





Cold Sprayed Self Lubricating Coatings

Cold Spray Action Team Meeting June 18-19, 2014

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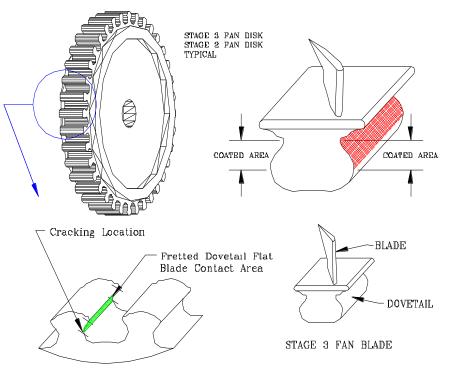
Presentation Outline

- Background
- Preparation of Coating Materials
- Nickel Encapsulation
- Cold Spray Deposition
- Coating Evaluation
- Summary



Objective

To create and apply self-lubricating coatings that will improve wear and mechanical properties of mating surfaces.



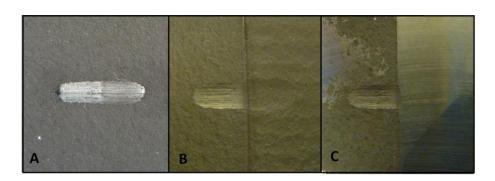


Background

- Solid lubricant are used in several applications
- Once the solid lubricant is depleted, the wear rate greatly increases
- Solid lubricant particles can be encapsulated in metal
- Composite powder can be deposited on the wear surface
- Thermal spray would melt the metal and solid lubricant
- Cold Spray can deposit the encapsulated powders without melting or destroying the powders

PENNSTATE Self-lubricating Coatings – Background

- Composite materials (Encapsulated solid particles)
- Can be used to improve surface properties
 - Reduce the coefficient of friction
 - Improve wear resistance
- Functionally gradable
- Repairable



Partially repaired wear damage of hBN-Ni coating on Aluminum ⁵



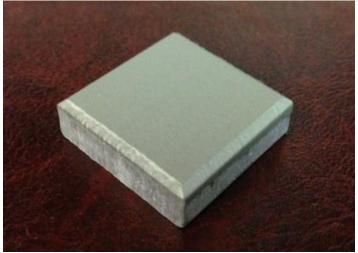
Process Optimization

- Size of solid lubricant
 - Minimize diameter of the coated particle
- Encapsulation process
- Ni coating
 - Minimum thickness to prevent fracture of the lubricant
 - Minimum thickness to ensure plastic deformation and bonding
- Velocity
 - Deposition efficiency
 - Good adhesion
- Temperature
 - Velocity
 - No damage to the solid lubricant particle



Preparation of Coating Materials

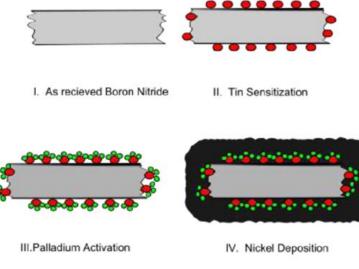
- Self-lubricating coating material composed of :
 - Hexagonal Boron Nitride (hBN) (lubricant)
 - Nickel (matrix)
- Nickel was selected due to:
 - Relatively high temperature capability
 - Potential for work hardening



Cold Spray coating on Al-6061 substrate PENNSTATE

Preparation of Coating Materials

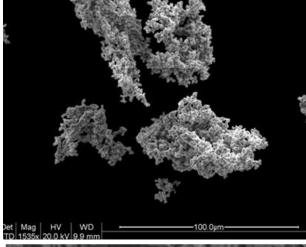
- hBN-Ni powder preparation:
 - Activate hBN surface with (Sn and Pd Chloride)
 - Ni deposited onto hBN particles via electroless Ni plating
- Thick Ni encapsulation via two-solution electroless Ni plating
 - Required for Cold Spray deposition
 - Better wear resistance and excellent corrosion behavior
- Mix hBN-Ni with Ni

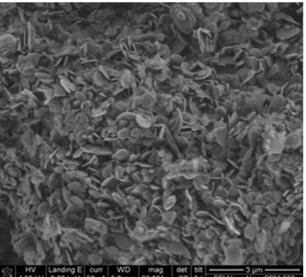




Preparation of Coating Materials

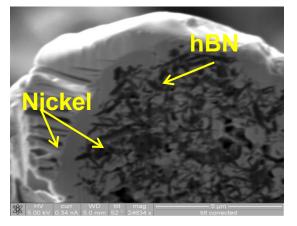
• Particles of hBN encapsulated with Nickel

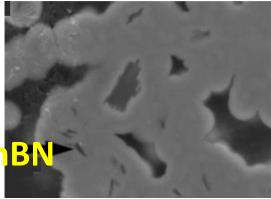




Coated hBN Particles

hBN Particles



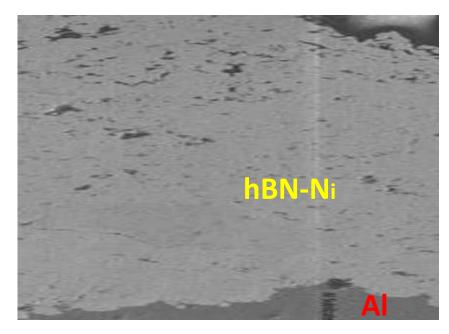


hBN encapsulated with Nickel particles (1 wt% hBN) 9

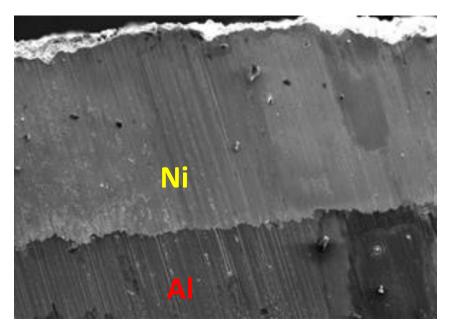


Application of Coating

• AI 6061 coated with hBN-Ni and Ni



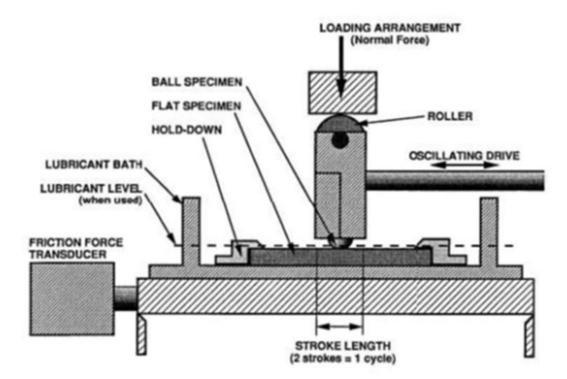
hBN encapsulated with Ni

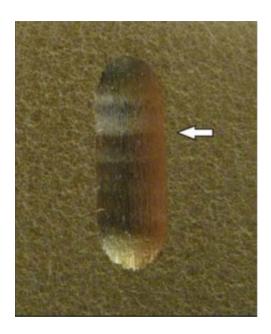


Pure Ni



• Friction Test





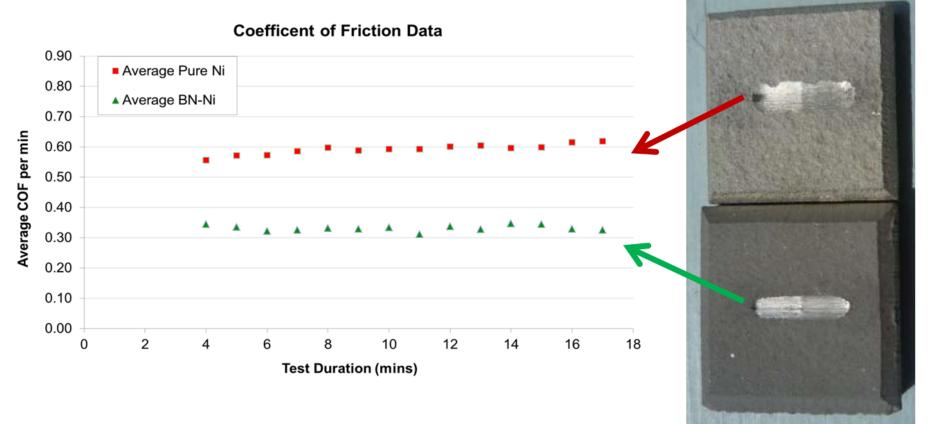
wear scar after the test

Reciprocating wear test (ASTM International 2008)



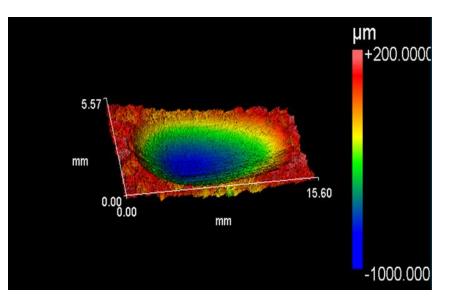
Evaluation of Coated Surfaces

 Comparison of the coefficients of friction of the Ni and hBN-Ni

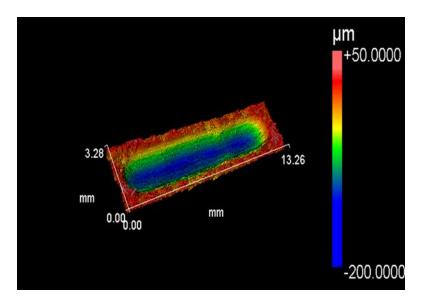




• Profilometry depth profiles



Coated with Ni



Coated with hBN-Ni

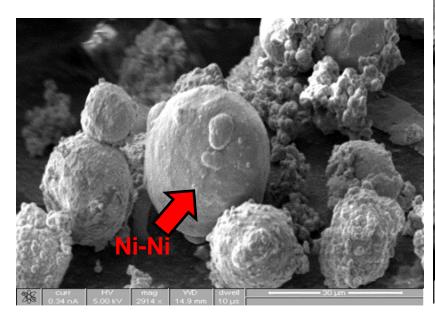


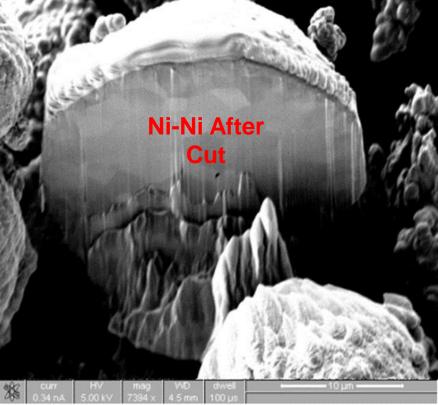
• Wear scar volume reduced by an order of magnitude

Material	Wear volume
AI 6061 coated with Ni	23.80 mm ³
AI 6061 coated with hBN-Ni	2.13 mm³



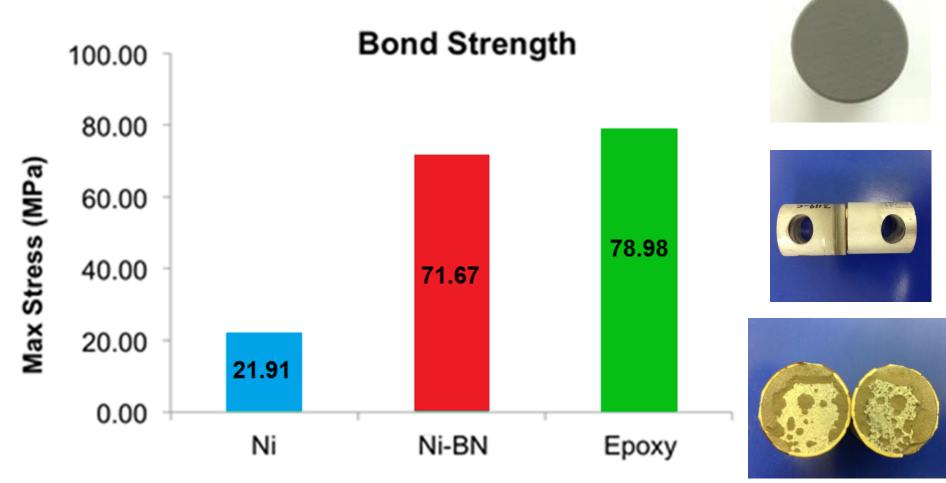
- Ni powder encapsulated with Ni
- Samples prepared using focused ion beam (FIB) milling







• Improved bond strength of hBN-Ni coating

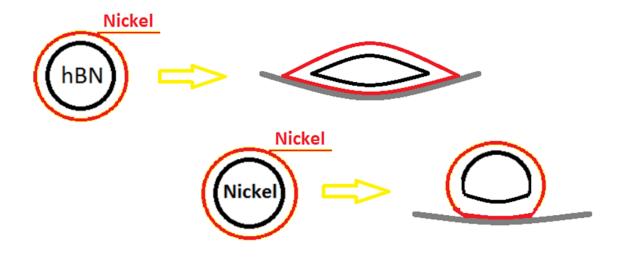




Particle Deformation

- hBN-Ni has good adhesion strength
- Ni-Ni coating has poor adhesion strength

Initial ductility and work hardenability of nickel





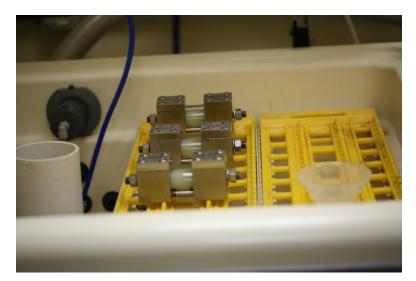
Conclusions

- Cold spray process and nickel encapsulation of hBN (hBN-Ni) allowed the creation of composite coatings with a metal matrix and uniformly dispersed solid lubricant particles
- hBN-Ni coatings:
 - Significantly higher bond strength
 - Markedly reduced coefficient of friction
 - Improved wear resistance (10x)
- Coatings were both repairable and functionally gradable
- Low temperatures of cold spray process also allows unique material and coatings (metal on glass, metal on plastics etc.)

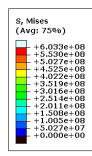


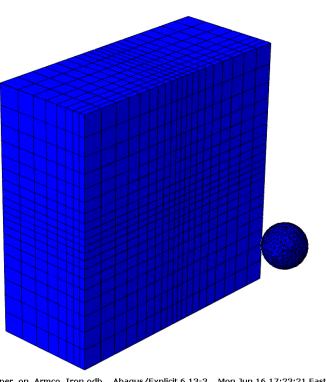
Stress Corrosion Cracking of Al-6061

- Wrought Al 6061-T6
- As Cold Sprayed
- Tensile tests for baseline following ASTM E8
- SCC following ASTM G49-85
- In process



FEM of a Cu particle impacting Armco Iron – 500 m/s





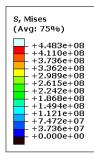


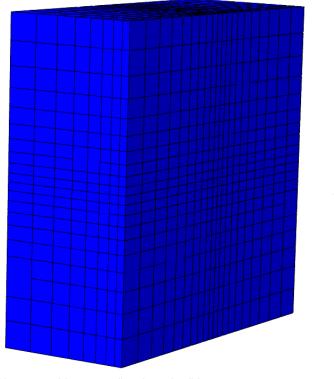
ODB: Copper_on_Armco_Iron.odb Abaqus/Explicit 6.13-3 Mon Jun 16 17:23:21 Eastern Daylight Time 2014

Step: Step-1 Increment 0: Step Time = 0.0 Primary Var: S, Mises Deformed Var: U Deformation Scale Factor: +1.000e+00 Step: Step-1 Frame: 0 Total Time: 0.000000

FEM of a CP AI particle impacting AI 6061-T6 – 500 m/s

Step: Step-1 Frame: 0 Total Time: 0.000000







ODB: Cold_Spray_Particle_Impact.odb Abaqus/Explicit 6.13-3 Mon Jun 16 17:11:45 Eastern Daylight Time 2014

Step: Step-1 Increment 0: Step Time = 0.0 Primary Var: S, Mises Deformed Var: U Deformation Scale Factor: +1.000e+00



THANK YOU