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The Use of Cold Spray Deposition for the Fabrication of NDE Qualification Samples

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Cold Spray NDE Samples



- Nuclear power plant based emphasis
- All NDE techniques require some level of Performance Demonstration using realistic flaw mockups (ASME Code and NRC requirements)
- Current technology for mockup fabrication is limited to surfaceconnected flaws (simulated service-induced corrosion)
 - Welded implants of fatigue cracks
 - EDM notches that are squeezed closed using hot isostatic pressure (HIP)
 - Lab-grown stress corrosion cracks (SCC)
- Undetected weld fabrication flaws are subsurface
 - Inclusions
 - Lack of fusion

False Positive UT Results



UT weld inspections rely on high sensitivity tip diffraction techniques

- Often, small internal, benign reflectors are mistaken for crack tips resulting in alarming false positive crack calls
- One instance misinterpreted data to show a 360-degree very deep crack
 - NRC issued potential shutdown orders for 12 operating plants
 - Industry impact was in the \$100s M



Undetected Near Surface Flaws



- Occasionally welding flaws exist in the near subsurface zone and are missed by the final penetrant testing (PT)
- The remaining ligament can be ruptured over time by thermal and mechanical stresses
- Exposing subsurface welding inclusions to high temperature water creates a highly caustic environment
- Cracking has resulted in primary system leakage
- Industry impact was in the \$100s M



Cold Spray Mockups



- The primary system pressure boundary in a nuclear plant is comprised of either stainless steel or high nickel alloy material
- Coating powders selected were
 - 316 stainless steel
 - Inconel 625 (annealed and non-annealed)
 - Substrate was 304 SS
- Samples were designed to
 - demonstrate the ability of UT to detect and distinguish subsurface flaws
 demonstrate that eddy current testing (ET) could detect near subsurface flaws

316 SS Sample



Side View: Two plates welded together with the seam simulating a subsurface flaw Top View: Three bands of thicknesses ranging from 0.7 to 1.5 mm nominally





316 SS Coating Thickness and Surface Contour (Ultrasonic Microscope)





³¹⁶ SS Coating Thickness

Differential Probe (0.12" Footprint)



400 kHz Flaw Detection

200 kHz Flaw Detection



ET Response at Various Coating Thicknesses



	Pk-Pk M	400 kHz % of Ref	Φ	Pk-Pk M	Φ	200 kHz % of Ref
Calibration	852.4	N/A	196.0	1412.9	N/A	195.1
Region 1	357.9	42	252.5	950.8	68	237.1
Region 2	180.4	21	290.1	494.5	35	265.1
Region 3	374.8	44	257.0	846.6	60	242.2
Region 4	N/A	N/A	N/A	N/A	N/A	N/A



- Small footprint probe used to accommodate actual part geometry
 - Larger probes do better for subsurface flaws
- Objective of detecting planar flaws up to 1 mm below the surface was met
- The cold spray 316 SS coating closely mimicked the ET properties of plate material for this application
- Signal attenuation and phase delay provided an indirect measurement of apparent bulk conductivity
 - This was not the intent of this study and surface roughness was too high to make accurate quantitative measurements
- Can we use ET measurement of "apparent conductivity" to assess coating quality?

ET "Spectroscopy"



- Work performed at Wright-Paterson AFB addressed using ET to measure "apparent conductivity" at several test frequencies
 - Application was for residual stress measurements after peening in high Ni alloys
- A similar approach is being studied to assess cold spray coating properties
 - This effort is just getting started
- Alloys of interest are Inconel 625 and SS 316

Conductivity Mosaic Absolute Pancake ET Probe



- Data collected with 4 frequencies (1.5, 1.0, 0.75, & 0.5 MHz)
- Balanced on Alloy 600 conductivity sample
- Scan and index resolution of 0.050"



Absolute Pancake Data – Conductivity Mosaic



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Sample Order from Left to Right:

- Inconel 600
- Inconel 625
- Inconel X750
- Incoloy 800
- Incoloy 825
- Nickel 200





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Inconel 625 Cold Spray Coating Scan

- Data collected using same setup from conductivity mosaic
- Scan dimensions: 5.0 x 2.4"





UT Scanning Arrangement



- Probe was placed on the smooth substrate surface
- 45-degree shear wave and 60- degree longitudinal waves used
- Coating surface contour satisfied ASME requirement for UT (<0.8 mm variation over 25 mm)
- Due to relatively thin cross section, 5 MHz used



45 Degree Shear Wave Results



0.5 mm coating thickness: no discrimination from backwall



1 mm coating thickness: barely separable signals



45 Degree Shear Wave Results



Conclusions

- Subsurface determination is possible for ligaments with a minimum thickness somewhere between 1.0 and 1.5 mm
- This corresponds to approximately 2 wavelengths
 - This result is wavelength dependent, so lower frequencies would require a correspondingly thicker ligament

1.5 mm coating thickness: clearly separable signals



60 Degree Longitudinal Wave Results



0.5 mm coating thickness: no discrimination from backwall



1.0 mm coating thickness: no discrimination from backwall



60 Degree Longitudinal Wave Results



Conclusions

- The longer wavelength of the longitudinal wave requires a greater ligament thickness for discrimination of subsurface flaws
- For most actual field applications, a discrimination level of 2 mm would be adequate
- Longitudinal waves are actually the preferred method for high alloy welds

1.5 mm coating thickness: slightly separated signals



Future Work with UT



Bond quality assessment will be investigated

- Conventional high frequency 0 degree UT has been shown to be ineffective
- Contaminants that cause weak bonds also act as ultrasonic couplant and transmits the sound
- Alternate wave modes are being studied
 - Interface waves that are only produced at well bonded interfaces of similar metals
 - Layer modes (one free surface and one well bonded surface)