





Prediction of Particle Impact Conditions via CFD Process Modeling

ARL Cold Spray Modeling Program

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Program Objective

To generate a model or a series of models to predict the resulting mechanical properties of a deposit sprayed from a new material, based on the process parameters used produce the deposit.















Outline of Work at SDSM&T

- Estimation of effects of He/N_2 mixing through 1D model
- Produce particle splat samples and model process
- Accurate estimation of particle impact conditions through CFD
- Effects of particle injection imperfections through CFD
- Provide accurate input for solid mechanics models









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Today's Outline

- 3D case study: Powder feeder line misalignment
- Controlling particle impact velocity & temperature









Effects of Powder Feeder Line Misalignment

- Experimental velocity measurements reveal lower velocity particles than expected...
- Imperfections?
 - Hose assembly
 - Nozzle assembly
 - Feeder tube assembly
 - Powder feeder assembly
- Introduce imperfections to evaluate process sensitivity
 - Starting with feeder tube alignment



Can we simulate like real particle exit velocities by introducing imperfections?







Signs of Misalignment



- Accelerated wear in the nozzle
- Reduction in particle velocity
- Increase in velocity variation







Aligned Powder Feeder Tube





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Misaligned Powder Feeder Tube

















Physical Model



Gas Model

- Nitrogen (ideal gas)
- Energy equations
- k- ϵ turbulence model
- Hot gas input
 - 3.85 MPa & 360 °C
- Cold gas input
 - 3.85 MPa & 50 °C
- Outlet
 - Atmospheric conditions
 - 0.101 MPa & 20 °C
- Gas flow rate
 - 1150 g/min

Particle Injection

- Lagrangian particles (DEM optional)
- Input Microtrac data for d_p
 - Real particle size distribution
- Drag forces
- Lift forces
- Two-way coupled flow (Gas/Particle)
 - Momentum & Energy
- Particle injection rate: 12.4 g/min







Accounting for Losses from Particle/Nozzle Interactions

• Nozzle wall impact angles assumed*

< 30°

- Coefficient of friction*
 - Coulomb's law of dry friction (0.33)
- Tangential coefficient of restitution*
 - $e_t = 0.7$
- Normal coefficient of restitution*
 - $e_n = 0.8$

^{*}Wu, C.Y., Thornton, C., Li, L.Y. Rebound Behavior of Spheres During Elastic-Plastic Oblique Impacts. International Journal of Modern Physics B. 22 (**9, 10, 11**). 2008. *pp. 1095-1102*.





Simulation







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Model Validation



	Mean	Std. Dev.	Variance	Min	Max
	[m/s]	[m/s]	[%]	[m/s]	[m/s]
Aligned Tube Simulation	633	74	12%	432	809
Misaligned Tube Simulation	623	92	15%	430	852
TECNAR Measurement	627	80	13%	260	932







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Effects of Misalignment on Particle Impact



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Spray Radius & Particle Angle with Measurement Plane





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Particle Nozzle Interactions

Aligned Feeder Tube Scenario



Misaligned Feeder Tube Scenario









Effects of Misalignment on Nozzle Wear

- Reduction in nozzle expansion ratio
 - Nozzle throat wear
 - Drop in particle velocity
 - Reduction in the amount of
 - Inefficient increase in gas consumption
- Increase in nozzle expansion ratio
 - Wear in diverging section
 - Colder particles
 - Particles possibly impacting too substrate too fast
 - Causing erosion









Controlling Particle Impact Conditions

- Control impact velocity for an average size particle $(22 \ \mu m)$
- Help control particle bonding mode on substrate
- Use Al6061
- Use 1-D *He-N*₂ mixing model





Al 6061 Properties					
Density (kg/m^3)	2700				
Ultimate Tensile Strength (MPa)	310				
Melting Temperature (°C)	650				
Thermal Conductivity ($W/m ^{\circ}K$)	170				
Specific Heat ($J/kg \circ K$)	900				





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22 µm Particle Impact Velocity

		Particle Impact Velocity Contour [m/s]							
Impact Velocity Ranges		600	82	5	1050		1275	1	500
1 2 8									
		T [C] \\ P (MPa)	2.38	2.94	3.51	4.07	4.64	5.21	5.77
	0%	250	595	603	609	613	617	620	623
595 – 700 m/s	Не	300	620	628	634	639	643	647	650
		350	644	652	659	664	669	672	676
		400	666	675	682	688	693	697	700
	T [C] \\ P (MPa) 2	2.38	2.94	3.51	4.07	4.64	5.21	5.77	
741 005 /	50%	250	741	754	765	773	780	785	790
/41 – 885 m/s	He	300	770	785	796	805	813	819	824
	TIC	350	798	813	825	835	843	849	855
		400	824	841	854	864	872	879	885
		T [C] \\ P (MPa)	2.38	2.94	3.51	4.07	4.64	5.21	5.77
	75%	250	876	898	914	928	939	948	956
876 – 1065 m/s		300	909	932	950	964	976	986	995
	пе	350	939	964	982	998	1011	1022	1031
		400	968	994	1014	1030	1044	1056	1065
		T [C] \\ P (MPa)	2.38	2.94	3.51	4.07	4.64	5.21	5.77
	100%	250	1156	1198	1233	1261	1286	1307	1326
1136 - 143 / m/s	He	300	1193	1237	1273	1304	1330	1353	1373
		350	1228	1274	1312	1344	1371	1395	1416
Approved for Public Release		400	1261	1309	1348	1381	1410	1435	1457

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- 1. Capability of adjusting helium & nitrogen
- 2. 1D modeling of mixed gas spray conditions
- 3. Controlling particle impact conditions

- Assumptions
- 1. Constant nozzle geometry
- 2. Constant standoff distance
- Pressure is high enough to maintain supersonic flow exiting the nozzle





Sample Impact Velocity Variance Study Setup



- The desired particle velocity variance can be achieved by adjusting gas mixing ratio
- Recommended experimental setup:
 - Change impact velocity holding impact temperature constant
 - Varying pressure, temperature, gas mixing ratio for control

INPUTS				OUTPUTS			
Test No	He Mix	Gun Pres.	Gun Temp. η		Impact Vel.	Impact Temp.	
	[%]	[MPa]	[°C]	V _{im} / V _{cr}	[m/s]	[°C]	
1	0	5.21	300	0.91	647	122	
2	50	2.38	350	1.12	798	121	
3	75	2.38	400	1.36	968	120	









