


<p>VRC System Nozzle 71 Helium 35 bar, 425 C Mil Spec Al6061 Powder Valimet</p>
<p>VRC System Nozzle 71 Nitrogen 65 bar, 425 C Mil Spec Al6061 Powder Valimet</p>



Transmission Microscopy
Valimet-MilSpec-Al6061

<p>SPEE3D System Water Cooled Nozzle Air 35 bar, 500 C Copper Powder Praxair</p>
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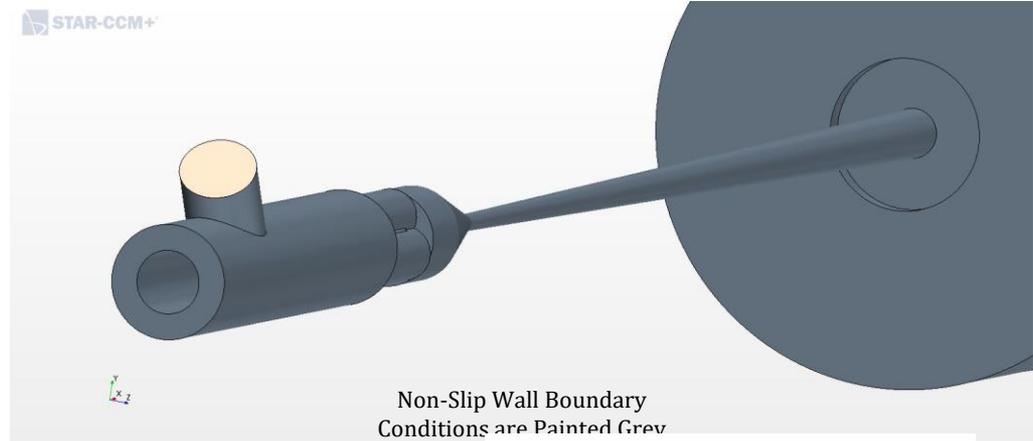
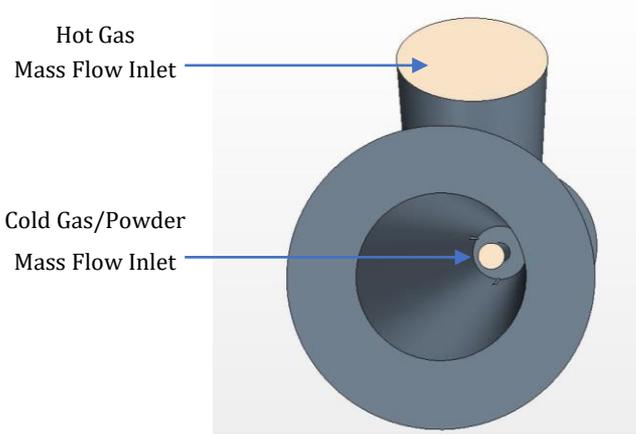


Transmission Microscopy
Praxair Cu-159-3



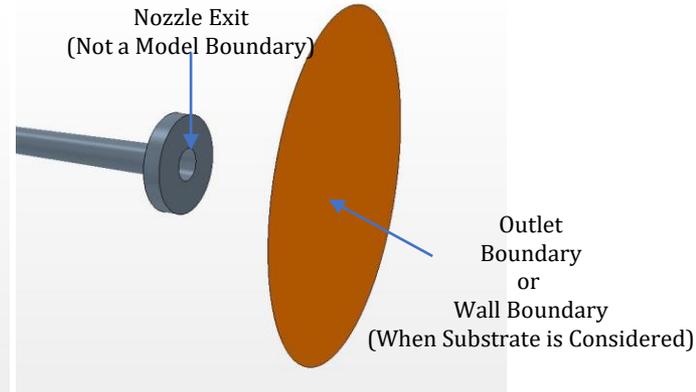
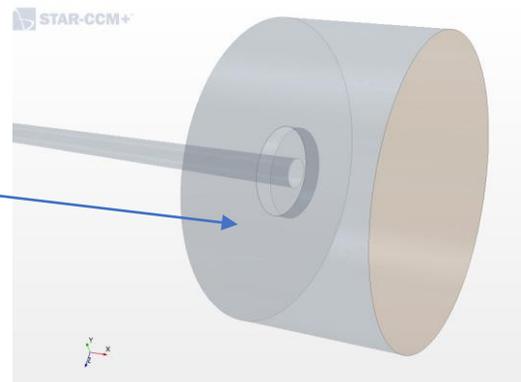
3D CFD Model Domain Boundaries

Particle Flight Behavior &
Impact Velocity and
Temperature



Wall Boundary
or
Outlet Boundary
(When Substrate is Considered)

This boundary is setup as a non-slip wall boundary condition to help stability when computational power is limited and mesh is course.



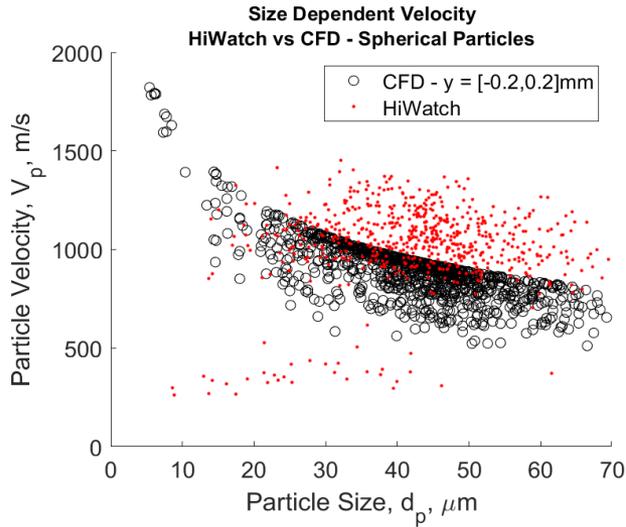
Continuous Phase Computations

- Navier Stokes Equations of Mass, Momentum, and Energy Conservation
- Realizable $k-\omega$ Shear Stress Transport Reynolds Averaged Navier Stokes Approximation

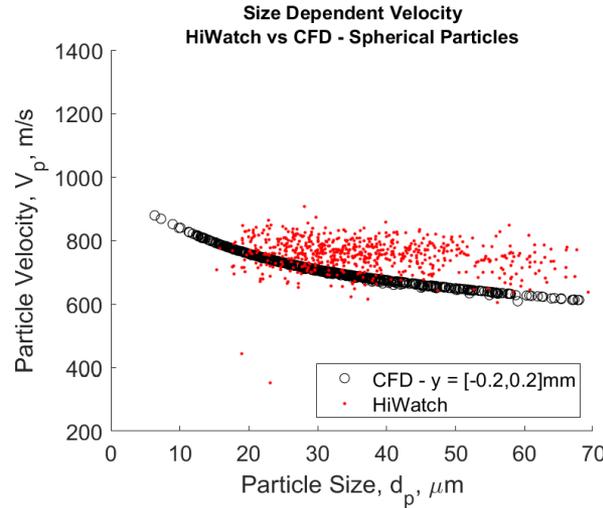


Initial HiWatch vs CFD Comparisons

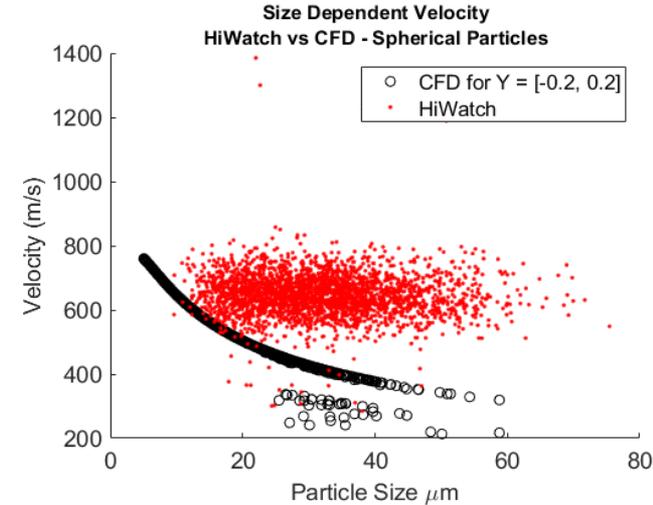
Particle Flight Behavior &
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VRC System
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35 bar, 425 C
Mil Spec Al6061 Powder
Valimet



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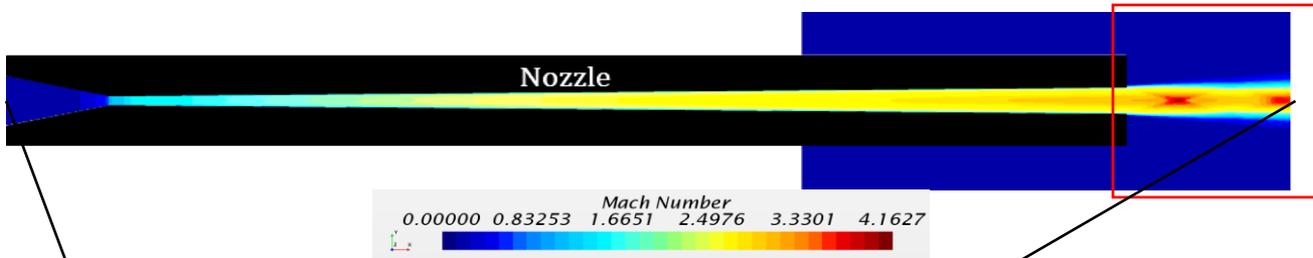
SPEE3D System
Water Cooled Nozzle
Air
35 bar, 500 C
Copper Powder
Praxair

- Mean particle velocity measurements with full particle size distribution (PSD) match mean measurements by HiWatch
- But HiWatch PSD does not match with actual powder PSD
- CFD simulations carried out by HiWatch measured PSD show discrepancy in mean and size dependent particle velocity.
- Possible causes
 - HW measures size inaccurately (ruled out after discussions with manufacturer)
 - Gas dynamics is not captured properly
 - Particle dynamics is not captured properly



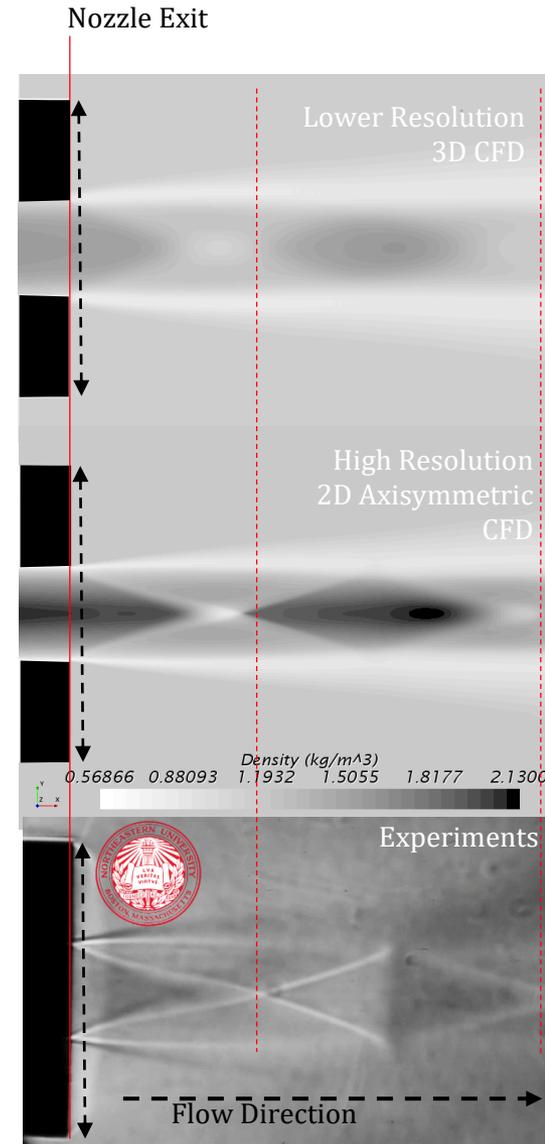
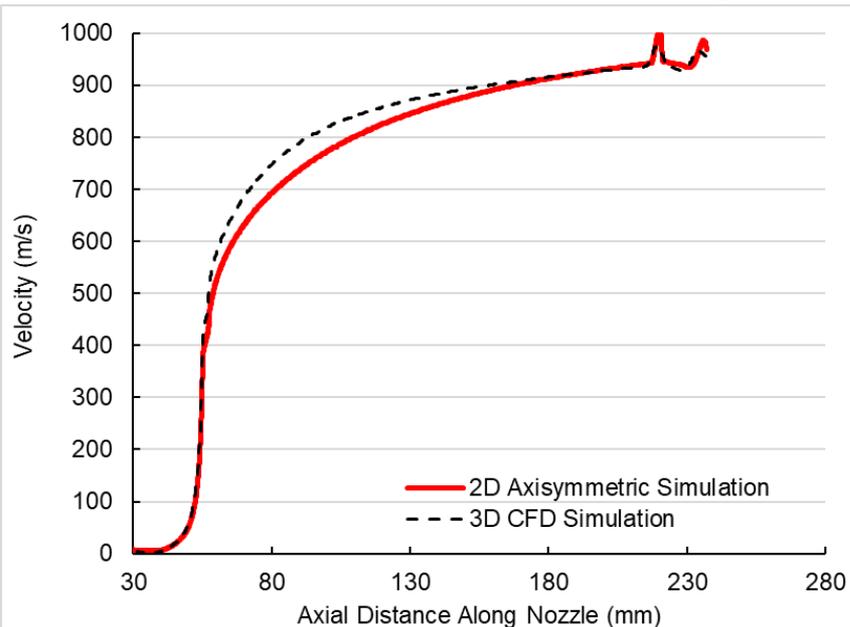
Confirmation of Gas Dynamics Calculations through Schlieren Imaging

Evaluate & Refine



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Mil Spec Al6061 Powder
Valimet

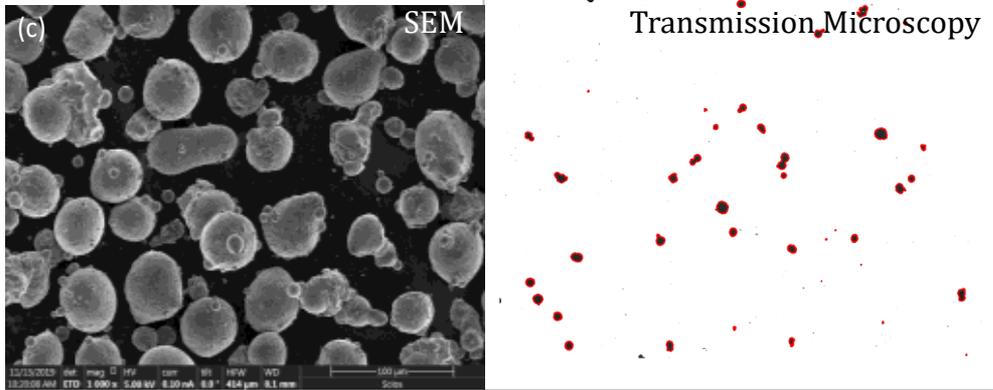
- Schlieren image of the nitrogen case shows that the supersonic jet formation is captured accurately by 2D axisymmetric CFD.
- Hi resolution 2D Axisymmetric simulation matches well with the lower resolution 3D simulations.
- Slight differences are expected.
- Mismatch is not sufficiently high to justify the big difference in particle velocity.





How spherical are gas atomized particles?

Evaluate & Refine



gas atomized aluminum particles

Drag Coefficient of Off-Spherical Particles

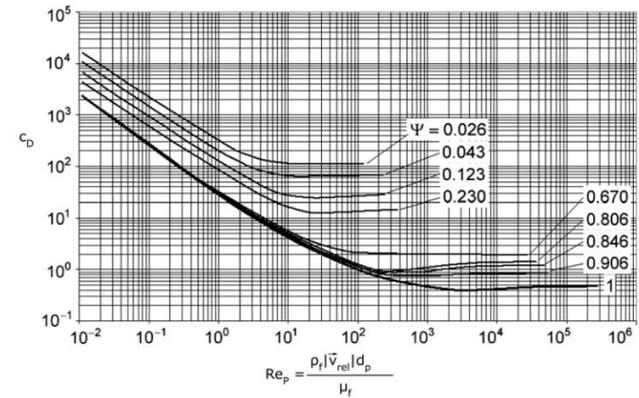


Figure 4.5. Drag coefficient of a non-spherical particle dependent on the particle Reynolds number and the sphericity ψ .

S. Martin, J.R. Williams, *Multiphase Flow Research*, Nova Science Publishers, Inc., 2009

$$C_D = \frac{24}{Re_p} \left[1 + \exp(2.3288 - 6.4581\Psi + 2.4486\Psi^2) \cdot Re_p^{(0.0964 + 0.5565\Psi)} \right] + \frac{\exp(4.905 - 13.8944\Psi + 18.4222\Psi^2 - 10.2599\Psi^3) \cdot Re_p}{\exp(1.4681 + 12.2584\Psi - 20.7322\Psi^2 + 15.8855\Psi^3) + Re_p}$$

S. A. Morsi and A. J. Alexander, "An investigation of particle trajectories in two-phase flow systems," *J. Fluid Mech.*, vol. 55, no. 2, pp. 193-208, 1972, doi: 10.1017/S0022112072001806.

Cold spray Re_p range: $0 < Re_p < \sim 10^3$
Significant effects of shape on velocity expected.

$$\Psi = \frac{\text{Surface Area of Equivalent Volume Sphere}}{\text{Surface Area of Particle}}$$

$$\Psi = \frac{d_n}{a}$$

$$\Psi = \left(\frac{bc}{a^2}\right)^{\frac{1}{3}}$$

$$\Psi = \frac{c}{(ab)^{\frac{1}{2}}}$$

$$\Psi = \left(\frac{c^2}{ab}\right)^{\frac{1}{3}}$$

Ψ = sphericity
 d_n = nominal diameter
 a = major axis
 b = median axis
 c = minor axis

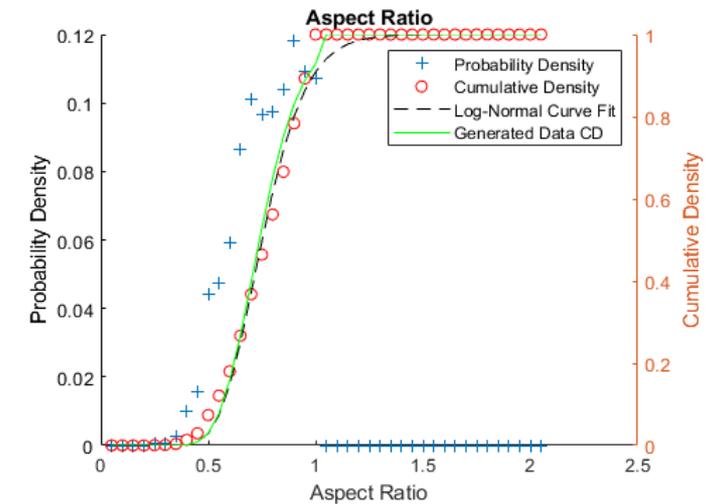
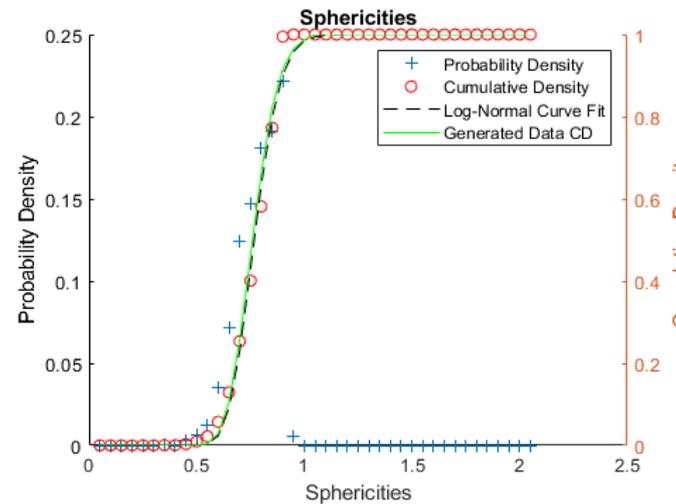
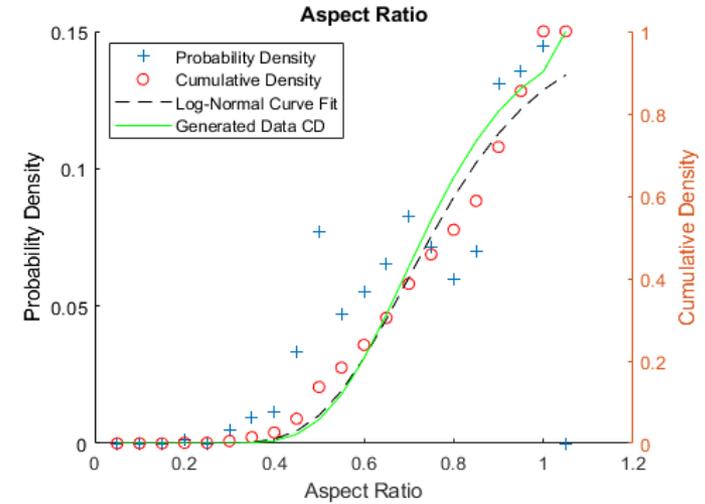
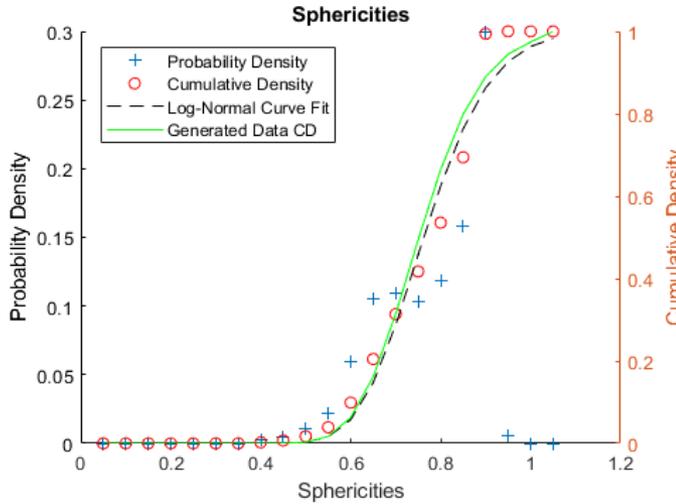


Particle shape distribution for Al and Cu through transmission microscopy.



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Water Cooled Nozzle
Air
35 bar, 500 C
Copper Powder
Praxair Cu-159-3



Effects of Sphericity

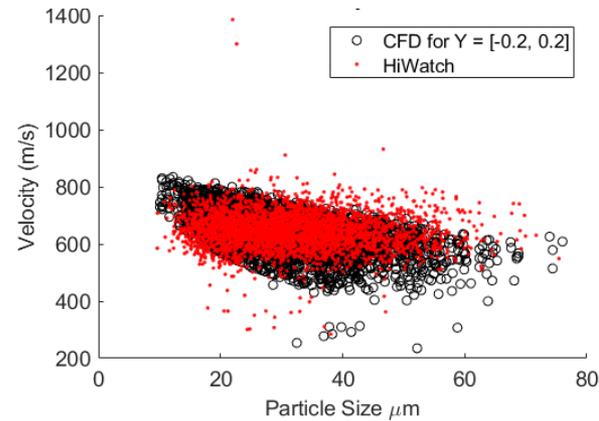
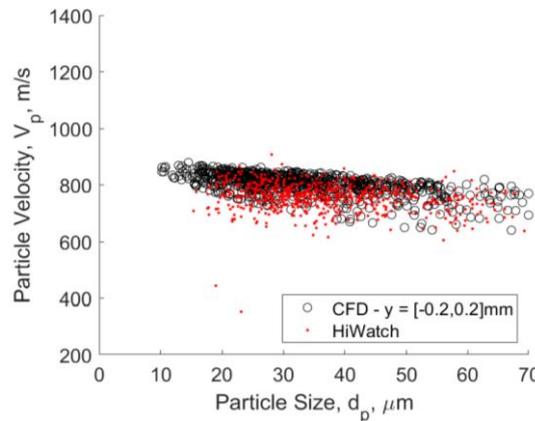
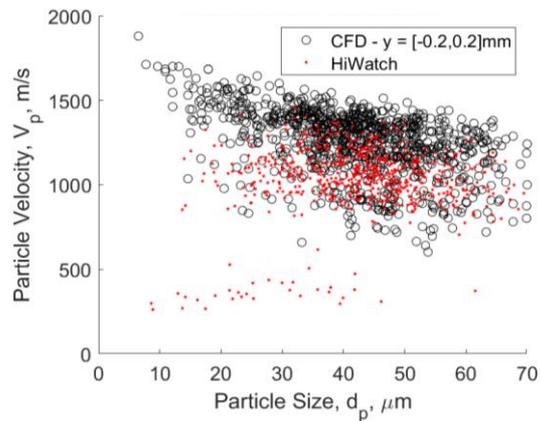
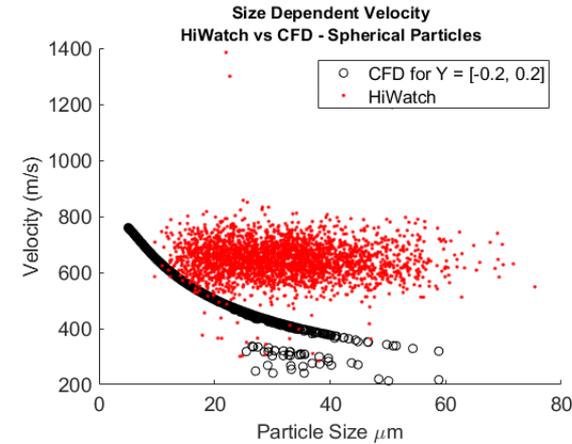
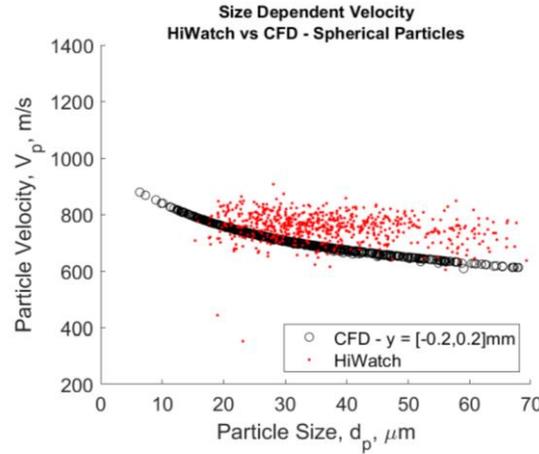
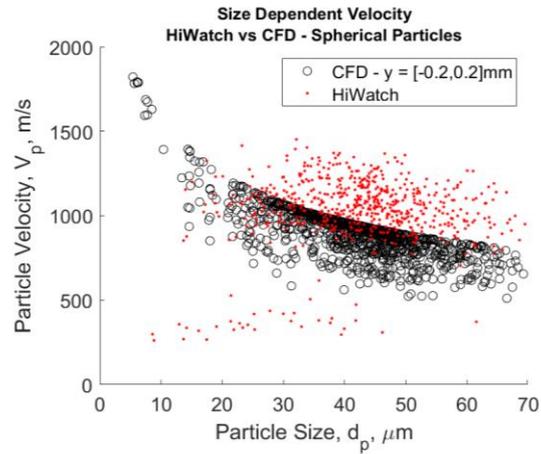
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Water Cooled Nozzle
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Perfectly
Spherical
Particles

Variable
Sphericity
Particles

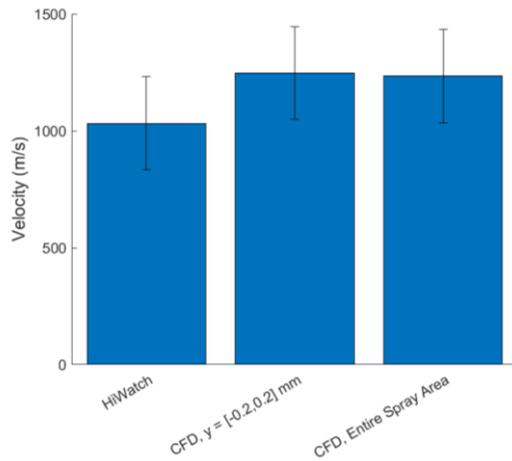
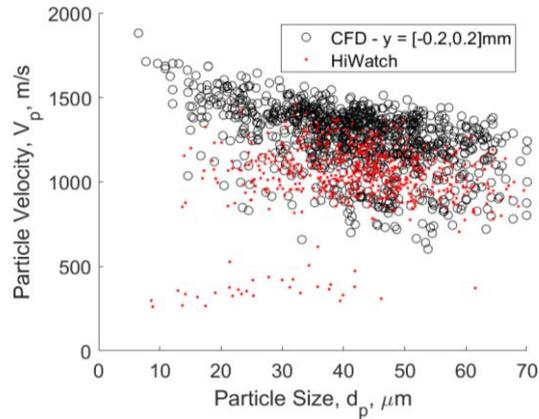


Velocity Estimation

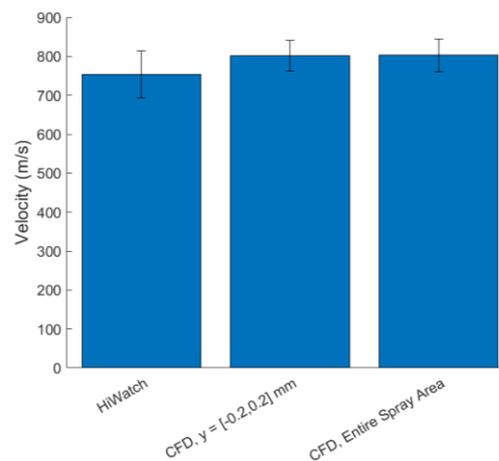
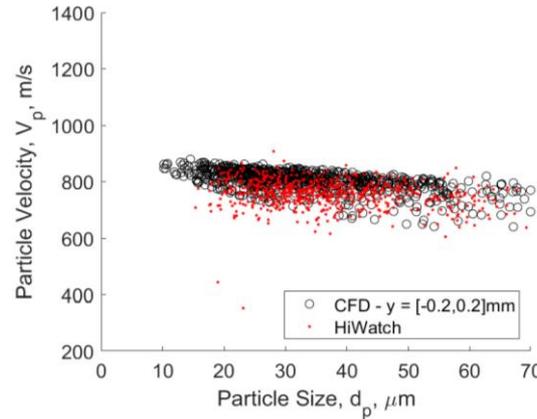
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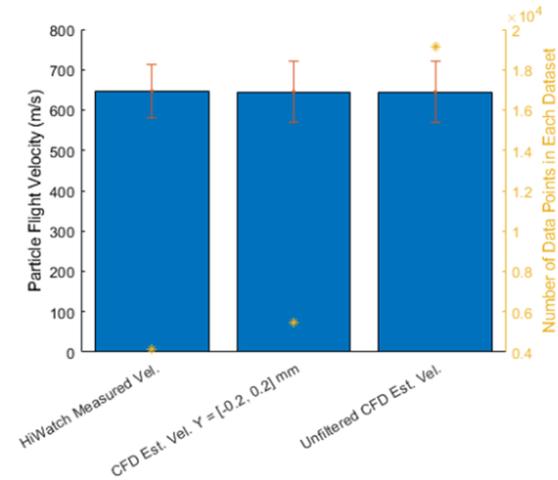
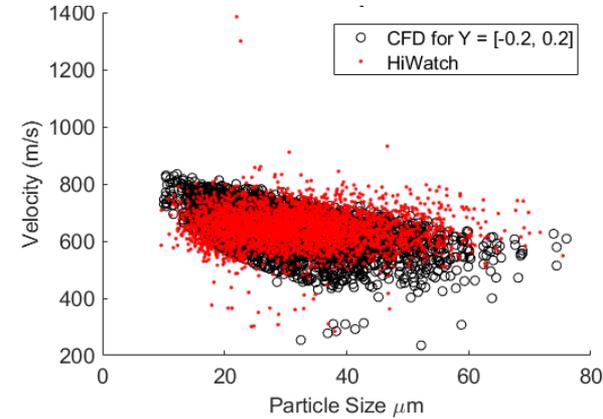
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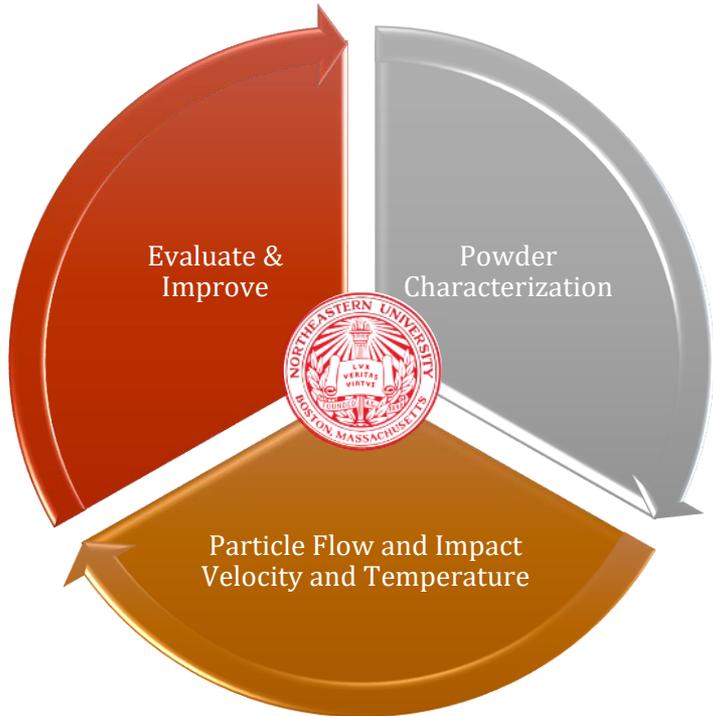


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Refine Particle Shape Measurement



Refined particle shape analysis through measurement of 3rd dimension through interferometry

$$\Psi = \frac{\text{Surface Area of Equivalent Volume Sphere}}{\text{Surface Area of Particle}}$$

$$\Psi = \frac{d_n}{a}$$

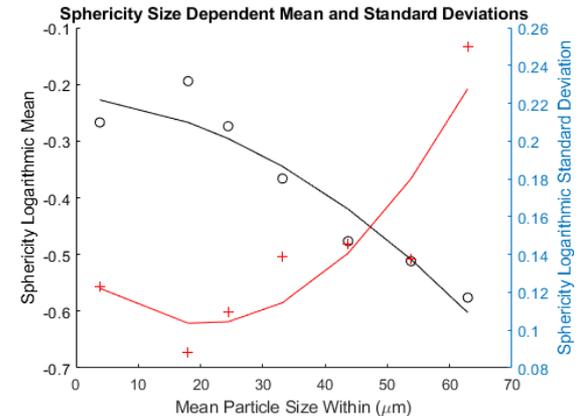
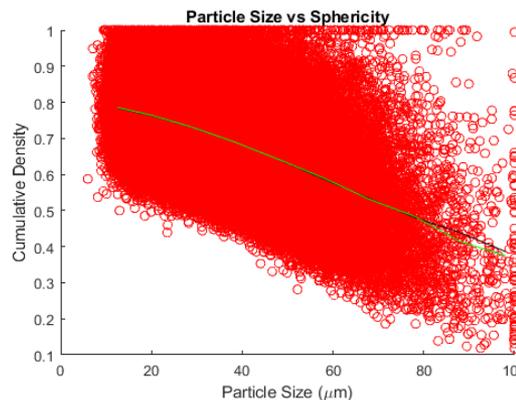
$$\Psi = \left(\frac{bc}{a^2}\right)^{\frac{1}{3}}$$

$$\Psi = \frac{c}{(ab)^{\frac{1}{2}}}$$

$$\Psi = \left(\frac{c^2}{ab}\right)^{\frac{1}{3}}$$

$\Psi = \text{sphericity}$
 $d_n = \text{nominal diameter}$
 $a = \text{major axis}$
 $b = \text{median axis}$
 $c = \text{minor axis}$

Dependency of particle shape to particle size.





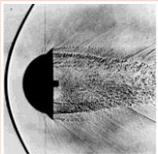
Major Findings



Particle shape, generally not measured in cold spray, is an important factor for impact velocity.



Particle shape measurement methods developed throughout this study needs to be improved to increase accuracy.



Bow shock that forms ahead of the substrate has a significant impact on particles that have off-spherical shapes. (More thorough analysis of this work will be published.)



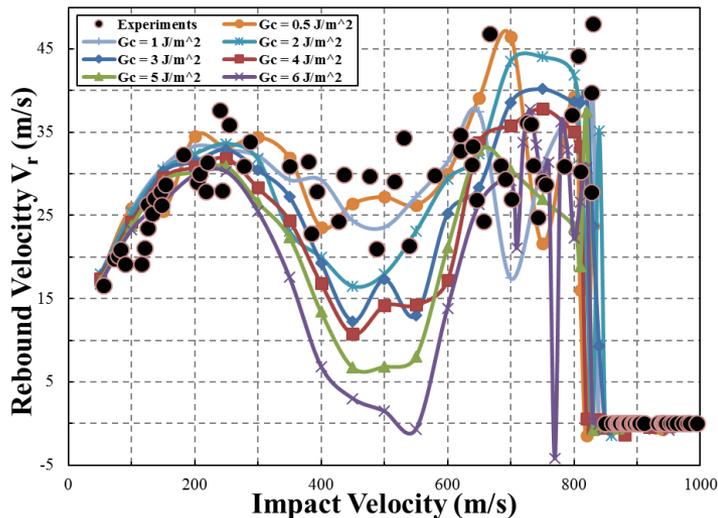
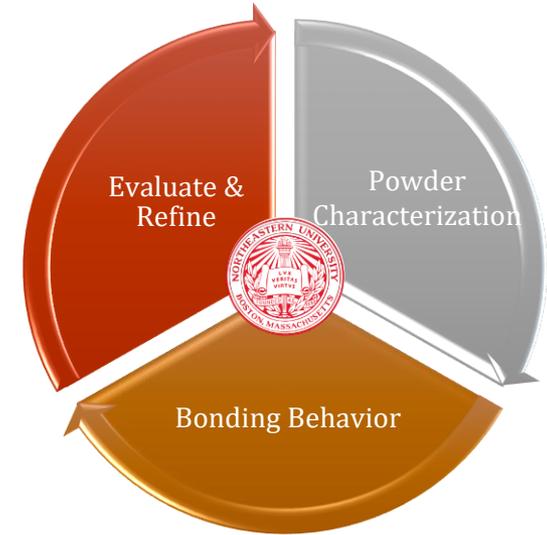
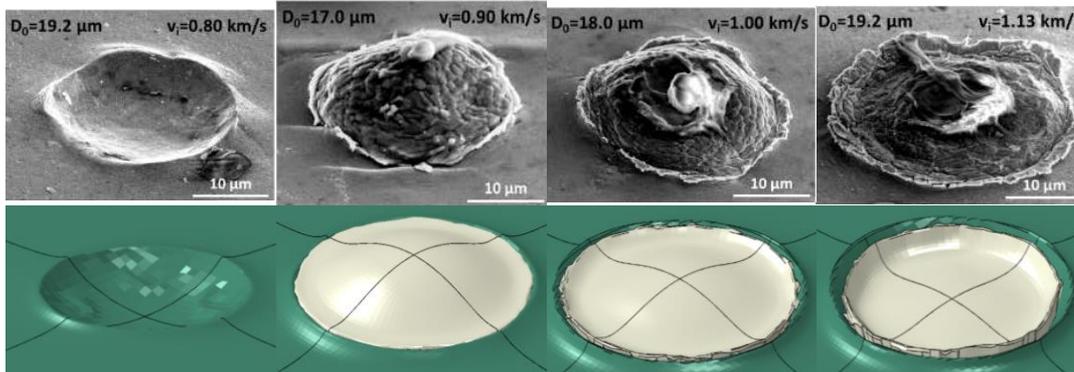
Calibrated Models Provide Interfacial Energy and Thermal Energy Rise During Impact



W. Xie, J.-H. Lee,
UMASS



Q. Chen, et
al., NU



Thermal energy
conversion to kinetic
energy

$$TE_{particle} = 0.34 \cdot KE$$

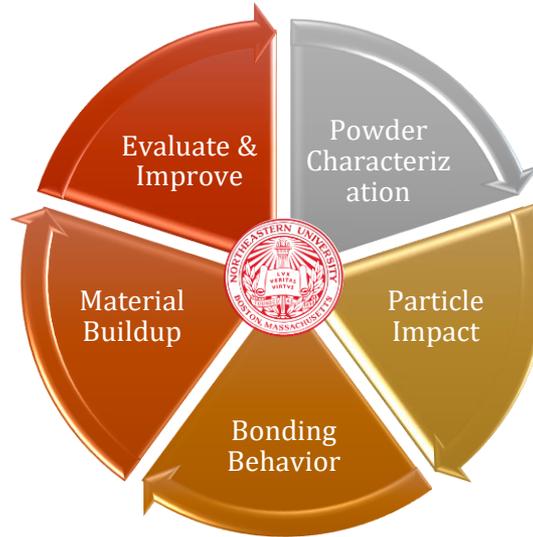
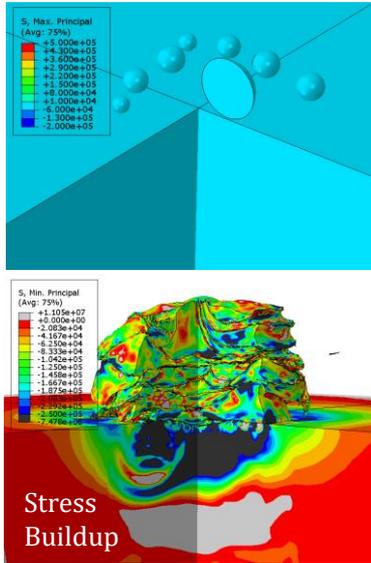
$$TE_{substrate} = 0.45 \cdot KE$$

$$V_c = 884 \text{ m/s}$$

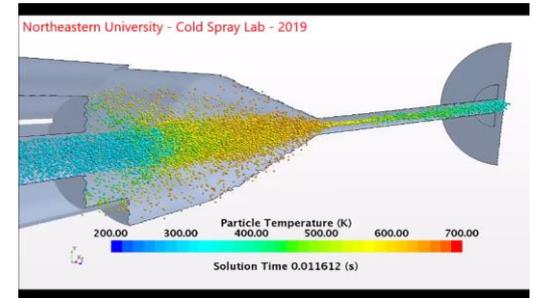
$$G^{Al} = 25 \text{ J/m}^2$$



Building on findings

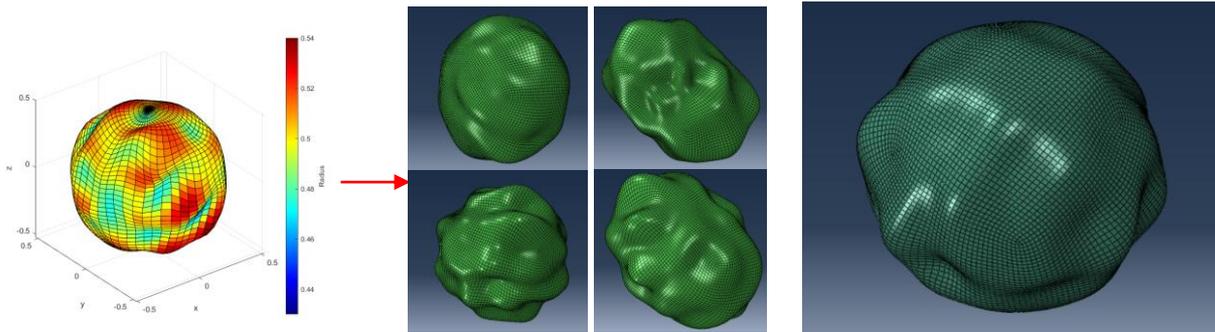


Refined particle shape analysis through measurement of 3rd dimension by interferometry



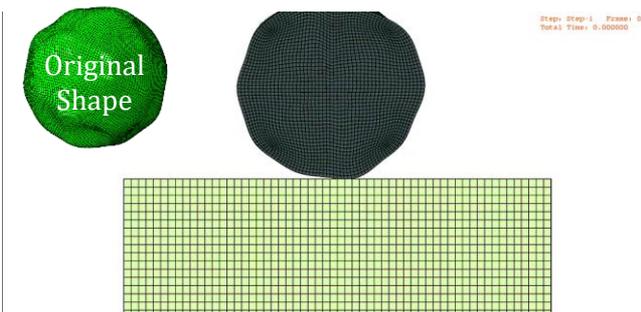
Shape Dependent Behavior

Sample impact FEM: Al-6061, 22 μm , 636 m/s



Script to generate parametrized shapes

Import into FEM Models





Thank you!
Questions

Acknowledgements

- This work was sponsored in part by the U.S. Army Research Laboratories, Aberdeen, MD under the grant number W911NF-15-2-0026 and W911NF-20-2-0024. Any opinions, findings and conclusions or recommendations expressed in this material are those of the author(s) and do not necessarily reflect the views of the U.S. Government.
- This work was sponsored in part by Herrick Foundation, Detroit, MI.