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Suppression of Clogging in Cold Spray Nozzles

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CSAT 2018
Worcester Polytechnic Institute
June 19-20th

CSAT Cold Spray Action Team



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OUTLINE


1. Clogging. Causes and how to prevent it
2. Joule-Thomson effect
3. Development of the prototype
4. Testing the prototype
5. Results
6. Next steps

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Our enemy: clogging

- One of the biggest issues in Cold Spray
- Expensive problem (time + money)
 - Replacing the nozzle
 - Short operation times
 - Low quality of the deposit
- We know little about the exact causes of clogging



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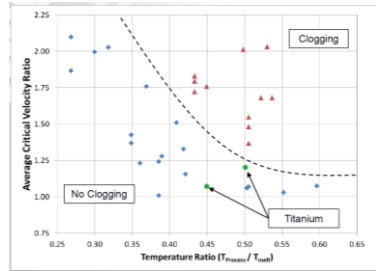
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What we know about the clogging

KNOWN SUSPECTS:

- Low-melting point particles
- Preheated particles
- High temperature of the nozzle wall

Empirical Data



Matt Siopis. Study of Nozzle Clogging During Cold Spray. CSAT 2017

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Strategies to prevent the clogging (I)

Nozzle material and geometry

Patent: US20130327698 A1
Nozzle for cold spray allowing for greatly improved long-term sustained usage over the prior art, without the occurrence of nozzle clogging.
Glass, Quartz or Boronitride

Patent: US20130087633 A1
An improved cold spray gun apparatus and system, which prevents nozzle clogging and erosion of the nozzle material. Spherical tetraamorphous silicate (STSA), low expansion glass, or silicon nitride.

Patent: US 20049191489 A1
Clogging of the passageway in the supersonic nozzle (4) is prevented by forming at least the diverging section (102) from polybenzimidazole (PBI).

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Strategies to prevent the clogging (II)

Cooling of the nozzle wall

Water cooling device

X. Wang, B. Zhang, J. Lv, S. Yin Investigation on the Clogging Behavior and Additional Wall Cooling for the Axial-Injection Cold Spray Nozzle. *Journal of Thermal Spray Technology* 24 (2015) 697-701.

Reduces nozzle wall temperature
Delays nozzle clogging when used.

Legend: 2.5MPa, 873K (solid lines); 2.5MPa, 873K (cooling) (dashed lines).
Pressures: 2.5MPa, 873K (blue); 2.5MPa, 873K (red); 2.5MPa, 873K (green).

The graph shows that wall temperature decreases significantly when cooling is applied, especially at the nozzle throat (around 100mm axial position).

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Strategies to prevent the clogging (III)

Active cooling of Cold-Spray nozzles by compressed CO₂ expansion

Joule-Thomson effect

$$\mu_{JT} = \left(\frac{\partial T}{\partial P} \right)_H$$

The graph shows the Joule-Thomson coefficient (kJ/bar) for H₂, N₂, Ar, and CO₂ as a function of temperature (K). CO₂ is circled in red, indicating its high coefficient at room temperature.

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Development of the prototype (I)

Inspirational ideas.

Fig. 5. Design rendering of the nitrogen-cooled spray nozzle.

Fig. 6. Cross-sectional view of nitrogen-cooled spray nozzle.

Fig. 7. Spray rendering of the nitrogen-cooled spray nozzle.

Fig. 8. Cross-sectional view of nitrogen-cooled spray nozzle.

Temperature points: T1 176.4°F, T2 118.2°F, T3 118.2°F, T4 126.7°F, T5 81.0°F, T6 81.0°F, T7 81.0°F, T8 168.4°F, T9 83.4°F.

Nitrous oxide cooling in hybrid rocket nozzles, *Progress in Aerospace Science*, 46 (2010), 106-115

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Development of the prototype (II)

Mk.1

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Development of the prototype (III)

1/16" stainless steel pipe

CO₂ expansion

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Development of the prototype (IV)

$\phi = 0.5$ in

6 in

WC nozzle

Throat

Mk.2

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Development of the prototype (V)

Mk.2


Patent applications filed.

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Lab testing of the prototype (I)


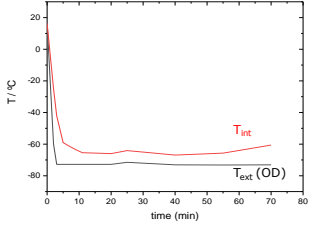
A couple of twin-linked high-pressure pumps pressurize the CO₂ and allow the system to run continuously while connected to a CO₂ tank.



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Lab testing of the prototype (II)

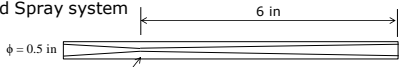
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Cooling tests at UTRC (I)

- VRC Gen III Cold Spray system
- WC nozzle
- 30 bar He
- 300 – 600°C
- High purity Ni (Praxair Ni-914-3)



0.058" x 0.200" 5° >>>> Temp. difference ID-OD 25-60°C

Special thanks to Matt Siopis and Aaron Nardis at UTRC

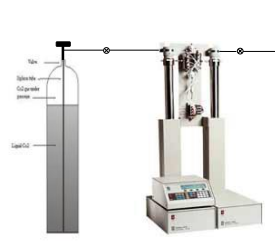

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Cooling tests at UTRC (II)

Experimental set up

CO₂ tank (w/ syphon) High-pressure pumps

Cold Spray system + robotic arm w/ cooling dev

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Cooling tests at UTRC (III)

Sample	Spray conditions	Cooling device	Clog	Time / min	Cooler Temp.
1	350°C	On	No	6	81
2	400°C	On	No	6	109
3	450°C	On	No	14.5	187
4	500°C	On	No	9.5	210
5	550°C	On	No	8	255
6	600°C	On	No	9.5	288
7	600°C	Off	Yes	3.5	368

The device was able to cool down effectively the nozzle's outside wall at all the conditions tested and to prevent the clogging

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Simulation Details

Pressure Inlets: 698 K, 4 MPa

Pressure Outlet: 300K, 101325 Pa

Tungsten Carbide Cobalt
Nozzle wall

- Axisymmetric Steady State Model
- VRC nozzle used @ UTRC
 - 0.068" Throat Diameter
 - 6" Diverging Length
 - 0.2" Exit Diameter

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Cooling tests at UTRC (IV)

Computed Heat Transfer Rate

What we have:

- $q = 832 \text{ W}$
- Inlet Temp: 698 K
- Outside Wall Temp: 421 K

What we want:

- $q = 3700 \text{ W}$
- Inlet Temp: 698 K
- Outside Wall Temp: 210 K

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Cooling tests at UTRC (V)

Cooling jacket experiment results

Measured Wall Temperature

Wall Temperature (K)

Inlet Temperature (K)

$y = 0.8549x - 176.07$
 $R^2 = 0.9788$

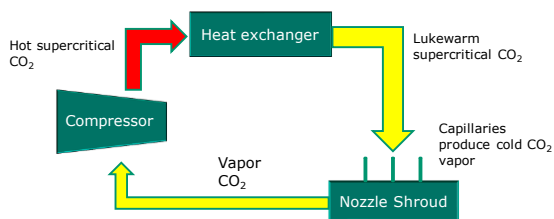
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Next steps (I)

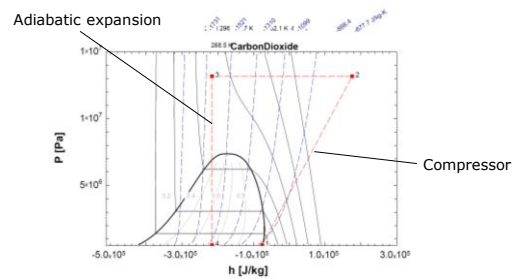
- Greater flow rate
- Automatization of the system
- Increase the operation time (60 min)
- More compact pump system

Next steps (II)

- Final design
- Reduce size
- Increase safety measures
- Flexible lines
- Recycling of CO₂

Recycling the CO₂

Essentially, a supercritical CO₂ refrigeration system

CO₂ refrigeration system

CONCLUSIONS

We have designed and fabricated a prototype of an experimental device able to cool down significantly the inner wall of the Cold Spray nozzle taking advantage of the adiabatic expansion of CO₂ in the outer wall of the nozzle to overcome the appearance of clogging.

We were able to effectively remove heat from the nozzle's outside wall using this prototype and prevent the appearance of clogging inside the nozzle.

With the cooling device we were able to cold spray systems and conditions ever reached before.