



CSAT Meeting: WPI, Worcester, MA

B1 Bomber-FEB Panel Repair by Cold Spray

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Project Team



- Repair, Refurbish, and Return to Service Center (R3S) a SD Governor funded 2010 Center of Excellence at the South Dakota School of Mines and Technology (SDSMT)
 - Director, Christian Widener, Ph.D.
- HF Webster Engineering Services, Inc.
 - Mr. Rob Hrabe
- Air Force Engineering Technical Services Ellsworth AFB and Ph.D. student SDSMT
 - Mr. Brian James
- Army Research Lab
 - Dr. Victor Champagne
- Life Extension of Navy Weapon Systems Project managed by ACI Technologies, Inc. – Navy Mantech Benchmarking and Best Practices Center



- Mr. Carmine Meola
- Ms. Rebecca Morris







- Aluminum aircraft external access panels are typically secured to the airframe with steel TRIDAIR fasteners.
- The fasteners are designed to sit flush with the panel to enable laminar airflow over the fastener head.
- Repeated access to these panels wears and enlarges the holes in the panel.
- As wear increases, the fastener sits further and further below the surface of the panel, resulting in turbulent airflow, vibration of the panel, and eventual pull through and loss of the fastener in flight...





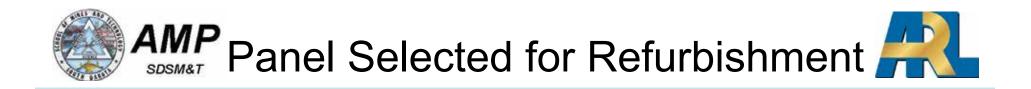


- Integrally stiffened bonded panel composite metal hybrid structure
- Currently, no acceptable permanent repair exists
- Furthermore, new repair technologies are not systematically incorporated into maintenance supply processes.
 - Organizational barriers prevent implementation of new technology into aging weapon systems
 - Very little funding is available for developing repair processes on legacy weapon systems
- Replacement Cost >\$200K each, but parts are not even available...Fleet liability of approx. \$50M.



A cold spray repair solution has been developed... ROI > 10:1





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External Doubler
 Repair



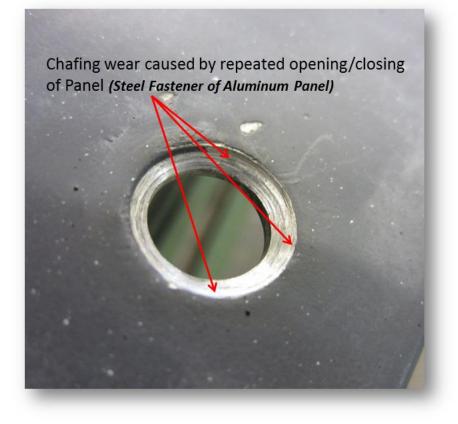
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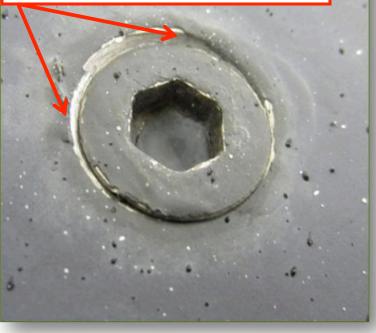


Example: Worn Fastener Holes





Damage accelerated by air turbulence on elongated fastener hole





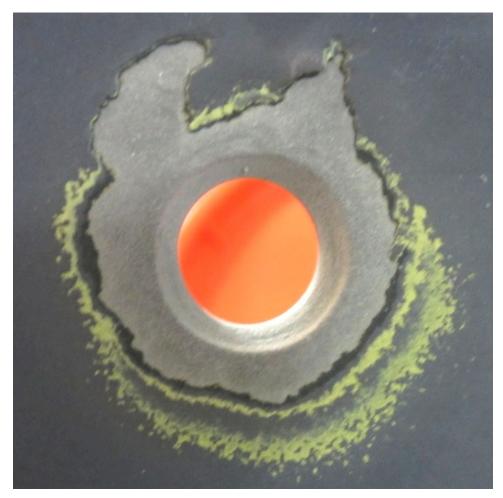
Repair, Refurbish, and **Return to Service**



Grit Blast



• Each hole was grit blasted prior to cold spray to remove paint from the area and to enhance bonding to the surface.





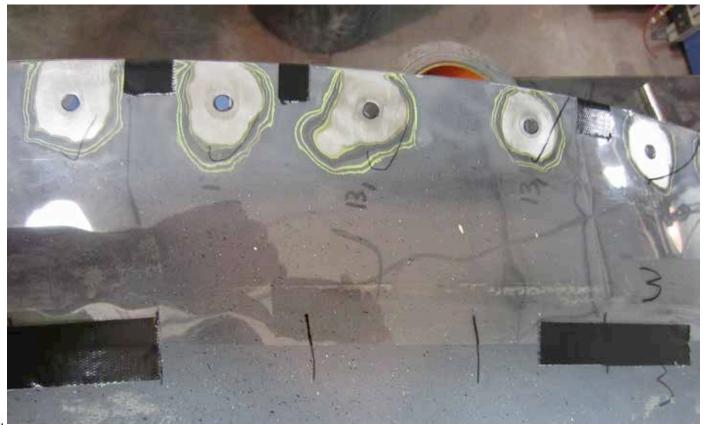




Template



• Templates were created on Mylar from the existing fastener holes prior to performing the cold spray repair.











- Temperatures on the back side of the panel were monitored by thermocouple and did not exceed 100°C.
- Max. observed transient temp during repair was 153°F, but • 137°F shown here was typical (<63°C).

There is no detrimental effect to the 2024 or composite material substrate at these temperatures.









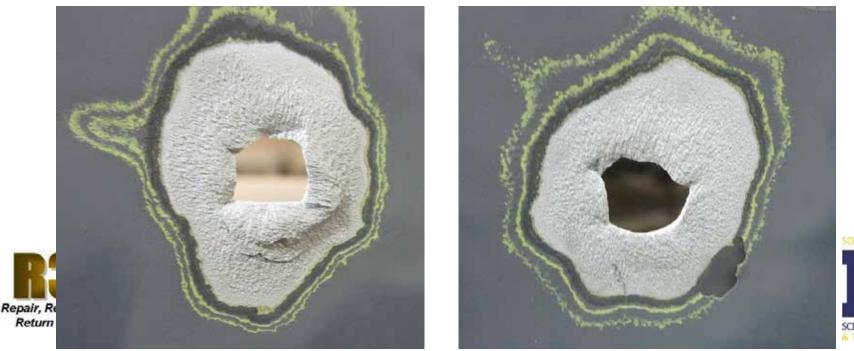




Cold Spray



- HP cold spray depositions were added by hand to the surfaces of the worn fastener holes.
- Gen II prototype HP CS system
- 350 psi, 350°C, A0027 Centerline powder –Ultralife[™] nozzle

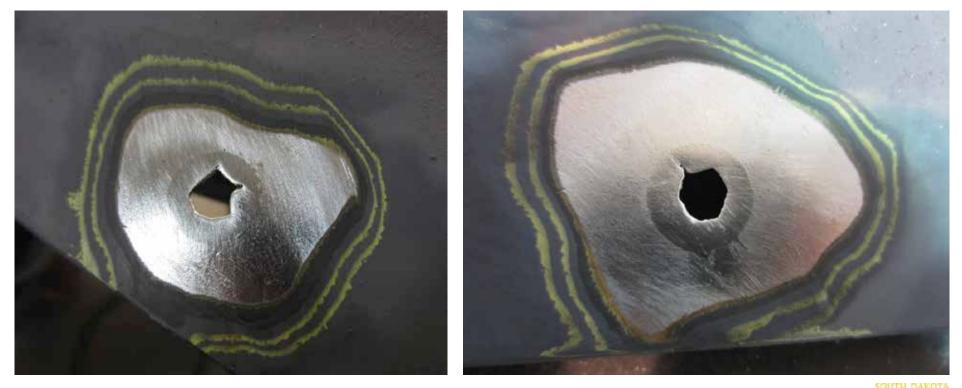




Fine Polish



• After grinding, the holes were polished with fine scotch brite discs.











• Final machining was performed using a micro-stop tool to cut the proper chamfer for the Tridair fastener.









After Micro-Stop



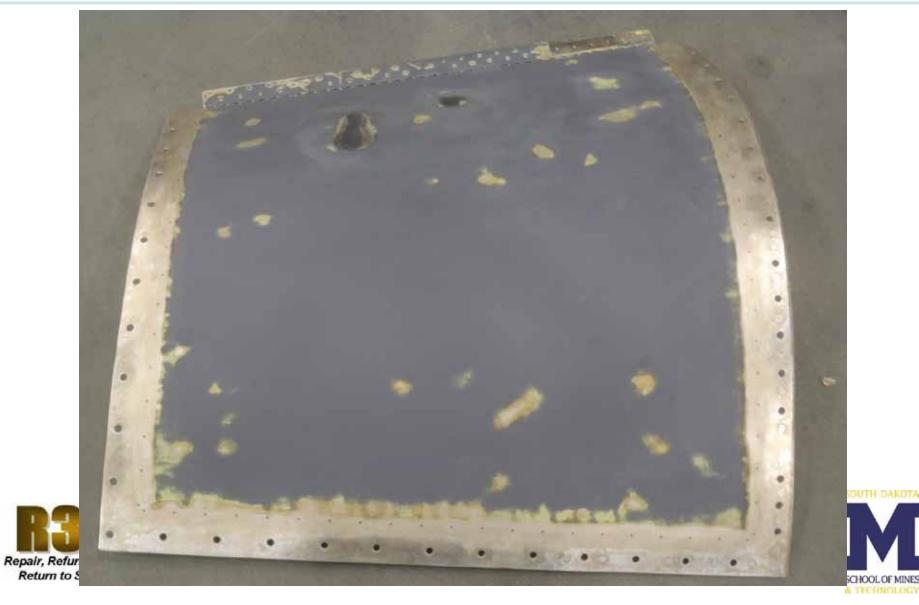
• Final repair before painting.













A5083 FEB Door - Primed







AMP A5083 FEB Door - Top Coat applied



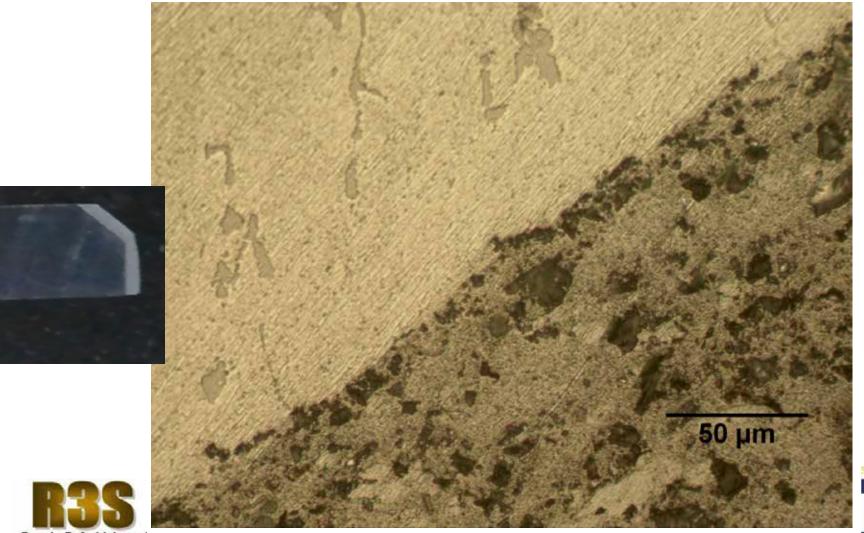












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SCHOOL OF MINES



Procedure



- Sprayed at SDSMT using a Gen II System
- A procedure for the repair of the fastener holes using cold spray was prepared by the R3S Center at SDSMT: CSPS-R3S-2012-AMP01.
 - The specification covers the repair of elongated fastener holes in 2024 aluminum sheet for aircraft skins.
 - The repair was documented using a cold spray process control sheet.

10000 (F1000)	KJS gan, Amarana, A. Intan in Jeruize Research Ganar	Cold Spray Procedure Specification	
	y Process Control Sheet	CSPS-R38-2012-AMP01	
VENDOR: SDSMT-R3SCes DEPOSITION #	ter Sheetof	L. Suge	
VENDORPROCESS *: PUPCHASEORDERNUMBER	CERTIFICATION: M4.865.921	This principles reveals the repair of dougsted furthers holes for secretly size 2004 colors and	
PART NUMBER: AREA TO RECEIVE DEPOSIT	5.N: ION:	II. Applicable Decements	
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METHOD OF CLEANING:	PARI DELPARALIUS	teen decree, to real broaded source an occases one along	
MASKING INFORMATION		 MESTD 2021 - DEPARTMENT OF DEFENSE MANUFACTURE 	
GRIT TYPE AND SIZE:		TTANDARD MATERIALS DEPOSITION, COLD SPRAY (64 A	
GRIT BLAST PRESSURE:		procedures connered by this standard are subsided to ensure that cold operations, either manual or automated, user proceeded experiment	
PRIMARY OAS:	TIMPERATURE	The saved to restore financially discrepant parts, or parts requiring the saved to restore financially discrepant parts, or parts requiring precession and wear (e.g. atraining, consider 5, and ensure) but us	
MAIN GAS PRESSURE	FEEDER GAS PRESSURE:		
COATING POWDER		abiotos	
POWDERMATERIAL-	POWDER SIZE:		
SUPPLIER:	MATERIAL LOT #	III. Paul Ingenties	
COATING DATA		1) Lightly card, with pales analyse earlies of each hole to sensive fe	
TIME BETWEEN SURFACE PI	REP AND SPRAY:	a. Use up to 10 gait pipes, be cautious of sandaig the edge of p	
POVDERFEED RATE:		Using port-a-blast get blaster, prepare hides for spray	
POWDER WHEEL SPEED:		a Using 85 grit A2203	
NOZZLE TO WORK DISTANC	1:	b. 10 20pe compressed at c. Be cure to rotati up entre hole, chamfer and arright sector.	
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DEPOSITION THICKNESS AS	SPRAYED:		
NUMBER OF PASSES FER LA	YER: NUMBER OF LAYERS:		
METHOD OF COOLING:			
NOTES:			
COLD SPRAY OPERATOR:	Date:		
APPROVAL Date:		15-826-202 AURI	

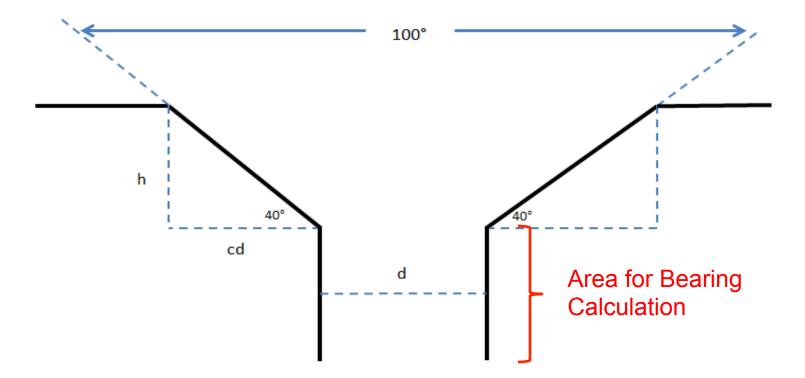


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Repair, Refurbish, and Return to Service















- Based on Mil-HDBK-5H guidelines, section 1.4.7, calculated bearing load depends on straight section thickness.
- Measured panel thickness of 0.147-in. leads to a max load of 3369 lbs.

P = Fbry*(t-h)*d $h = \tan(40^\circ)*(cd-d/2)$

t=0.095-in. bearing surface

Edge Distance	е	1.25	in
U	C		
Hole Diameter	D	0.375	in
e/D	3.333333		
Bearing Yield Stress	Fbry	95000	psi
Hole Diameter	d	0.375	in
Thickness	t	0.147	in
Countersink Depth	h	0.052	in
Load	Р	3369	lbs







Testing Procedure

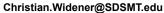


- Guided lap shear
- Fastener torque applied = 40 in-lbs
- Carried full Mil-HDBK fastener bearing yield load of 3400lbs.
- Tested up to failure at 5600 lbs no delamination at failure









Repair, Refurbish, and Return to Service





Cold Spray Adhesion

- Three lug shear testing
- >5000 psi avg. interface strength (Avg. 5681 psi ± 729)





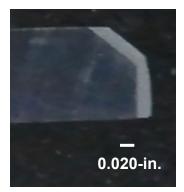




Testing Results



No evidence of cold spray material failure observed up to full bearing yield.







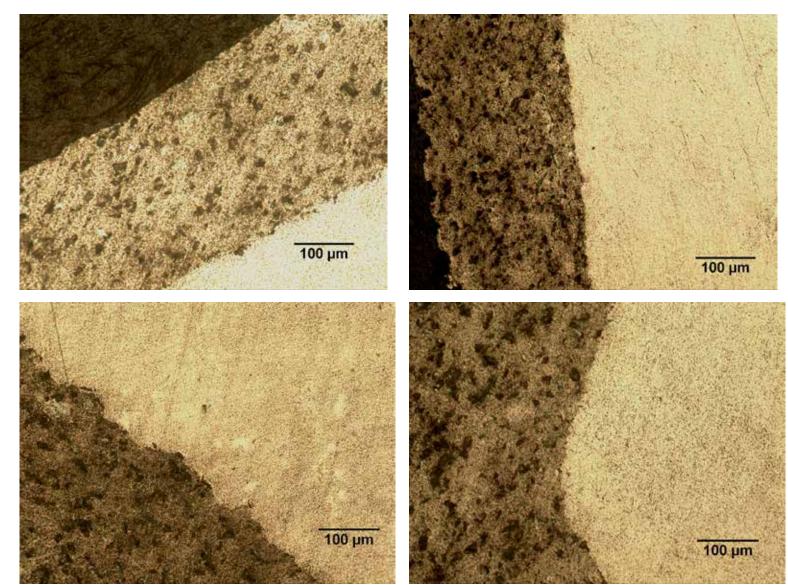












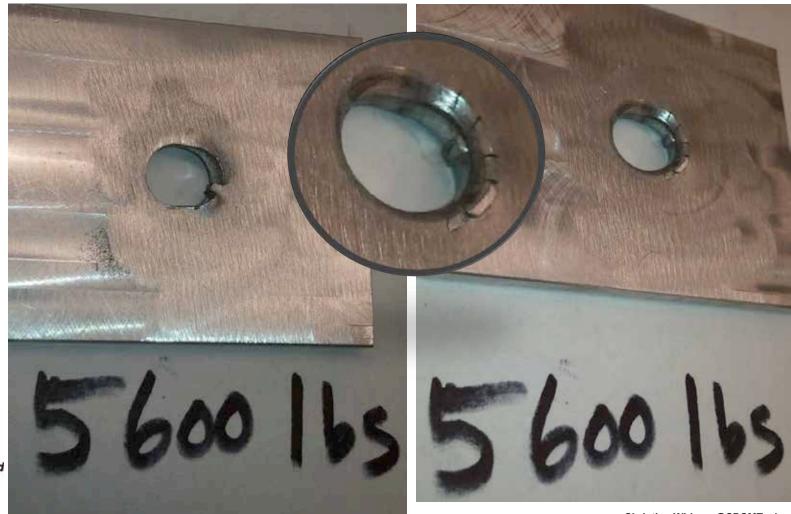




Failure Load Testing



• Even tested up to failure at 5600lbs, the cold spray material did not separate from the coupon.



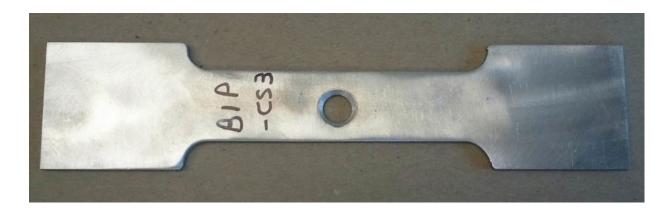






Fatigue Testing

- Open hole fatigue testing
- Coupons prepared per CSPS-R3S-2012-AMP01
- Testing performed per ASTM E466
- R=0.1
- At 15 ksi tensile stress (typical upper end for aircraft skin design loads) coupons lasted approx. 500,000 cycles.









Conclusions



- Panels can be restored to their full form, fit, and function.
- Cold Sprayed coupons **met or exceed the required bearing loads** for the parent material and fastener type for this application.
 - Even when tested to failure (greater than 1.5 x bearing yield) the cold spray material did not separate from the panel.
- The repair is expected to have an acceptable lifetime in service, and represents minimal risk of failing in service.
- The coating could even be reapplied if needed, since the process does not overage the substrate material.
- The repair is currently flying on a B1 under an ETAR (since August 2012).







Future Efforts



- The process is now being licensed by MOOG, and has potential application on other DoD and commercial aircraft
- A broad collaborative effort is also being initiated with the support of Tinker AFB to do a much larger qualification program to consider making it a part of the approved repair procedures for the B1.
 - Full qualification testing protocol, including spray parameters & powders
 - Identify opportunities on other aircraft
- Continue development of VRC-Gen III HP Hybrid Cold Spray System...



