

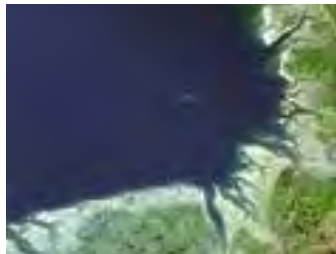
Systematic Tuning of Cold Spraying for Aerospace Applications

Thomas Klassen, K. Binder, M. Villa-Vidaller, F. Gärtner, T. Gartner, H. Assadi

Helmut Schmidt University, University of the Federal Armed Forces Hamburg
Helmholtz-Zentrum Geesthacht GmbH
Lufthansa Technik AG, Hamburg
Germany

CSAT2016, Worcester
June 21-22

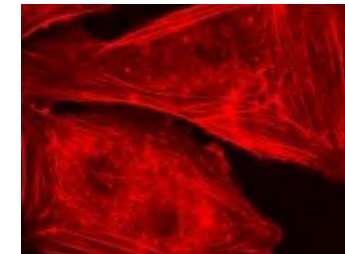
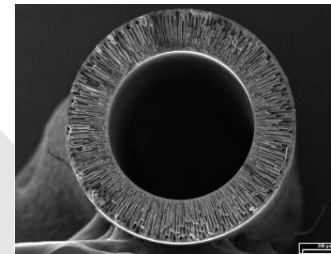
1/3 Coastal and Climate Research



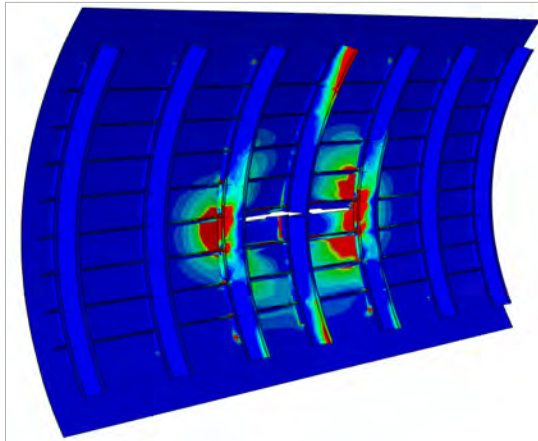
**Total budget
95 Mio €**

**Employees
850**

2/3 Materials Research for sustainable Energy and Mobility



Research on Novel Aircraft Structures and Manufacturing Technology



Theory

**Design,
Modeling & Simulation**



Characterisation

**Microstructure
and Residual Stress**

**Additive Manufacturing
and 3d Refurbishment**

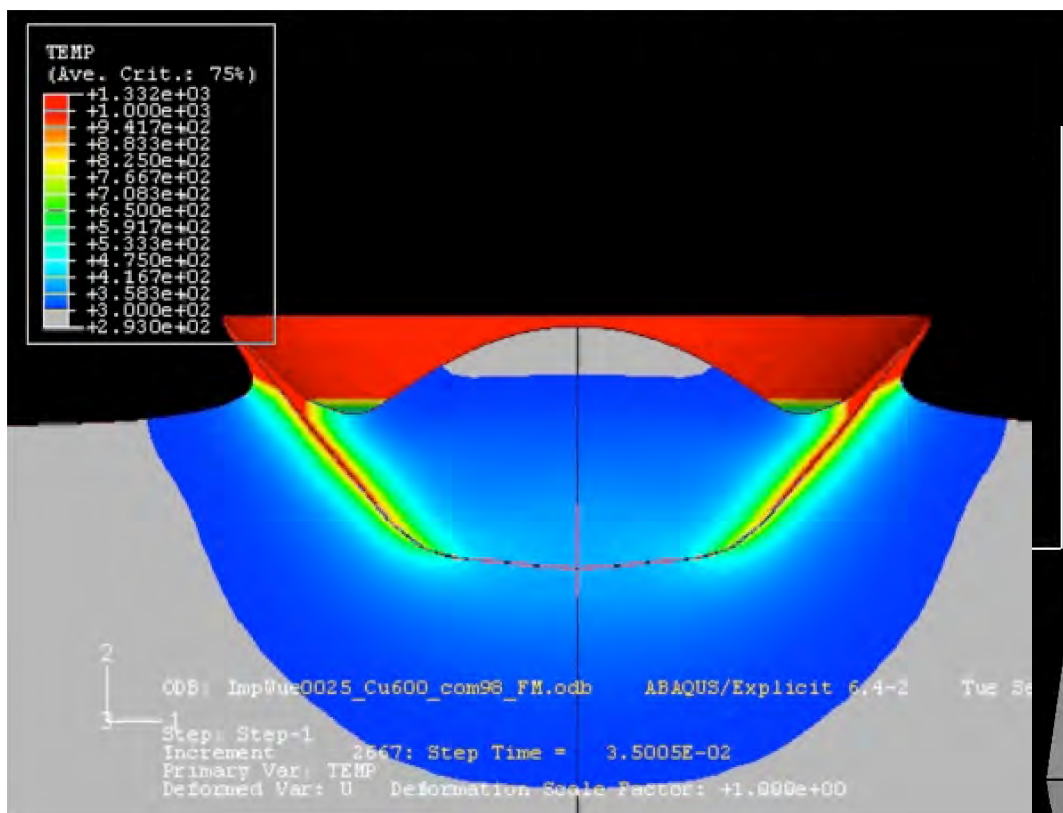
**Model Experiments
and Prototypes**

Kinetic Spraying: Basic Mechanisms

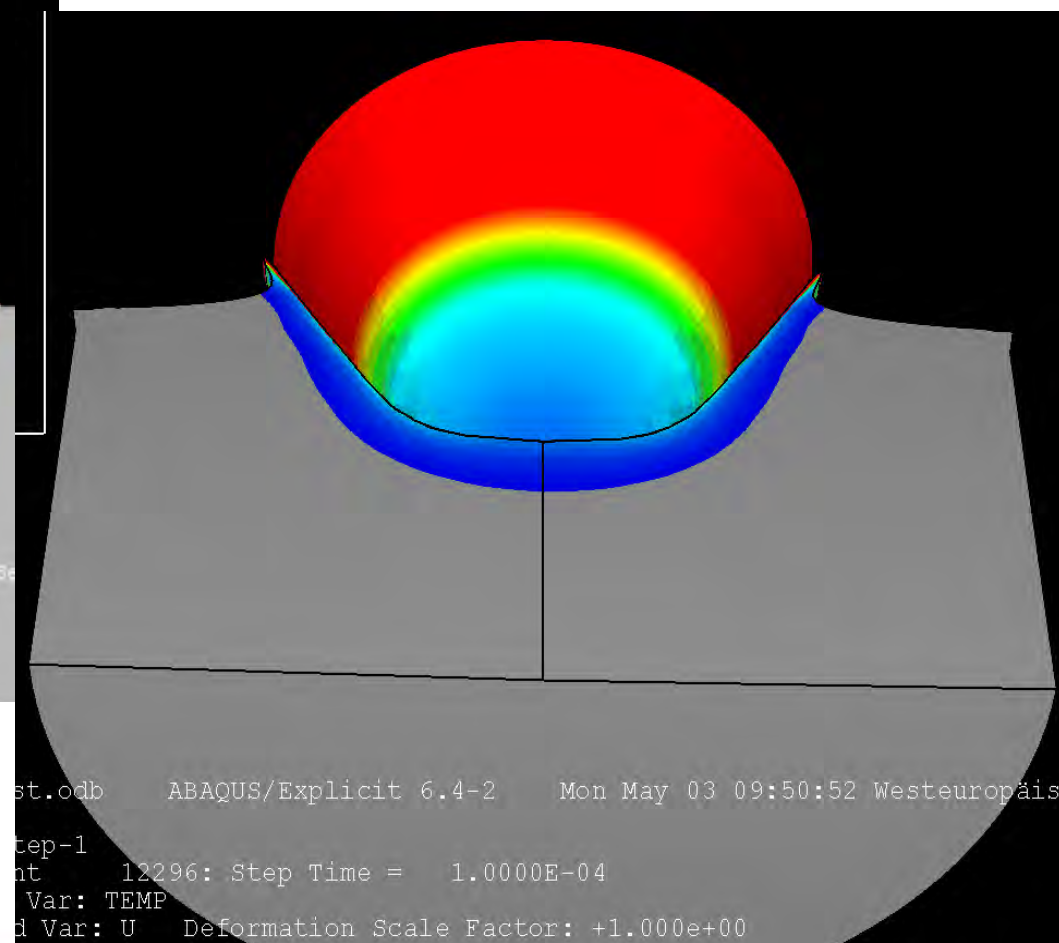
Particle Impact

temperature field showing thermal flow

25 μm , 600 m/s, 20°C, Cu

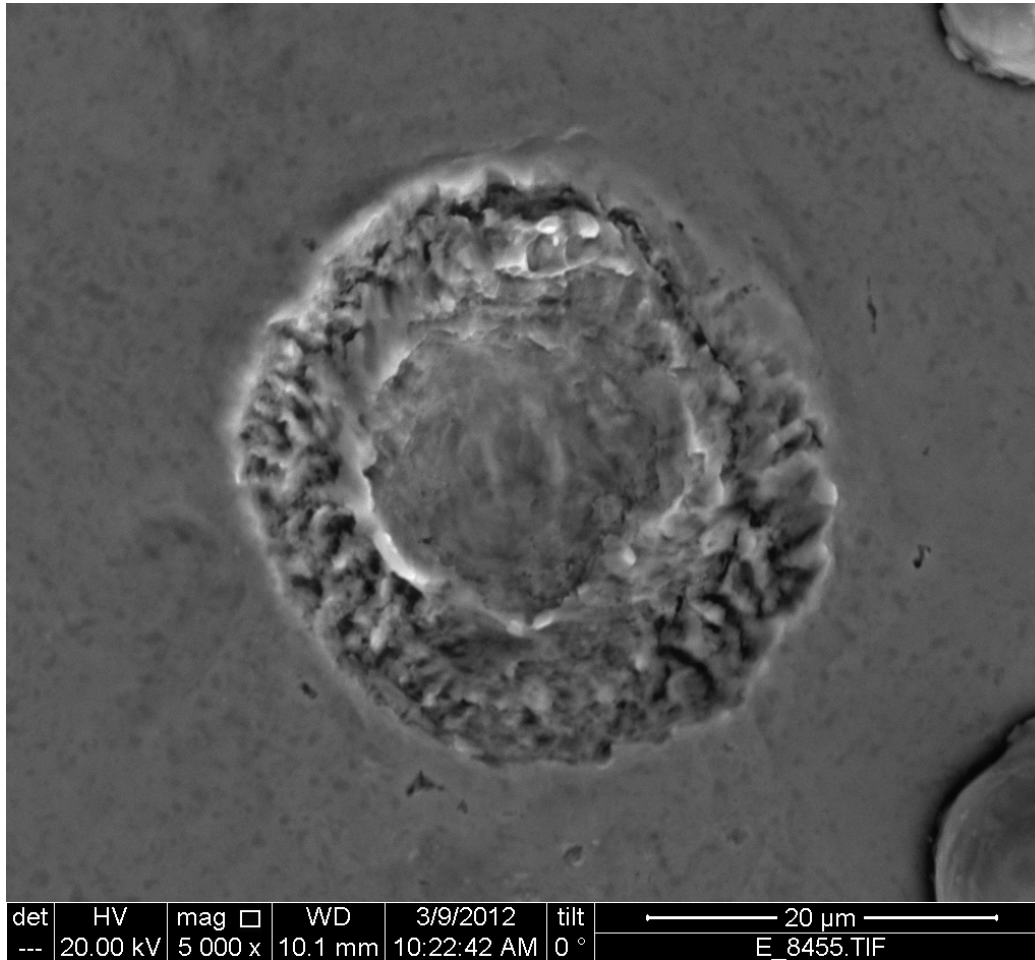


Area of Bonding



Single impact Ti-6Al-4V on Ti after cavitation

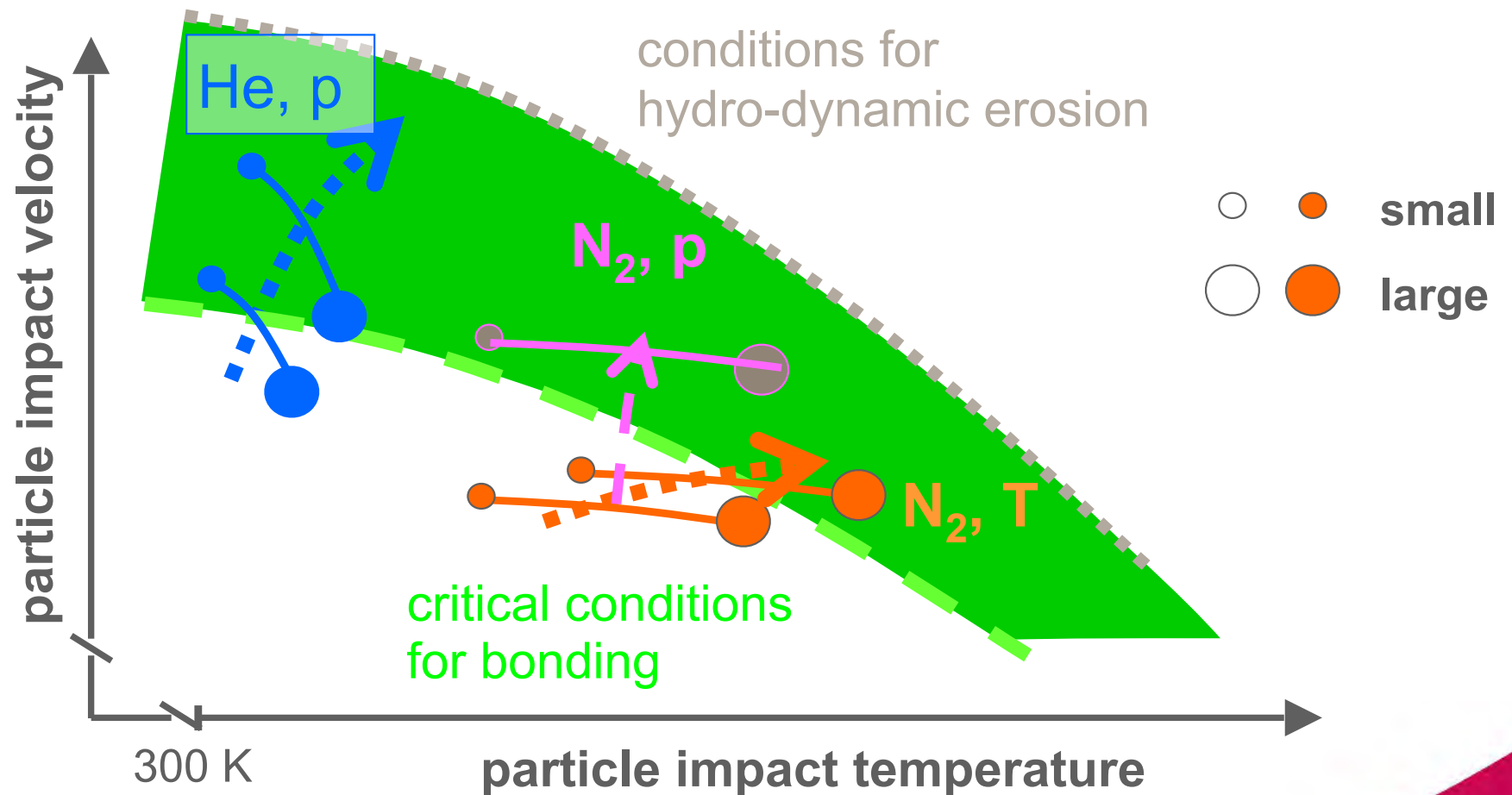
lost...



... and found



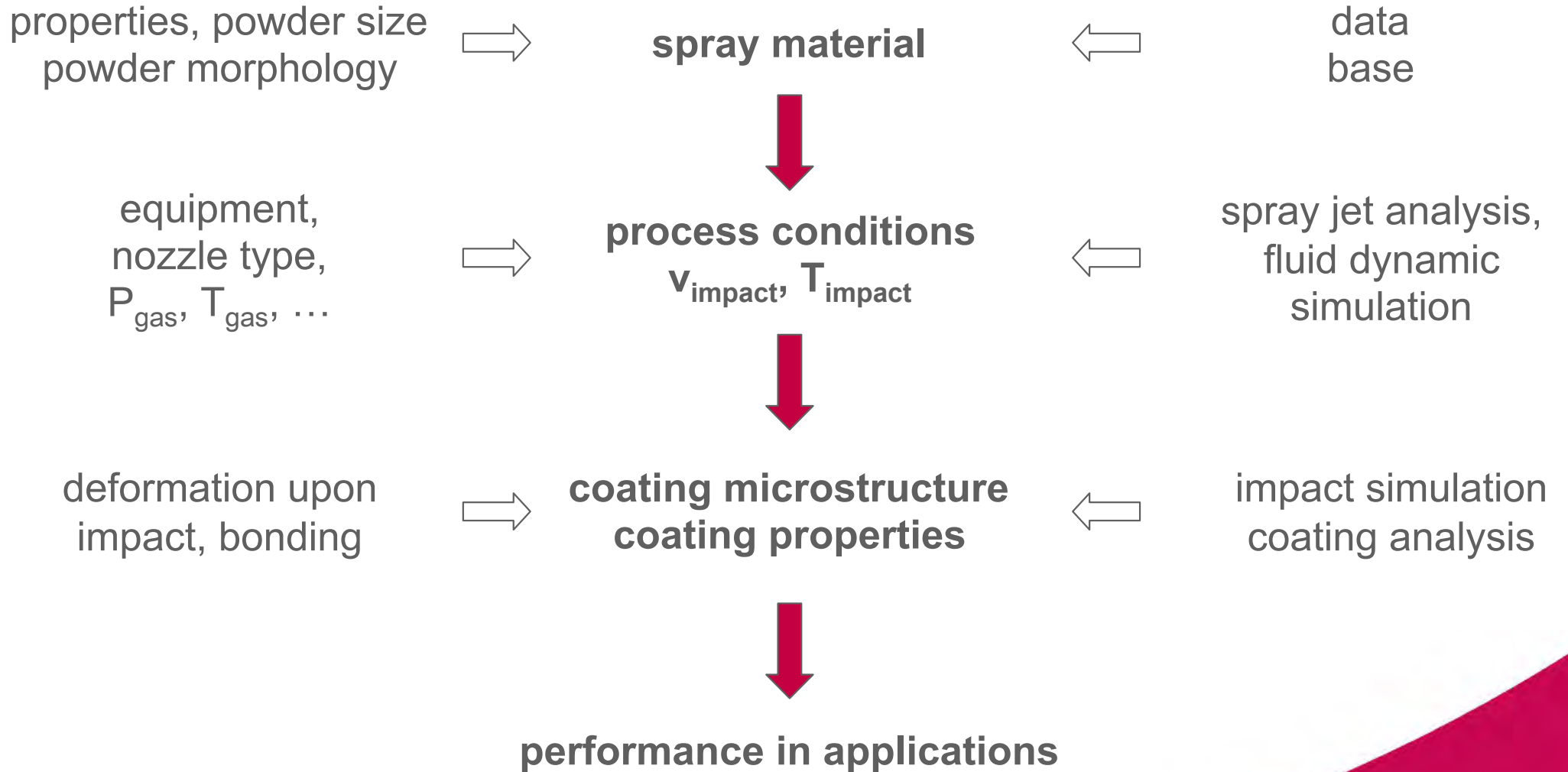
Process Improvements: Window of Sprayability



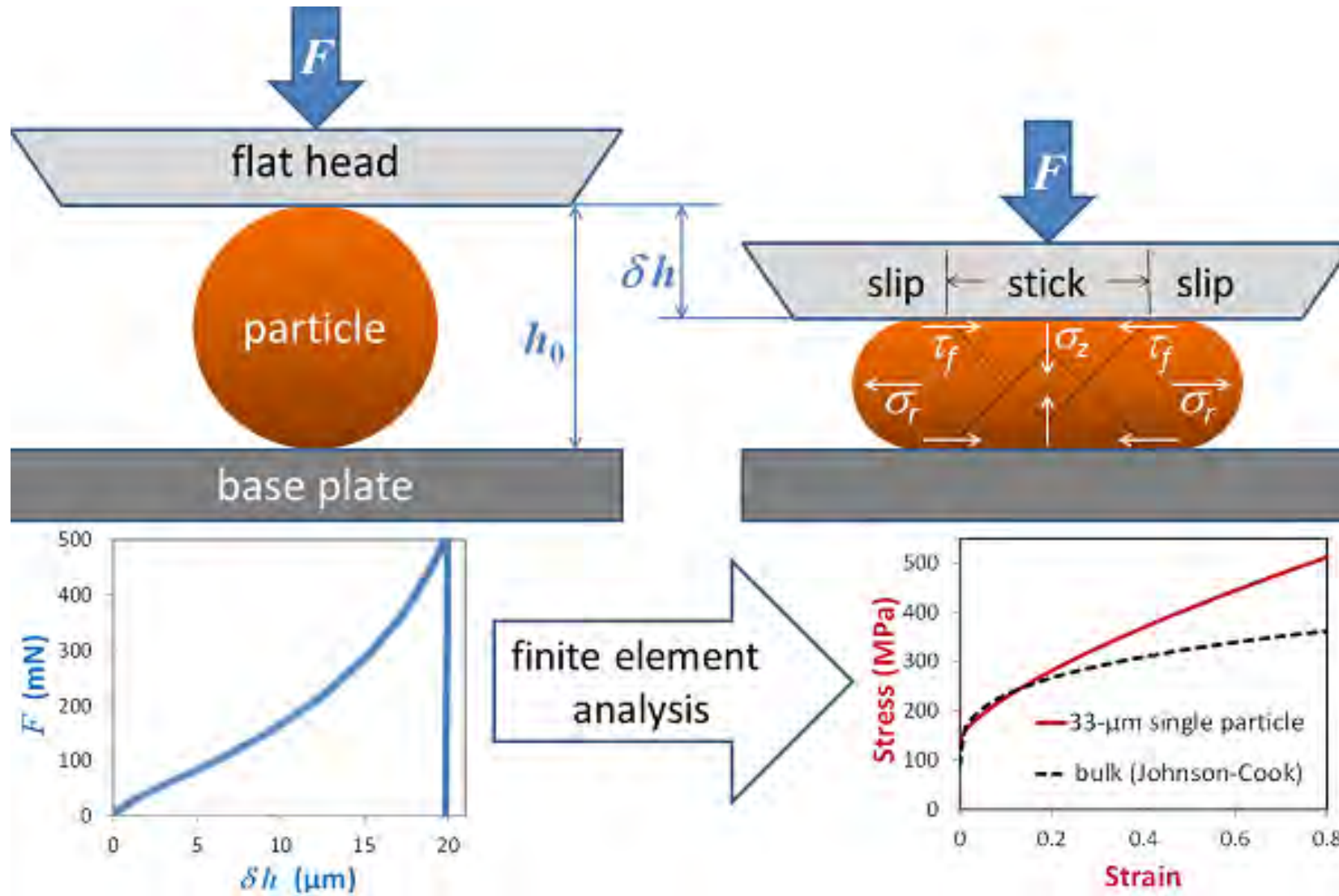
He route: very fast, **cold impact condition** (costly)

N₂ route: fast, **warm impact condition** (reactions?)

coating quality is predictable!

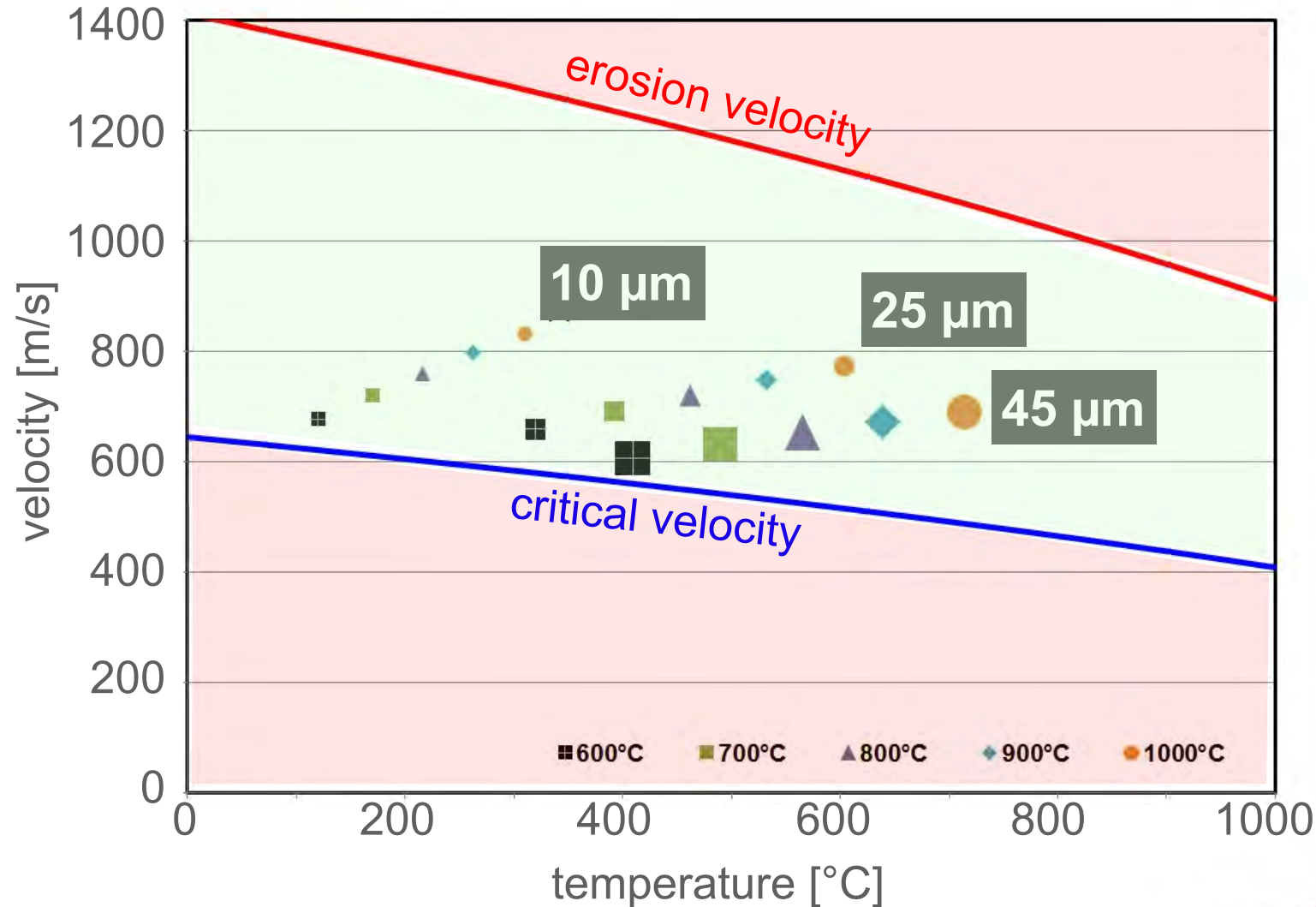


Powder development: single particle deformation



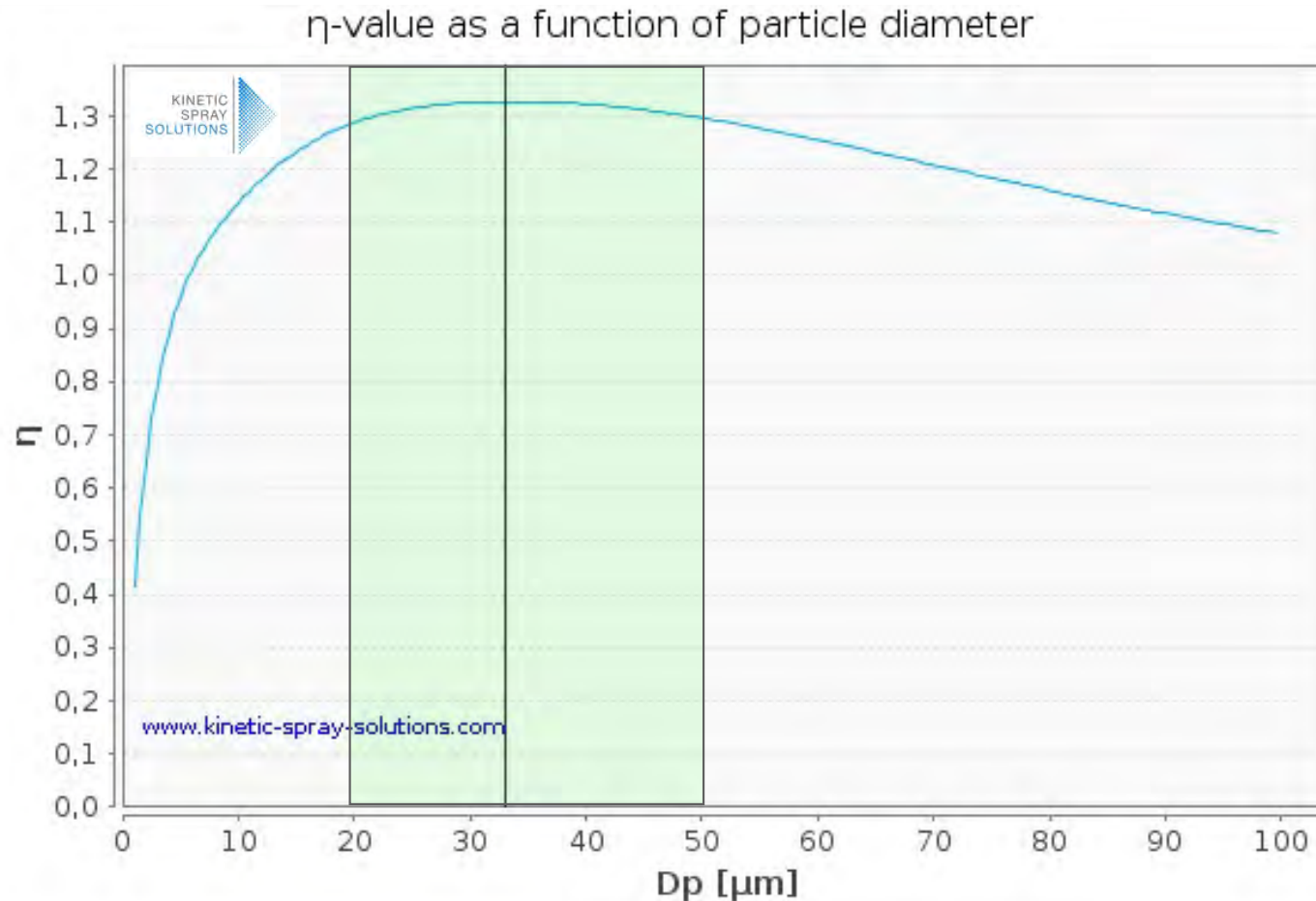
Kinetic Spraying: Titanium

Window of Deposition: Ti



materials properties \rightarrow window of deposition
process parameters \rightarrow impact conditions

Parameter selection: optimum Ti-powder sizes



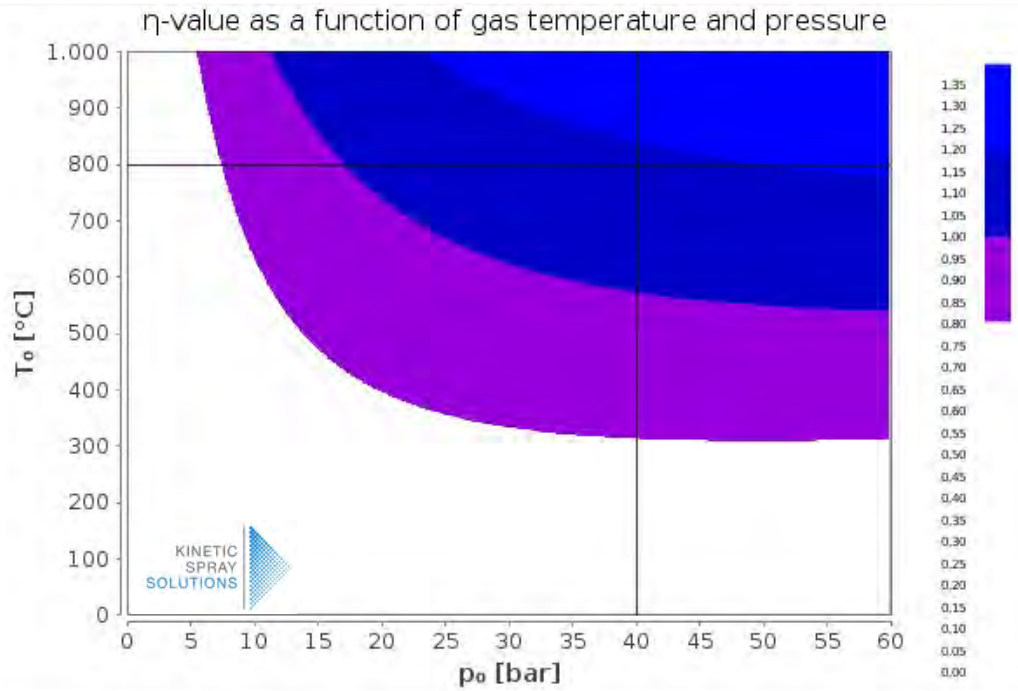
Nitrogen
nozzle 24,
 p_{gas} : 40 bar,
 T_{gas} : 1000°C

⇒ optimum size range: 20 – 50 μm ($D_{50} = 33 \mu\text{m}$)

Parameter selection

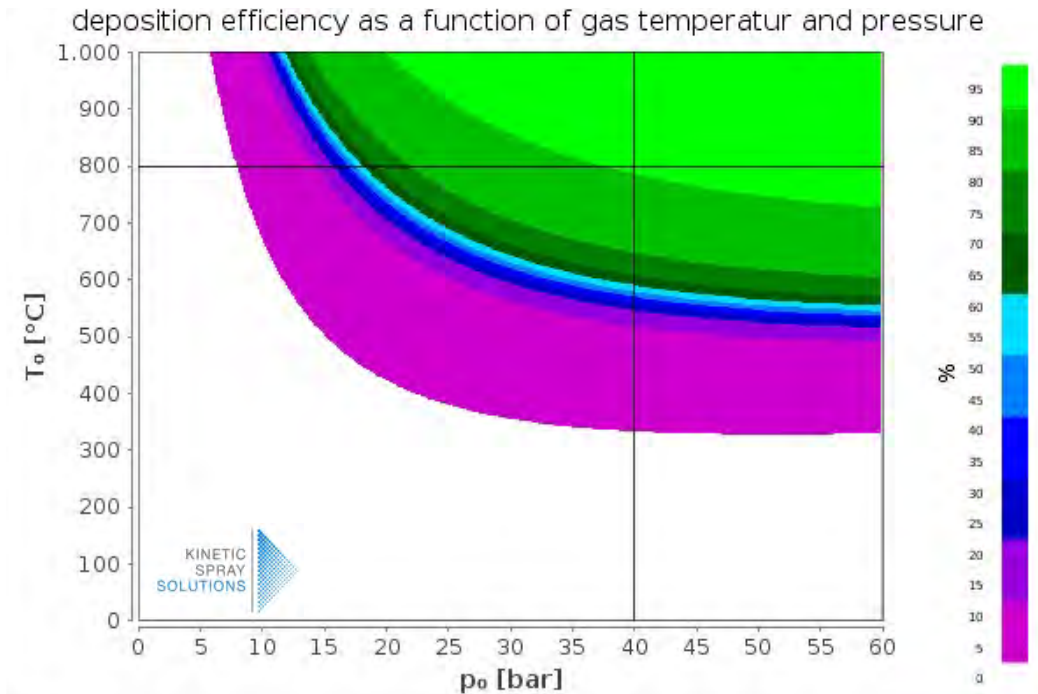
η , DE (gas pressure, gas temperature)

η



nozzle 24

DE



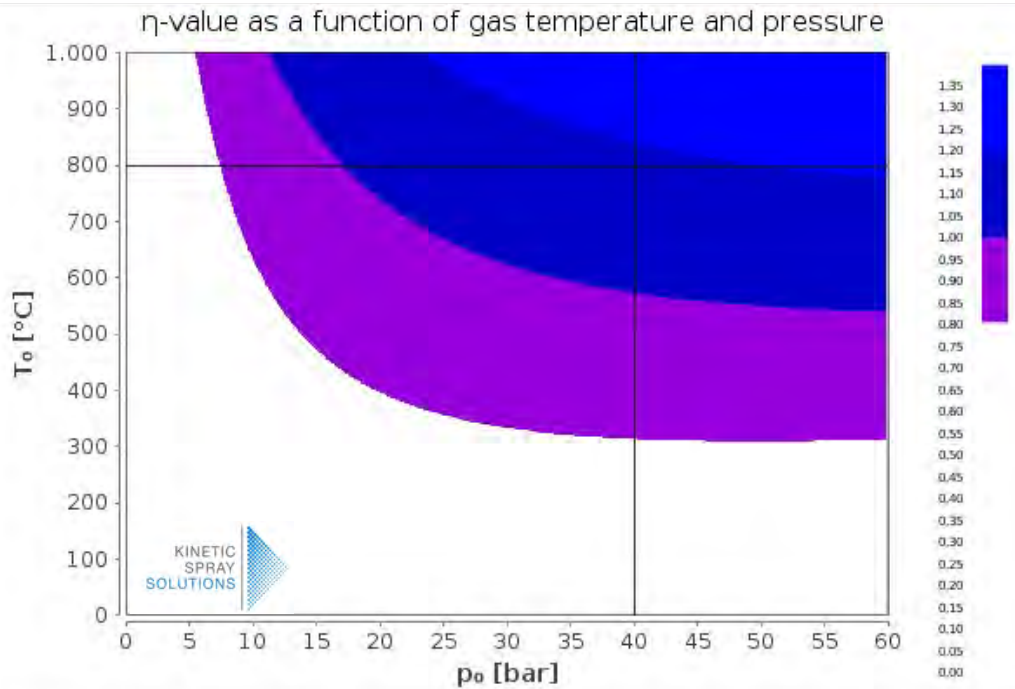
nozzle 24

→ saturation in DE: reached at $\eta > 1.2$;
 $p > 40$ bar, $T > 800$ °C

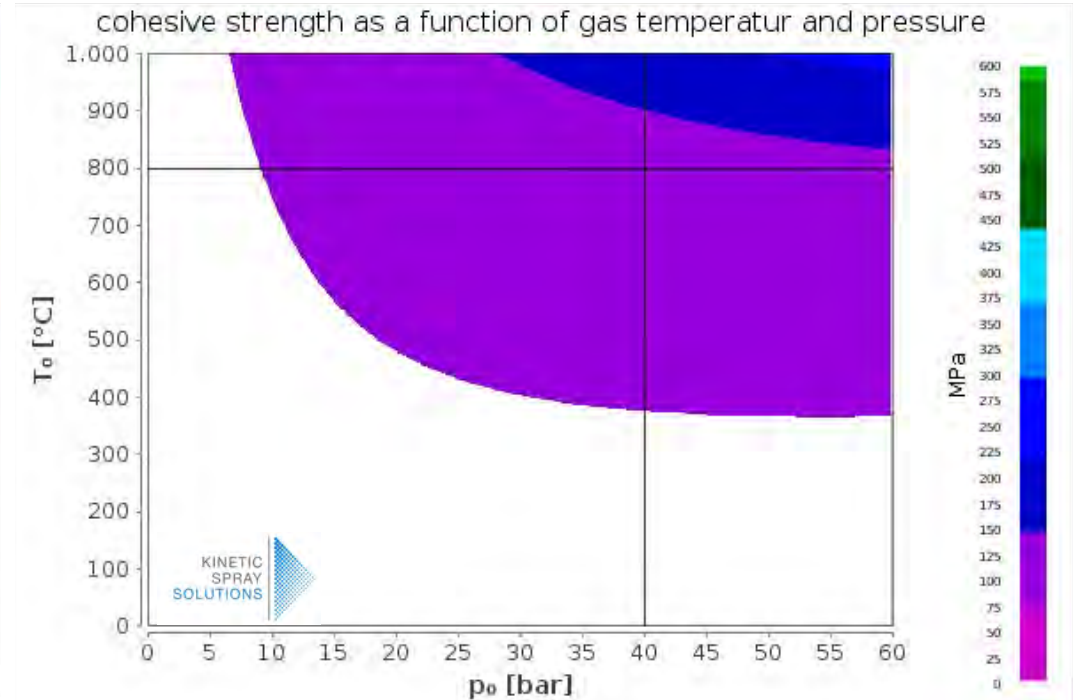
Parameter selection

η , UTS (gas pressure, gas temperature)

η



UTS



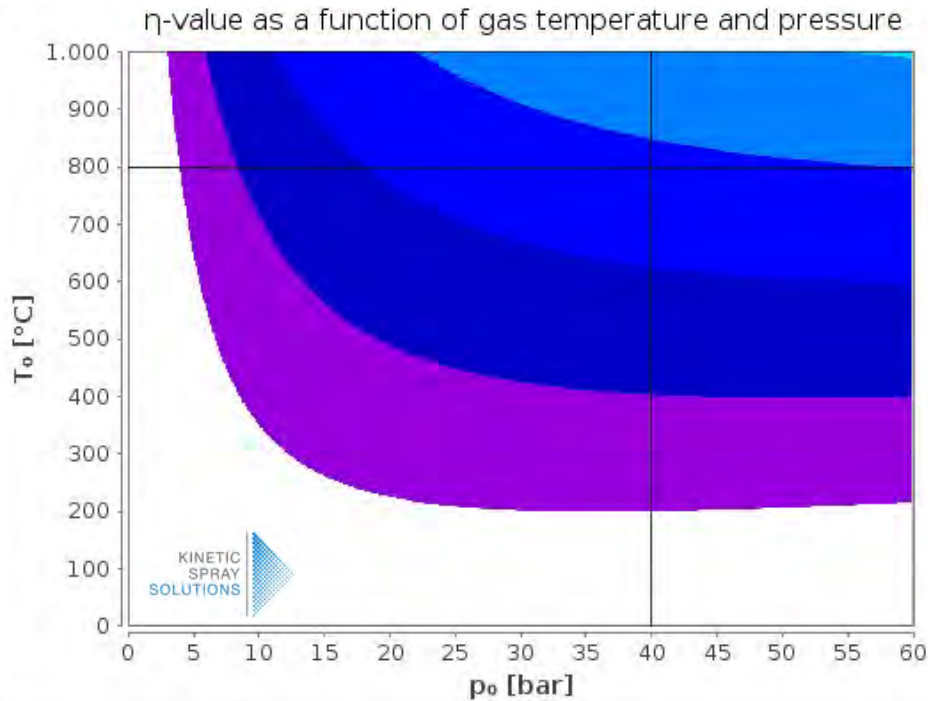
nozzle 24

→ strength > 220 MPa reached at $\eta > 1.4$,
here p_{gas} : 60 bar, T_{gas} : 1000°C

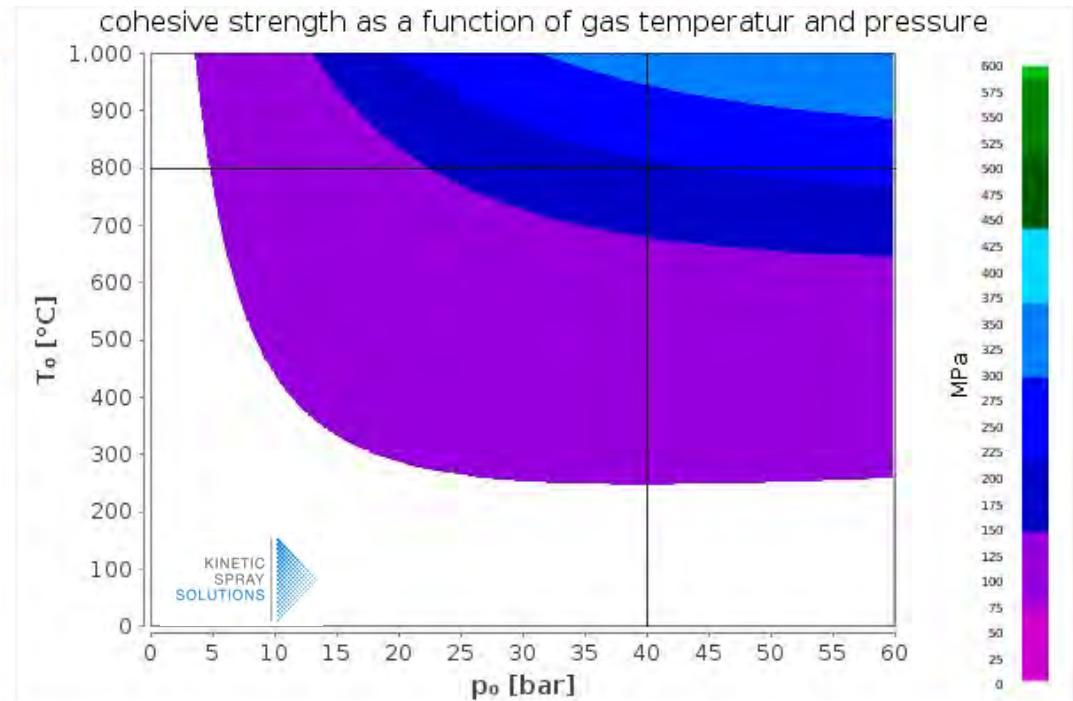
Parameter selection

η , UTS (nozzle selection)

η



UTS



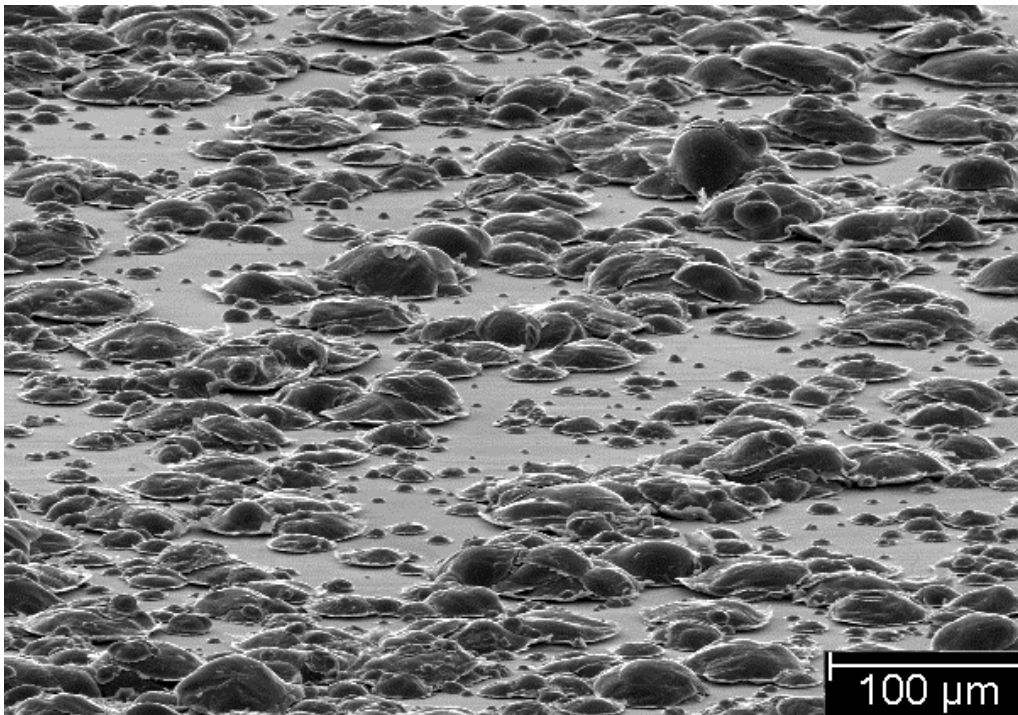
nozzle 50

→ strength > 300 MPa at $\eta > 1.5$,
 $p_{\text{gas}} > 50$ bar, $T_{\text{gas}} > 900^\circ\text{C}$

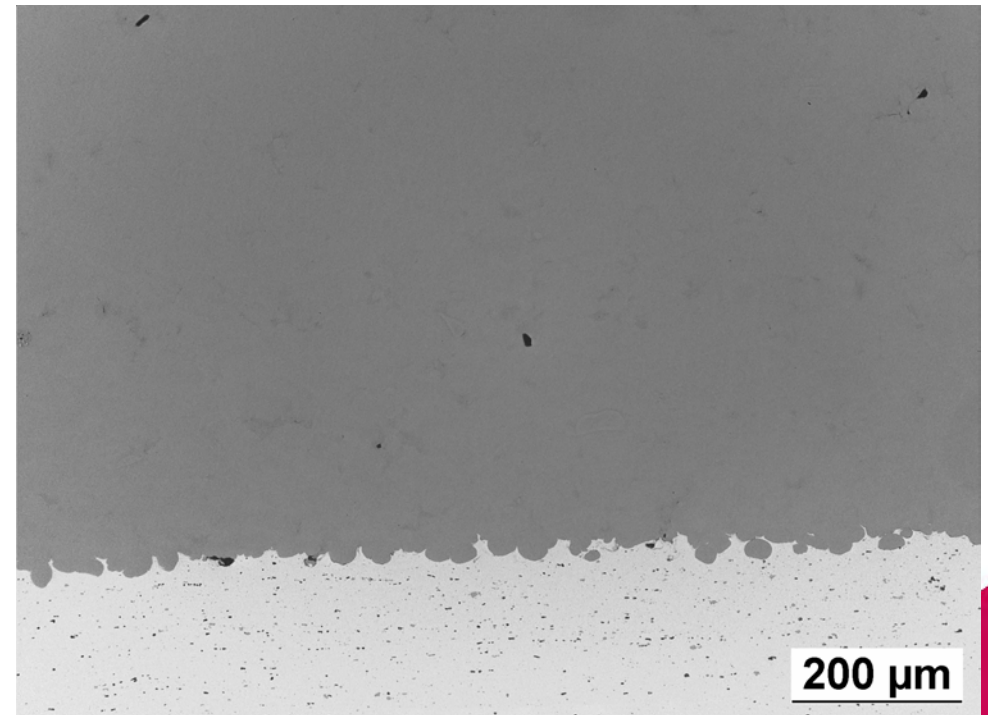
properties of cold sprayed Ti

Ti - Coatings: Microstructure

impact morphology

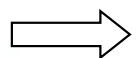
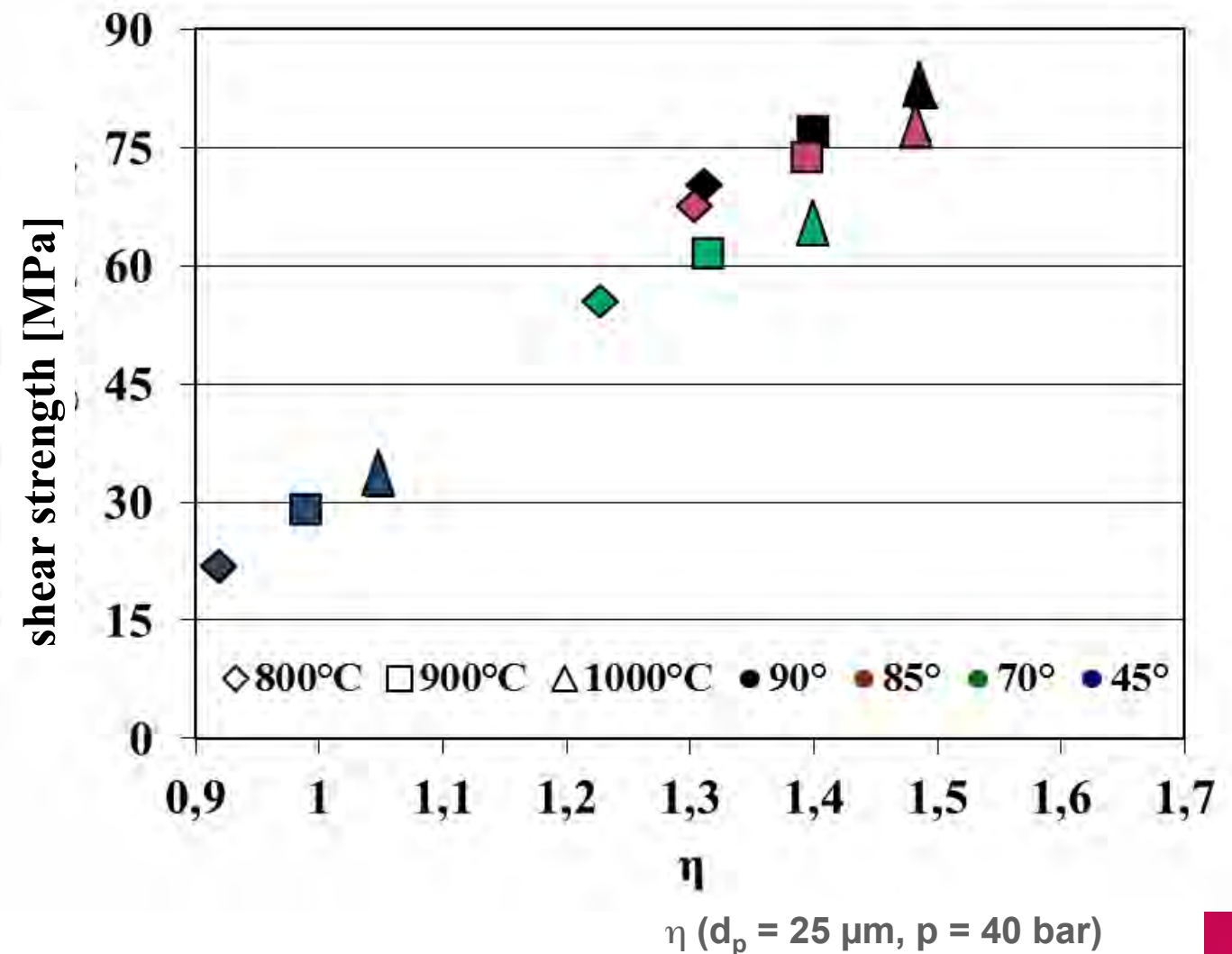
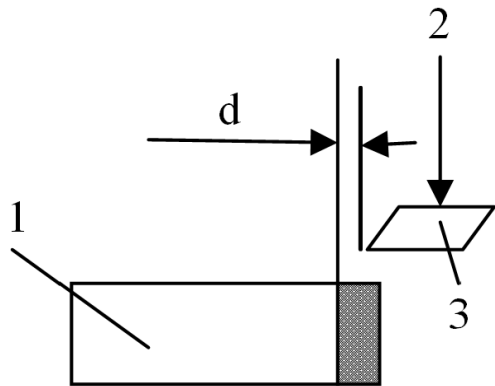


coating microstructure



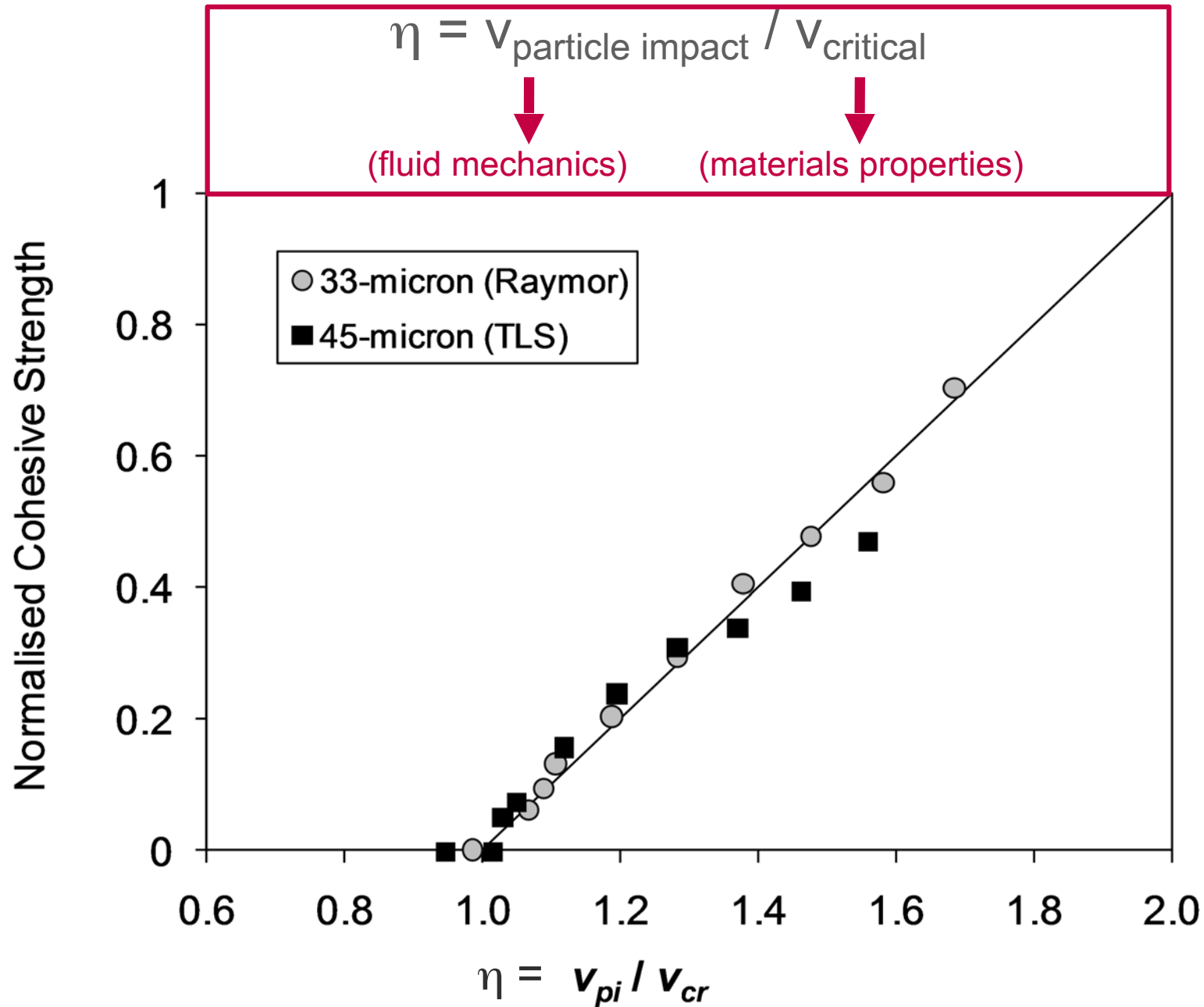
$$T_{\text{gas}} = 1000^{\circ}\text{C} \quad p_{\text{gas}} = 4 \text{ MPa}$$

Shear strength: η

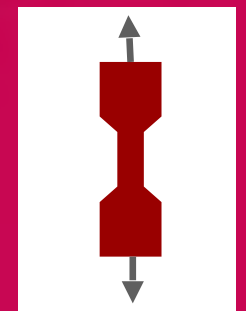
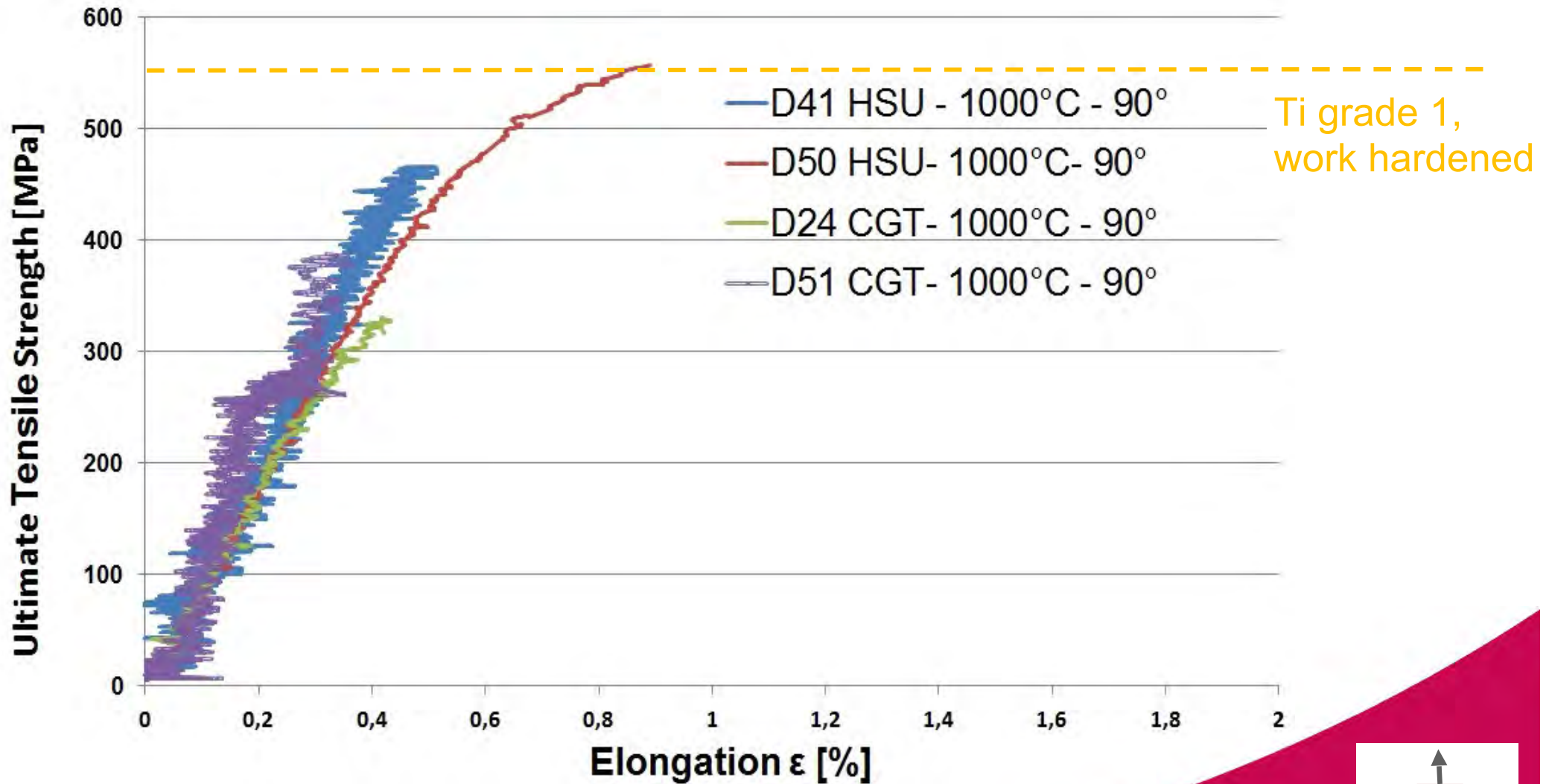


linear correlation with η

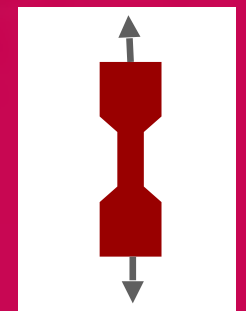
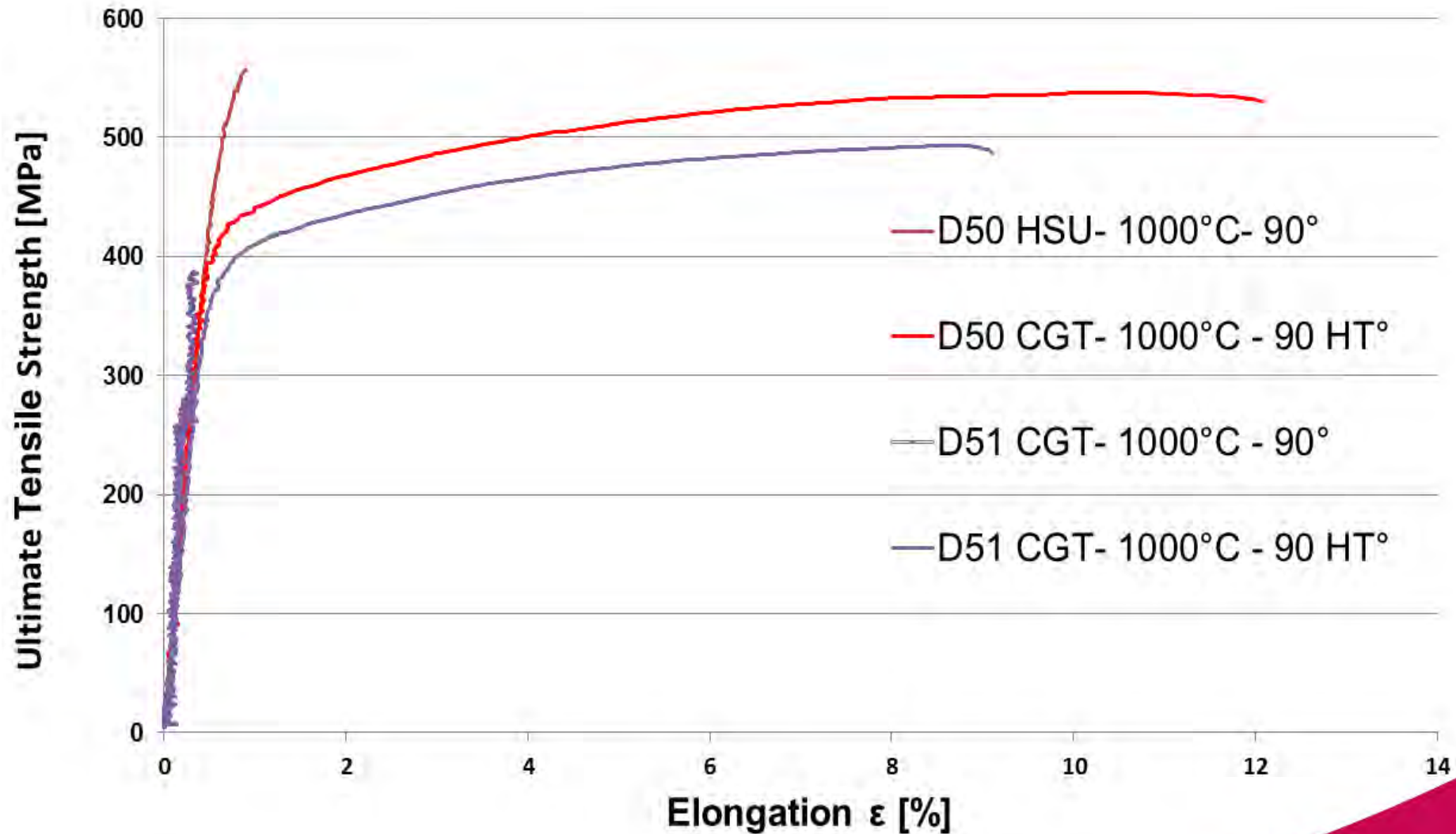
Cohesive strength: η



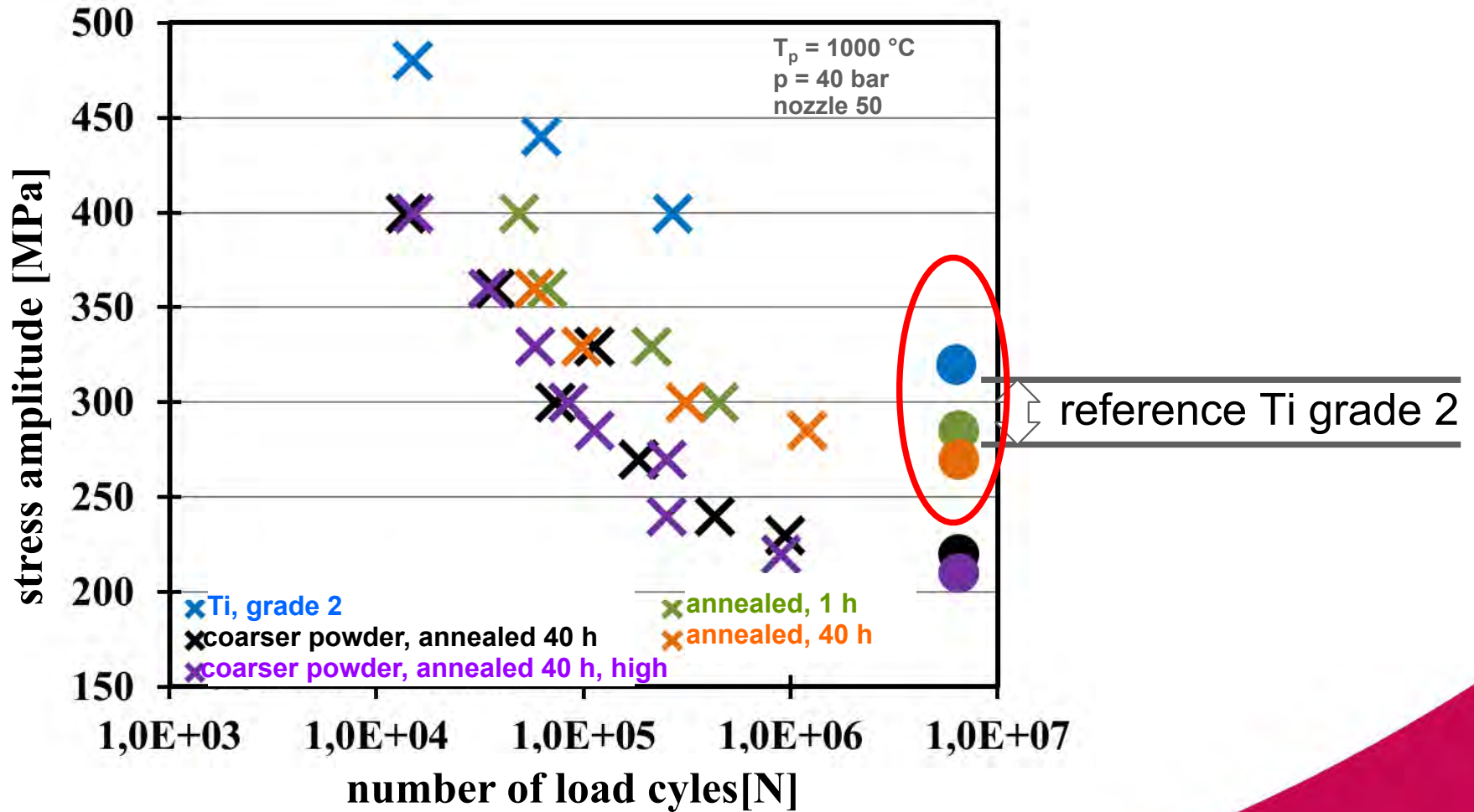
deposit strength and ductility: MFT-Test



deposit strength and ductility after annealing: MFT-Test



Fatigue strength similar to bulk Ti (grade 2)

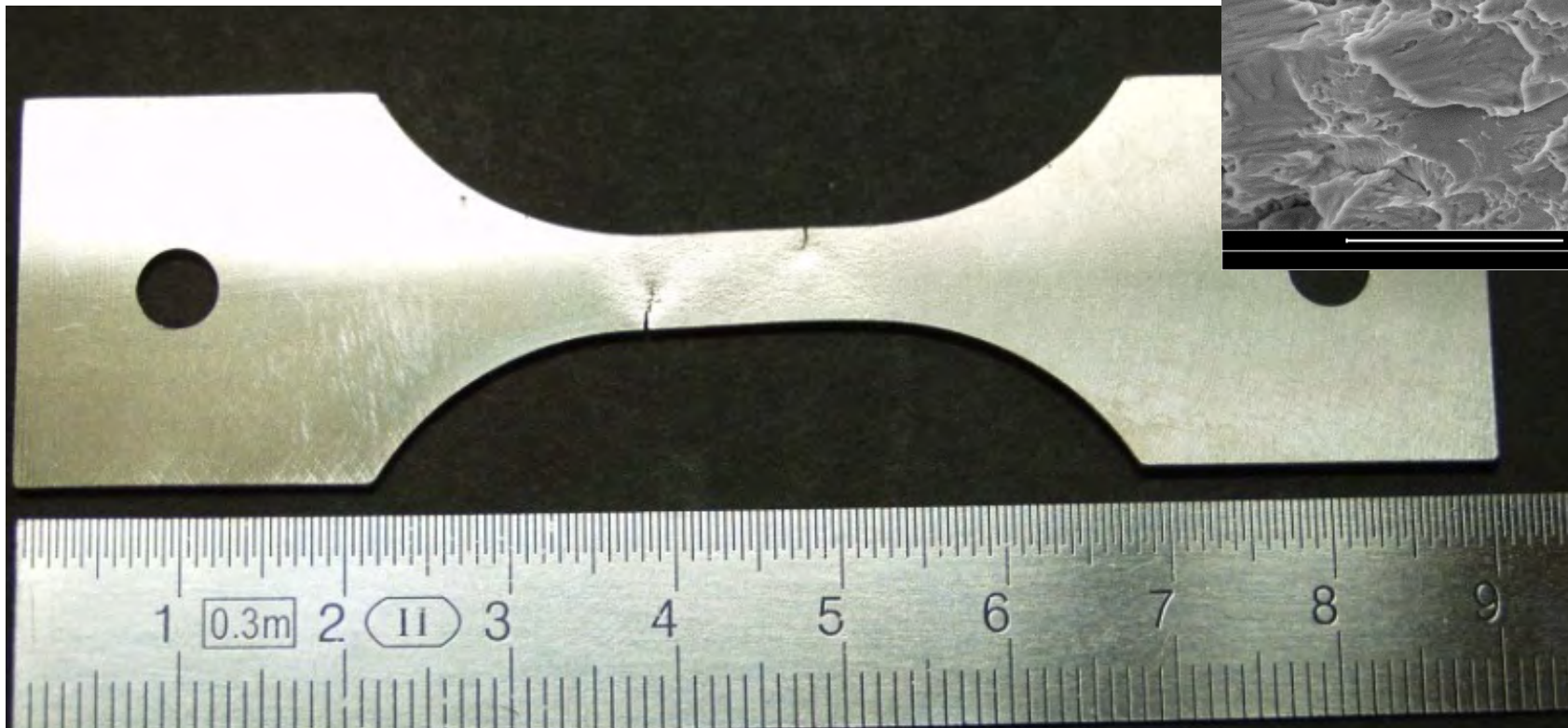


$R = \text{min. stress} / \text{max stress} = 0.05$
endurance limit: at $> 7 \times 10^6$ cycles

HSU Cold sprayed Ti samples show damage tolerance during HCF-testing

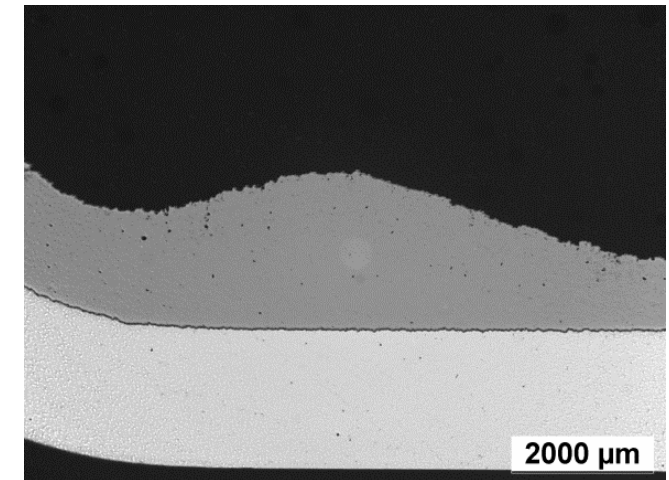
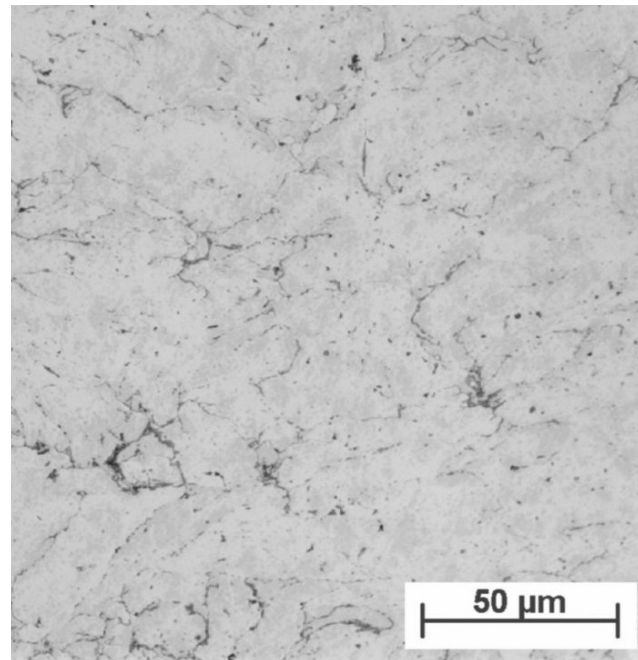
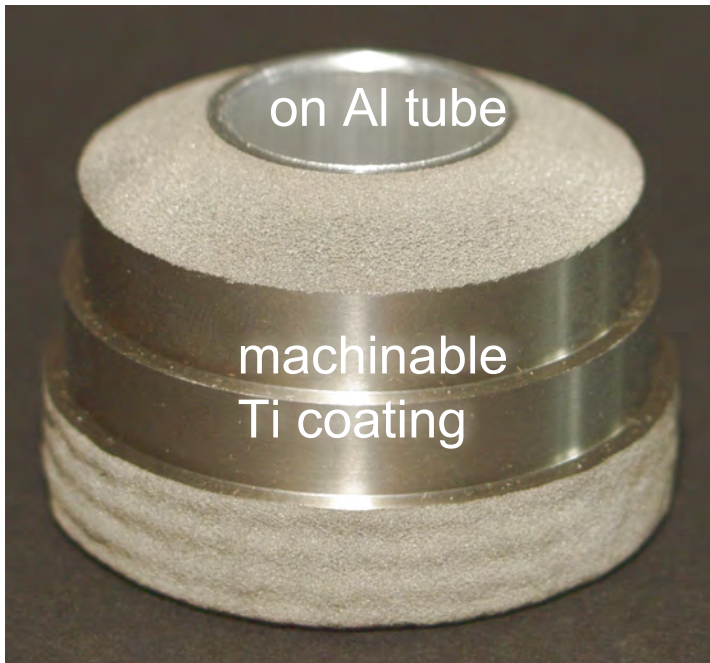
93 % of the fatigue endurance limit
of bulk Ti Grade 2

ductile failure
„riverlines“



cold sprayed Ti
High Cycle Fatigue
specimen annealed for 1h

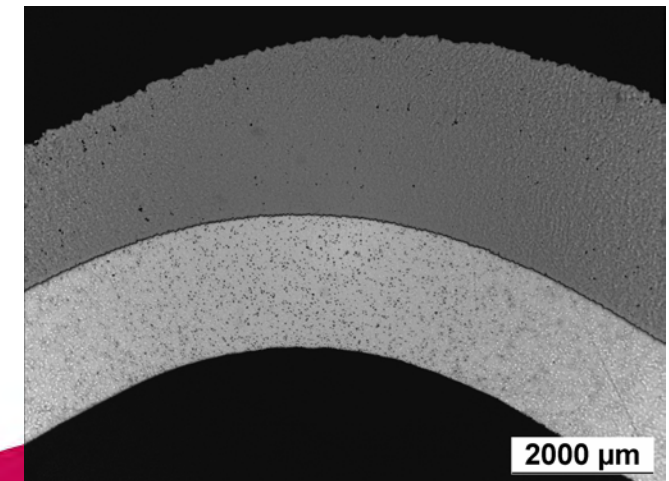
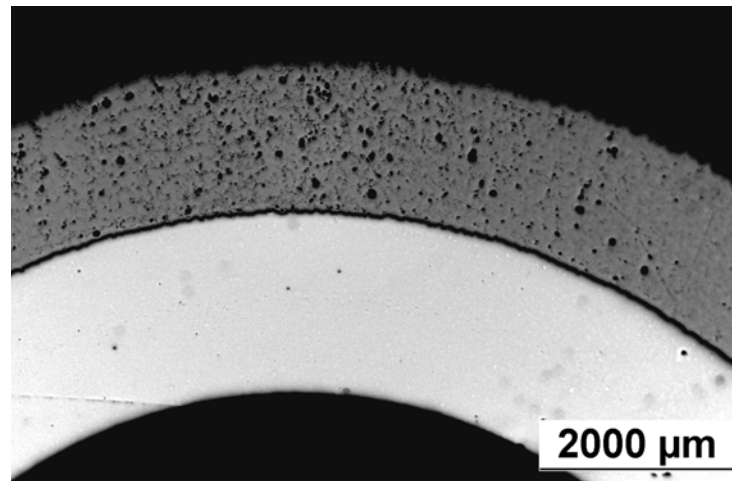
production of complex Ti-parts



challenge:
impact angle
at contours

goals achieved:

- fatigue strength 93% bulk
- tensile strength 560 MPa
- < 0.1% porosity
- > 95% DE
- < 1500 ppm Oxygen
- > 10 kg Ti per hour



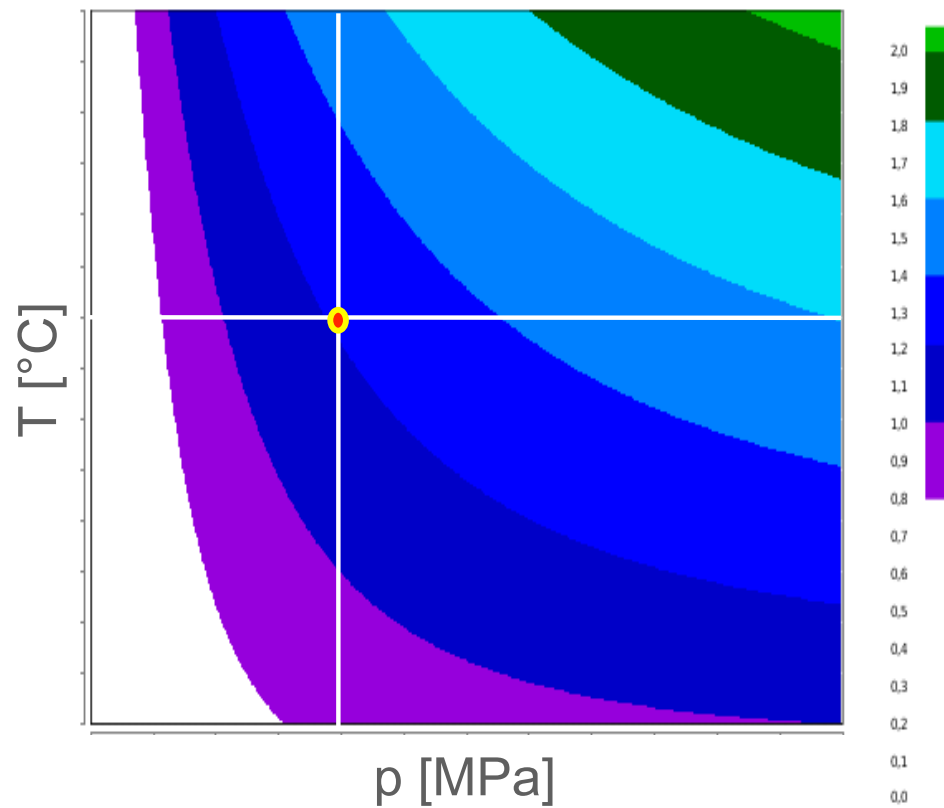
Cold Spraying of Al-alloys

Cold Spraying of Al-alloys

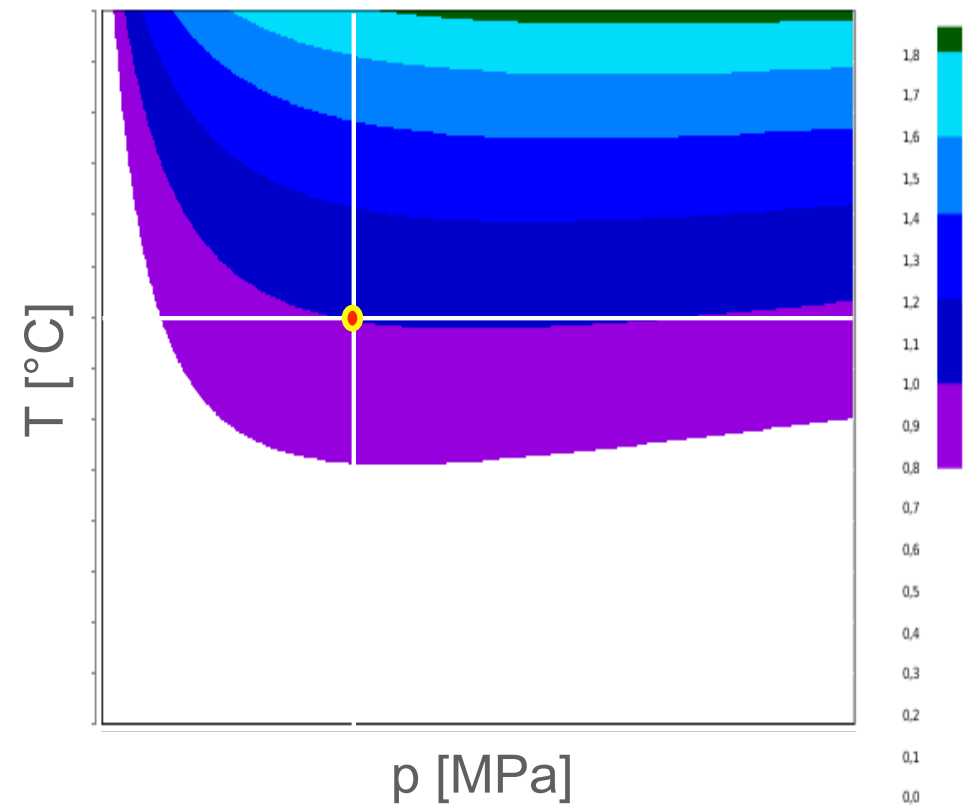
Parameter selection

η (gas pressure, gas temperature)

Helium

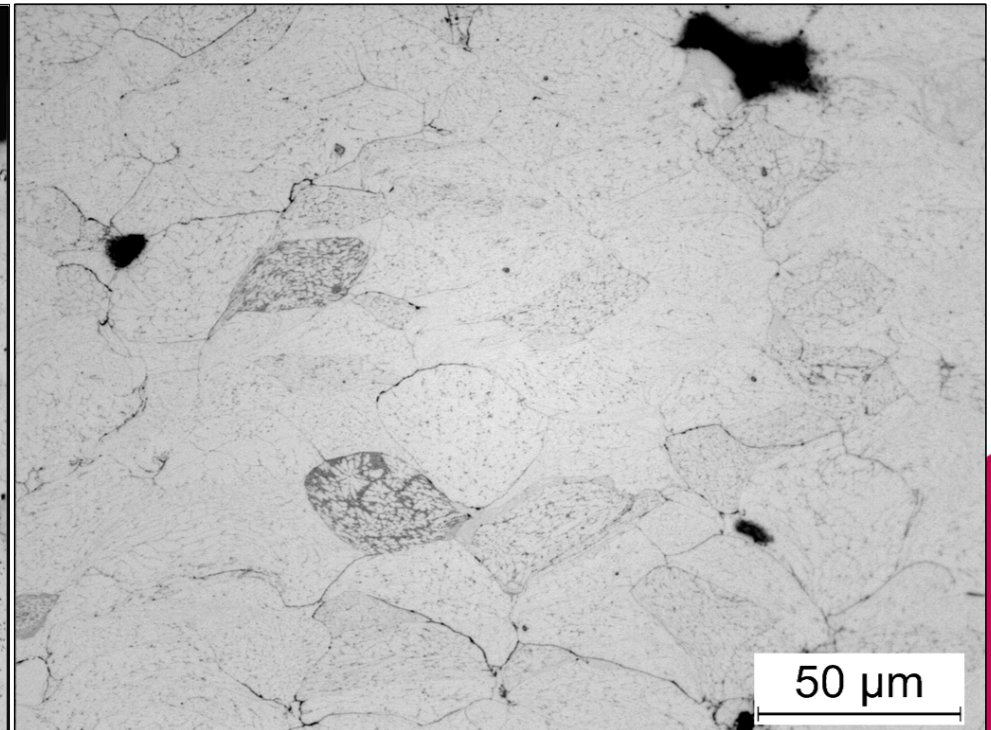
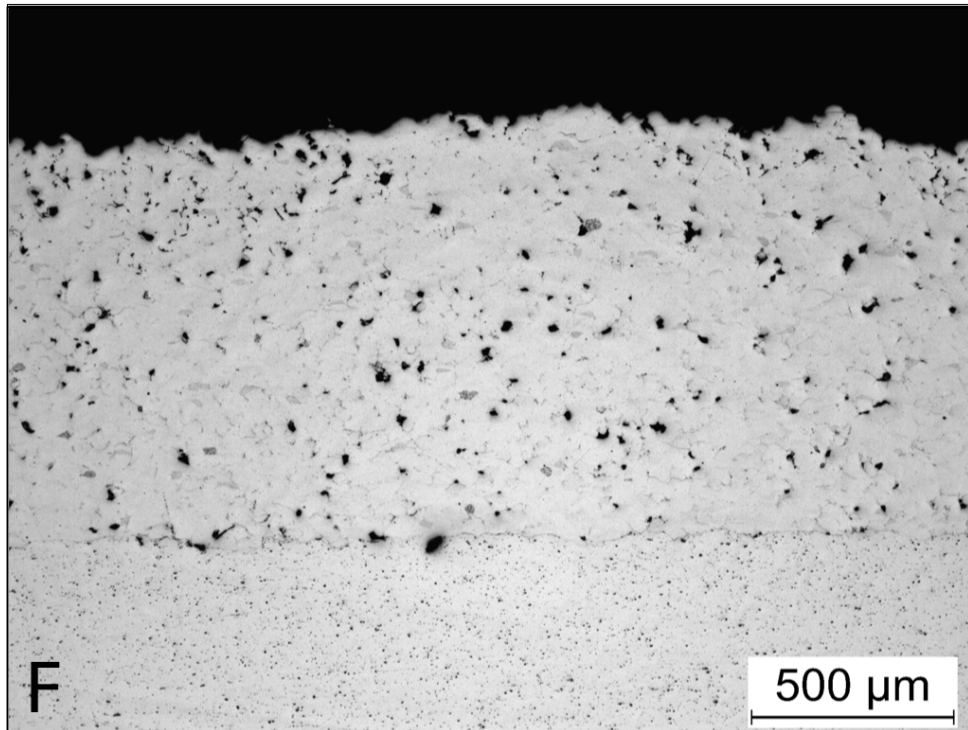


Nitrogen

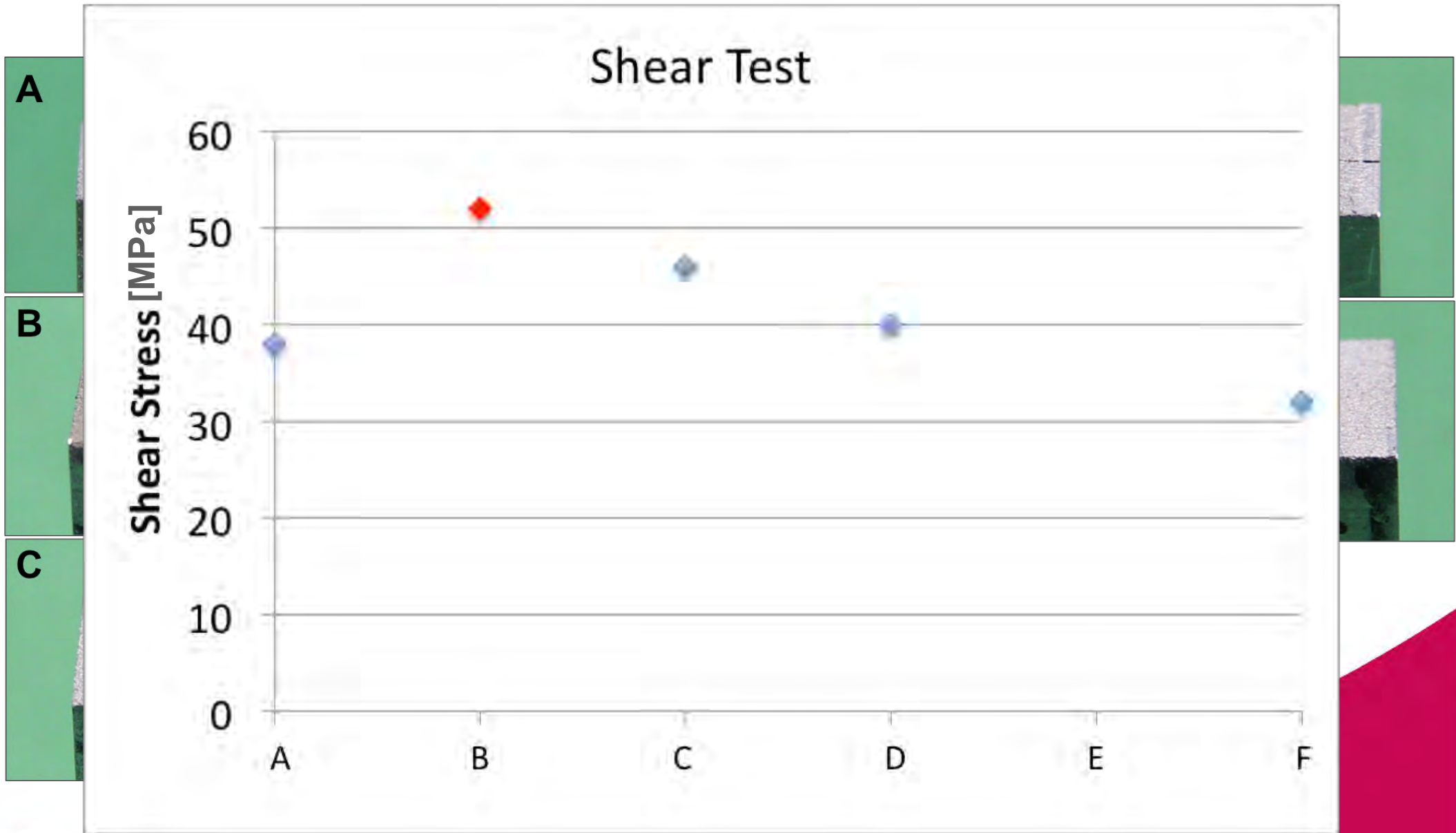


Coating Microstructures

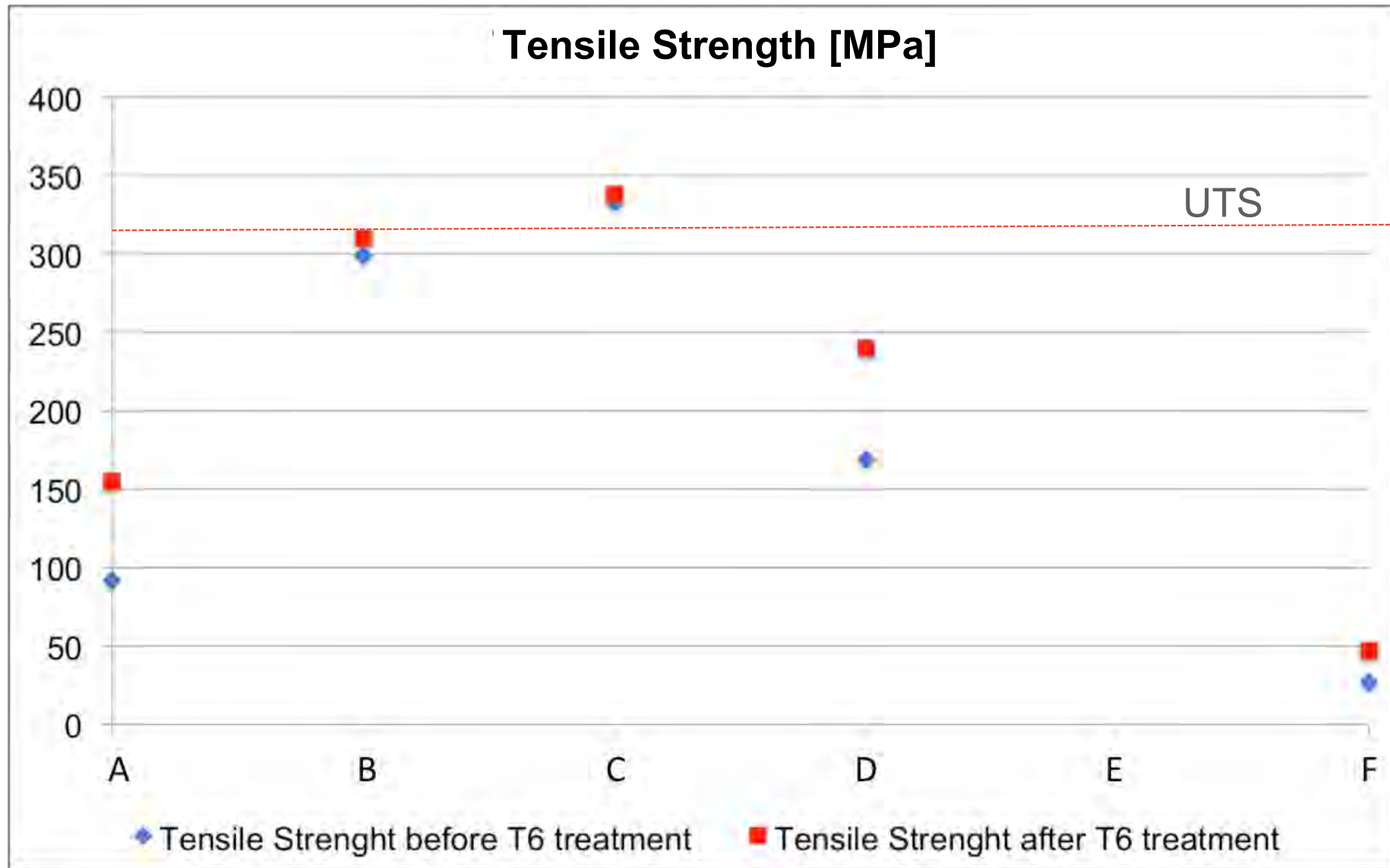
Spraying conditions	Cross-section hardness HV 0,3	Surface hardness HV 2.0	Porosity	η
A	97 ± 7	102 ± 7	$0,8 \pm 0,1$	1.21
B	104 ± 5	105 ± 5	$0,23 \pm 0,05$	1.35
C	106 ± 4	107 ± 4	$< 0,1$	1.45
D	105 ± 4	106 ± 8	$< 0,1$	1.14
F	89 ± 5	92 ± 6	$1,73 \pm 0,07$	1.30



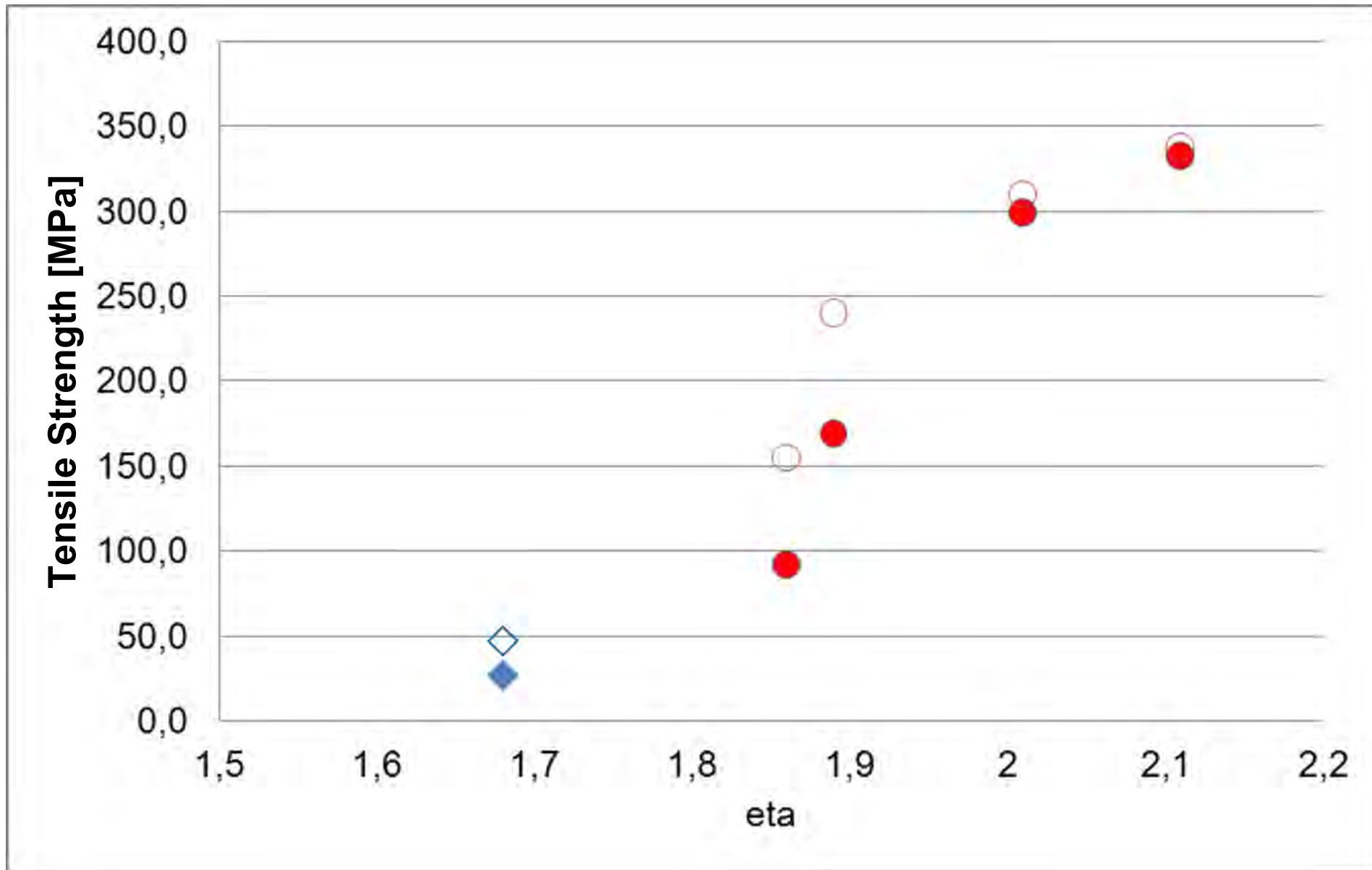
Shear Test



Coatings Strength (MFT)

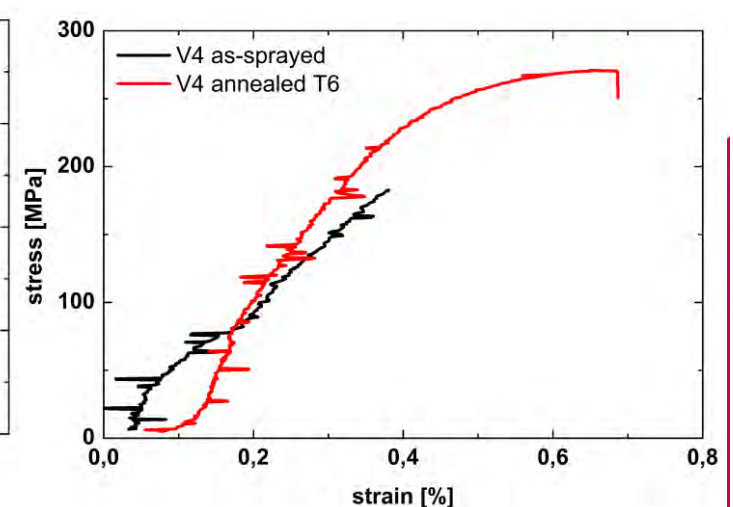
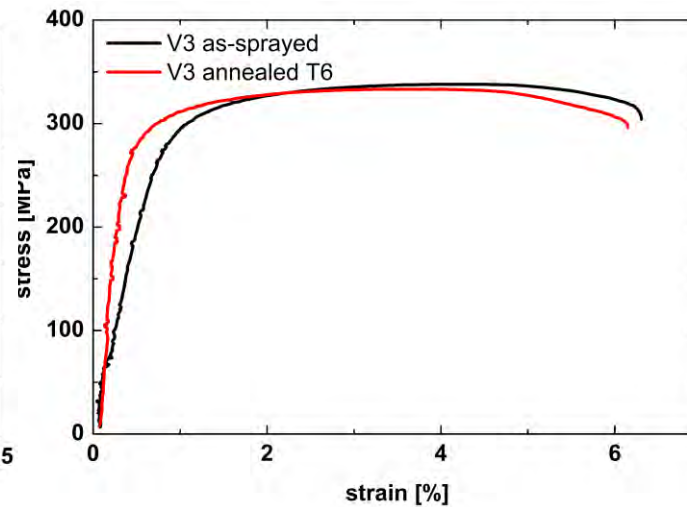
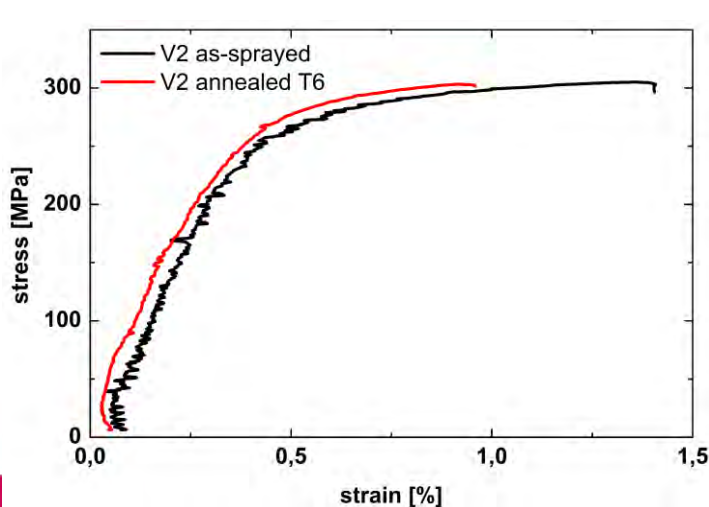


Tensile strength (MFT) vs eta

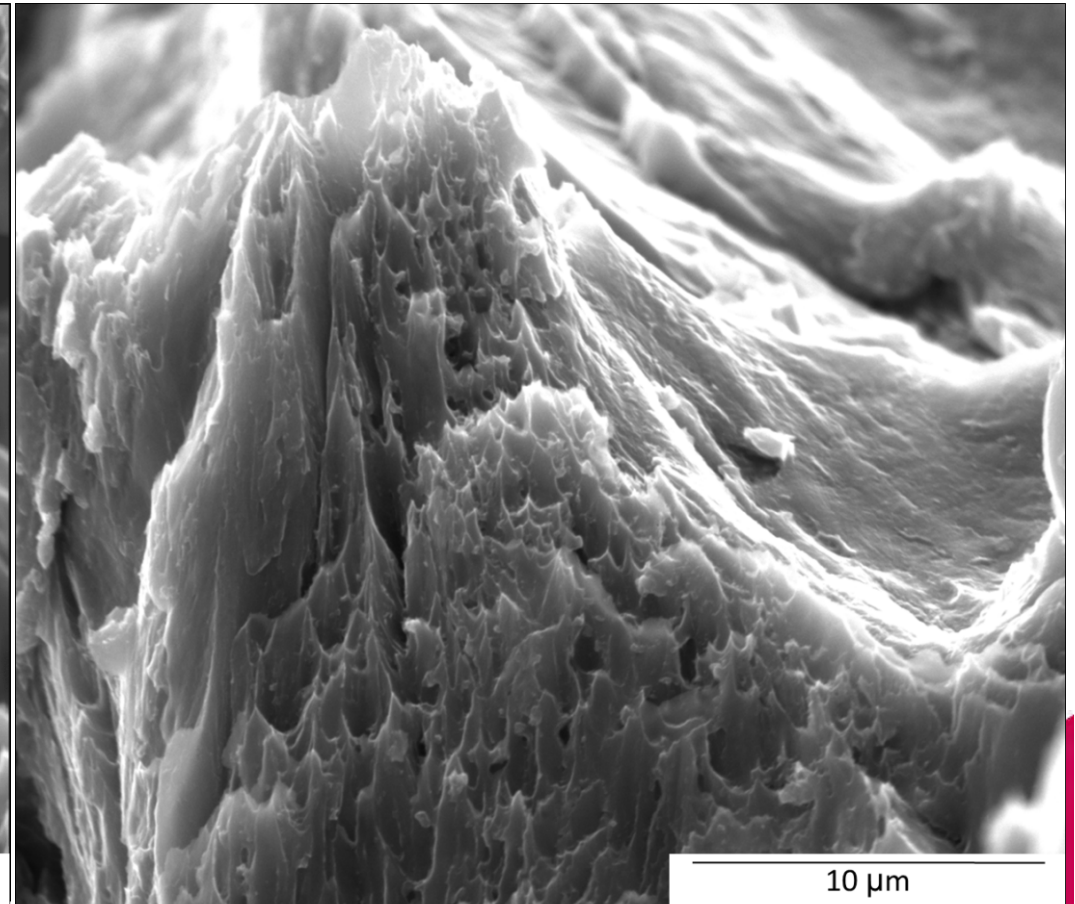
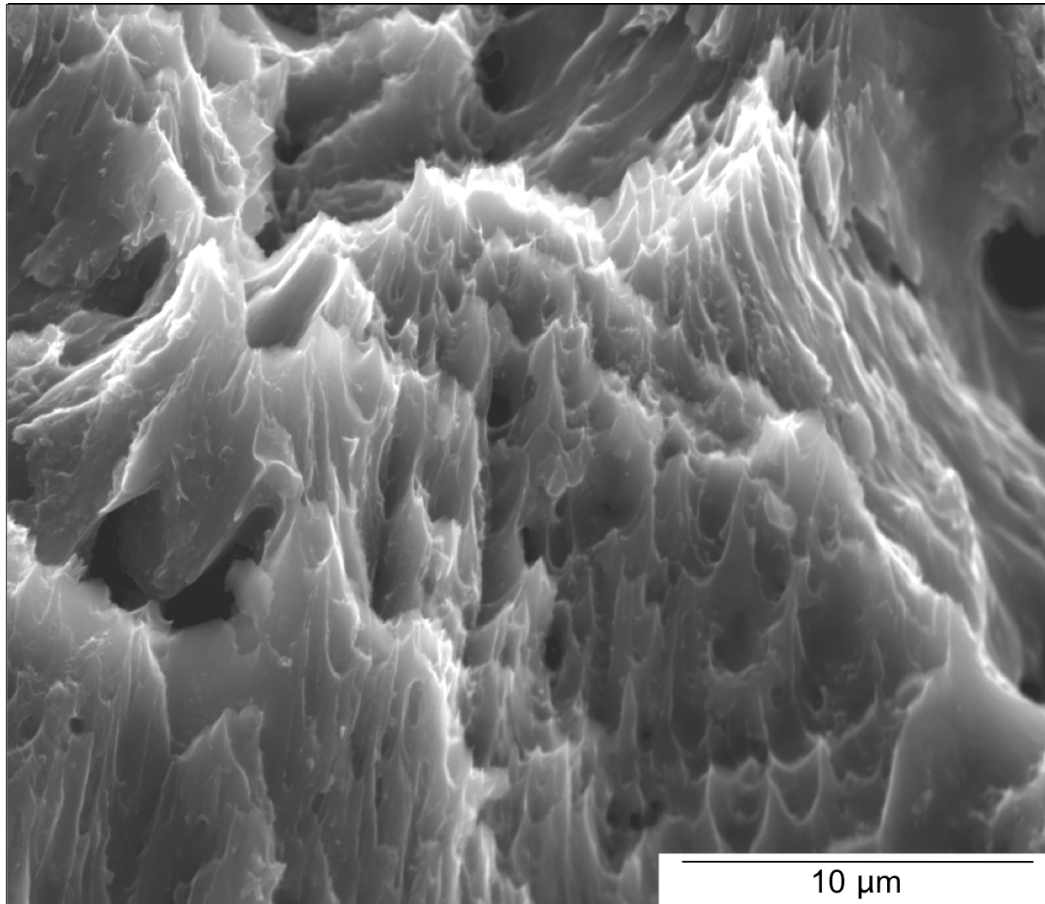


Coating Strength (MFT)

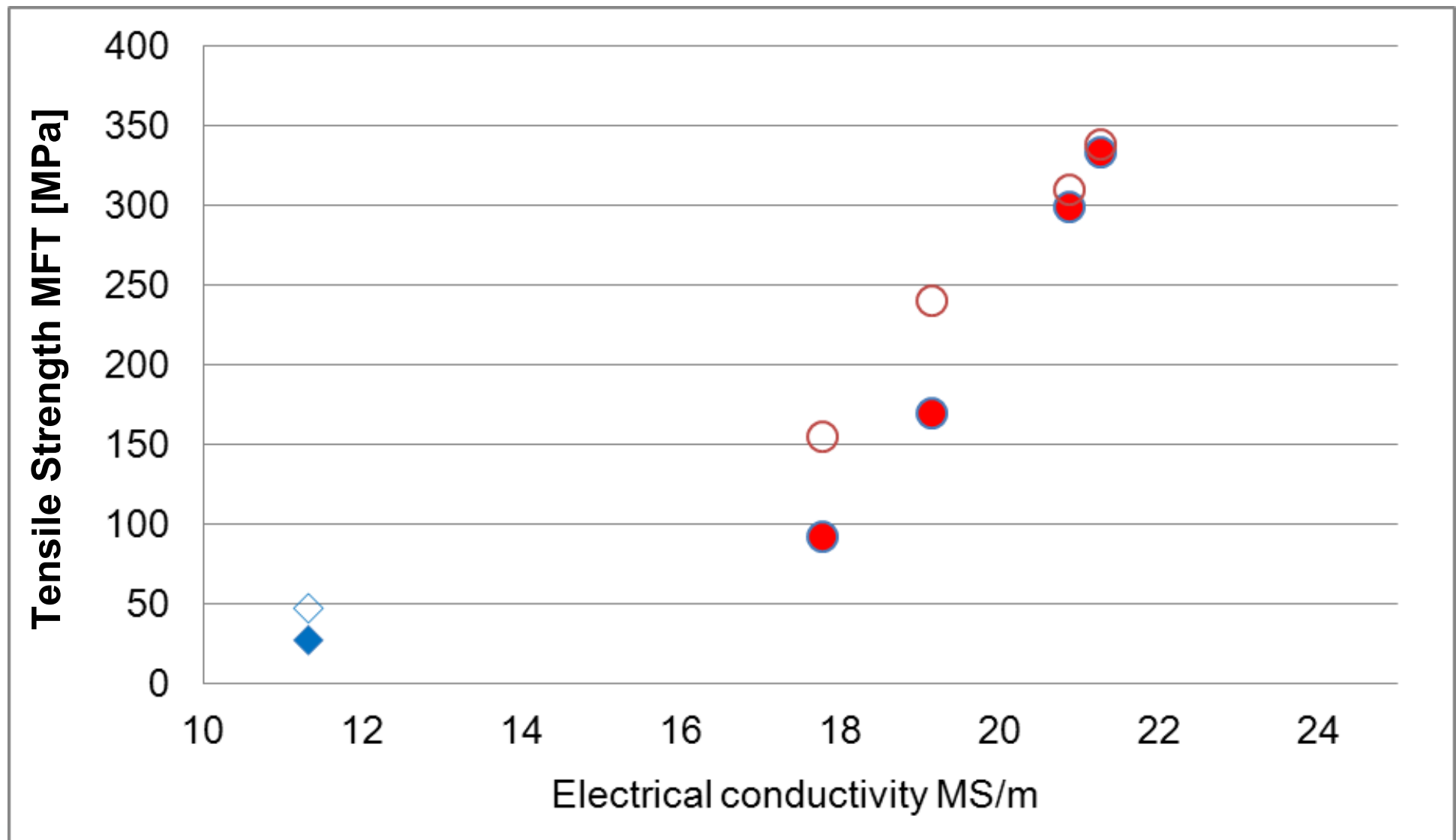
Parameters	yield strength (MPa)	UTS (MPa)	ductility (%)	total elongation (%)
B	277 ± 9	299 ± 6	0,7 ± 0,3	0,8 ± 0,3
B-T6 Treatment	289 ± 10	310 ± 4	1,0 ± 0,3	1,1 ± 0,4
C	293 ± 20	333 ± 3	2,7 ± 1,7	4,9 ± 1,7
C-T6 Treatment	291 ± 5	338 ± 7	3,1 ± 0,3	5,4 ± 1,0
D	-	169 ± 31	0,0	0,0
D-T6 Treatment	264	240 ± 36	0,1 ± 0,1	0,1 ± 0,1



Rupture Zone (MFT)



Quality Management: Electrical conductivity vs strength

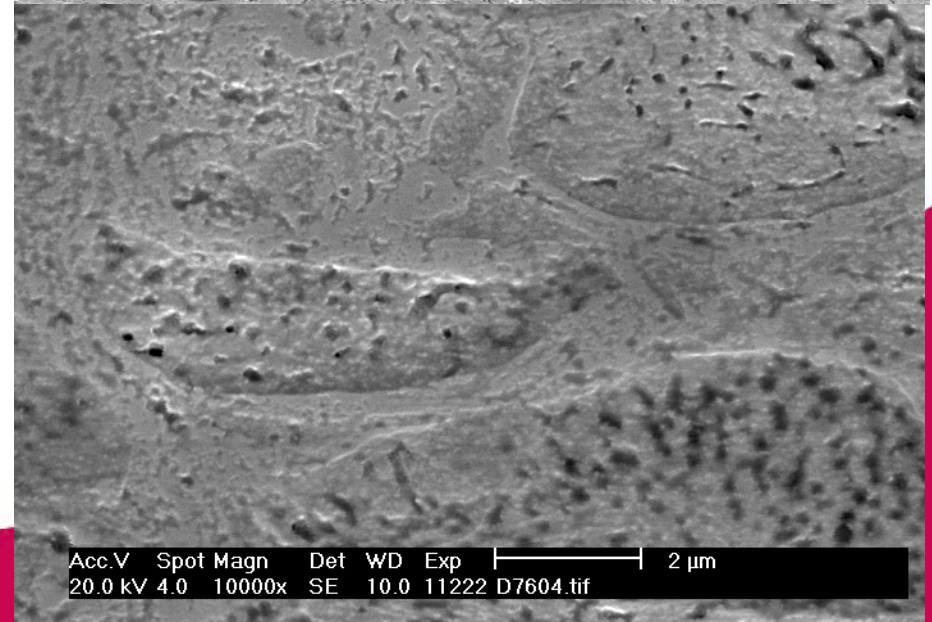
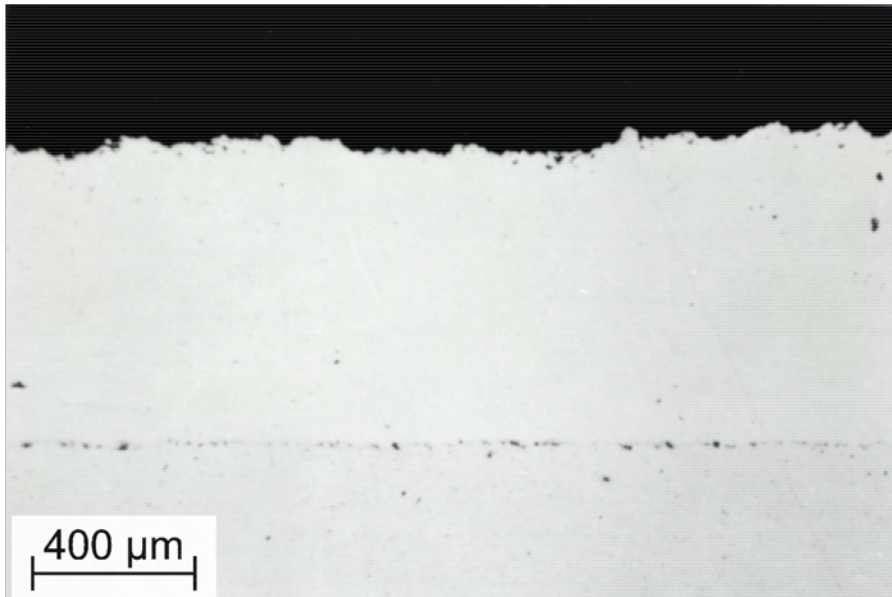


Kinetic Spraying – Ni-based superalloys

Ni-Superalloys: less brittle than expected due to deformation-induced phase transformation upon impact

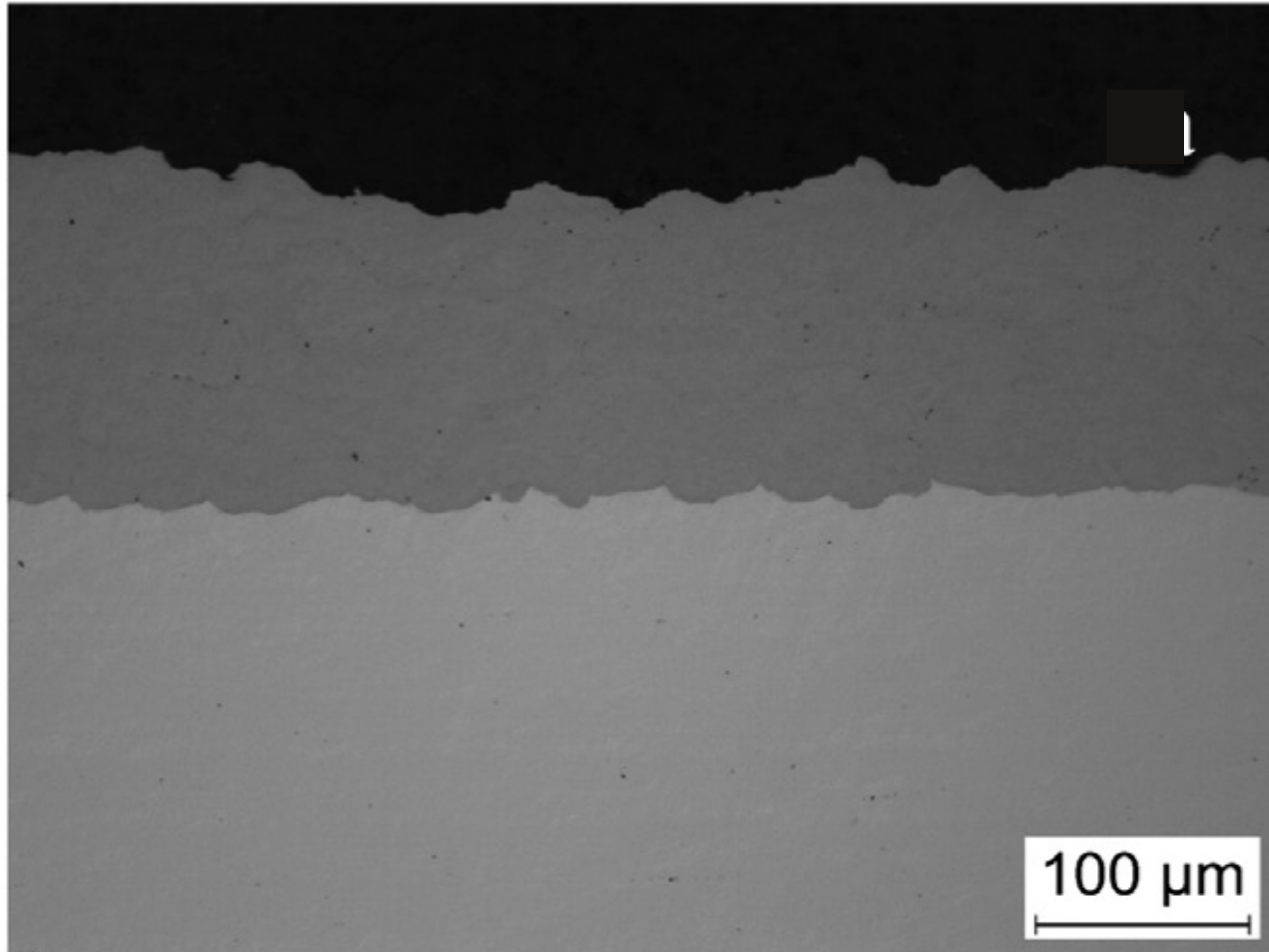
- Dense coating despite low impact temperature by spraying with He

process gas: He



Kinetic Spraying – Intermetallics

Intermetallic Fe - 40at.%Al



Centre de Projecció Tèrmica



conclusions

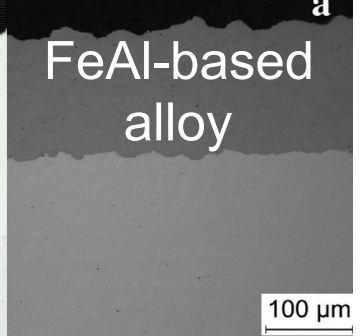
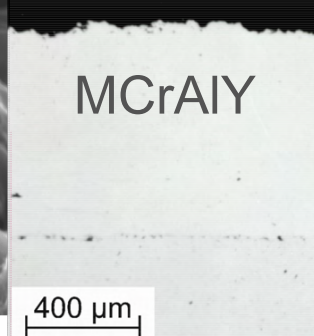
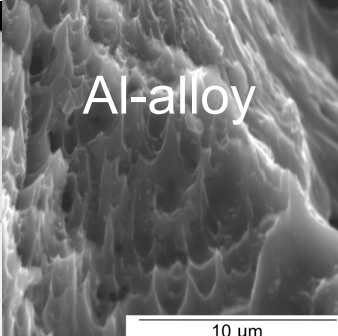
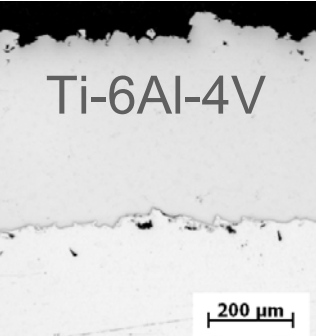
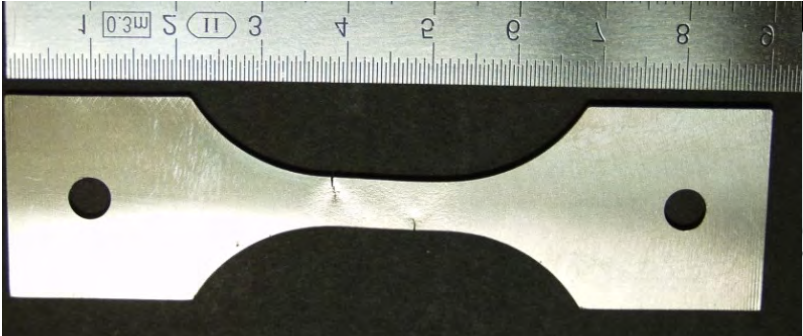
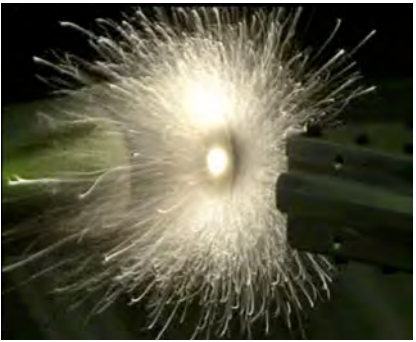
Understanding Mechanisms

Development of Spray Equipment

Cold Spraying for Aerospace Applications: bulk properties in repair or manufacturing!

coating quality „all-inclusive“ η

Kinetiks 8000-X:
nozzles, p, T



a